TANK 5 API 653 OUT-OF-SERVICE INSPECTION AND SUITABILITY FOR SERVICE EVALUATION FINAL CONDITION ASSESSMENT REPORT (PRE-REPAIR)

Joint Base Pearl Harbor-Hickam, HI (JBPHH)

August 20, 2020

Date of Inspection: October 2017 - January 2018

Contract Agency



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EEI Project No. 8877

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SUITABILITY FOR SERVICE TESTAMENT TANK 5

Enterprise Engineering, Inc. (EEI) completed a comprehensive, out-of-service, external and internal integrity inspection and suitability for service evaluation of Tank 5 at the Red Hill Fuel Storage Facility, NAVSUP FLC, Pearl Harbor, HI. The inspection was performed from October 2017 through January 2018. The inspection was performed in accordance with the applicable criteria of API Standard 653, UFC 3-460-01, UFC 3-460-03, the Statement of Work and the project's approved Inspection and Testing Plan.

The EEI inspection and evaluation found conditions that affect the hydraulic integrity of the tank. These conditions must be addressed prior to returning the tank to service.

This report provides inspection findings, tank suitability for service evaluation, conclusions, and recommendations for repair. Recommendations for continued long-term service are also provided.

EEI recommends the next internal out-of-service inspection be scheduled no later than January 2038 (20 years from 2018 inspection), or sooner if a change in condition has occurred.

In accordance with API Standard 653, this report satisfies the requirement for an out-of-service, integrity inspection and as such, should remain available as a historical record for future reference.

I hereby acknowledge that being familiar with the provisions of API Standard 653, the inspection and evaluation was performed in accordance with the provisions of API Standard 653 and good engineering practices, and with the exercise of usual and customary care.

This tank inspection has determined that mandatory repairs are required prior to return to service. Tank 5 may not be returned to service at this time. Recommended repairs have been identified, and if possible, should also be completed before returning the tank to service.

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TANK 5

API 653 TANK INSPECTION SUITABILITY FOR SERVICE EVALUATION RED HILL FUEL STORAGE FACILITY, NAVSUP FLC, JOINT BASE PEARL HARBOR-HICKAM, HI (JBPHH)

1.0 SUMMARY

Enterprise Engineering, Inc. (EEI) has completed a comprehensive, out-of-service internal integrity inspection and suitability for service evaluation of Tank 5 at the Red Hill Fuel Storage Facility, Naval Supply (NAVSUP) Fleet Logistics Center (FLC) Pearl Harbor, Hawaii under contract to Naval Facilities Engineering and Expeditionary Warfare Center (NAVFAC EXWC). The inspection was performed between October 2017 and January 2018. The inspection was performed in accordance with the applicable criteria of API Standard 653, UFC 3-460-01, UFC 3-460-03, the Statement of Work, and the approved project Inspection and Testing Plan.

Tank 5 is a mined underground storage tank consisting of an upper dome, barrel, and lower dome. The tank was constructed between 1940 and 1943 and is comprised of a reinforced concrete shell with a welded steel liner. As the reinforced concrete shell provides tank structural integrity and the steel plates serve as a shell liner, the entire tank (upper dome, barrel, lower dome) follows the requirements of API 653 for tank floors. Tank 5 is 100 feet in diameter, has an overall height of 250 feet, 6 inches, and has a nominal capacity of 300,000 bbl.

All accessible surfaces of the tank steel liner and plate butt welds were inspected by TesTex, Inc. (TesTex) using Low-Frequency Electromagnetic (LFET) (liner plates) and Balanced Field Electromagnetic (BFET) (welds) testing methods. The findings from the initial TesTex scanning were further evaluated (prove-up) by EEI through visual (VT), magnetic particle (MT), and phased array ultrasonic (PAUT) inspection techniques. In addition, EEI performed 100% visual inspection on all accessible tank shell liner plates and welds to confirm findings and identify additional indications. Further inspection was performed using vacuum box techniques on various components including the base of the tower legs, and the welds on the adjustment plate and expansion joint.

Common weld discontinuities that were identified included: porosity, undercut, lack of fusion, and incomplete fill. The majority of weld defects originate from the original construction and are located in the upper dome and extension ring plates. Other weld defects are a result of cover channel construction. More specifically, these defects were located on the fillet welds of the cover channels of the abovementioned areas in the tank. The upper dome inspection also identified several dent and gouge defects that require repair. These dent/gouge types of defects are presumed to be from contact from the boom end or other machinery and the tank shell.

Backside corrosion appears to be present within Tank 5. Defects were found in course A, B, C, and D of the upper dome, the extension ring, and barrel courses. However, it should be noted that most of the lower thicknesses in these areas were a result of grinding by a previous contractor under a separate contract, and not directly related to backside corrosion. Several large repair patch plates will be required to remediate the affected areas in the upper dome course A and extension ring areas of the tank. Repairs for each indication meeting or exceeding the repair threshold were determined during inspection of the tank. The repairs fall under two categories: weld repair or patch plate. Weld repairs will include grinding of the existing weld until the defect is no longer present and then rewelding of the area to meet weld profile and

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penetration criteria. Patch plates are generally designed per API 653 requirements (with some clearance exceptions) and will be fillet welded to the existing tank steel liner.

Because the structural integrity of the tank is provided by the reinforced concrete shell and the steel tank plates serve as a liner for the concrete, patch plate repair design and weld spacing for all areas of Tank 5 (upper dome, barrel, lower dome) follow the requirements of API 653 for tank floors.

The following table displays the number of shell repairs that fall under the categories of weld repairs and patch plate repairs.

Table 1-1 Shell Repair Requirements Summary						
Repair Type No. of Repairs Linear Feet of Weld Area of Patch Plate (sq. ft.) No. of Patch Plates No. of Patch Plates No. of Patch Plates No.						
Weld Repairs	333	173				
Patch Plate Repairs	81		80	70	11	
Totals	414	173	80	70	11	

The two nozzles on Tank 5 passed the strength (pressure) and leak-tests at 225 psig with water. A full visual inspection was performed on the 32-inch nozzle (man entry) as well as a 100% PAUT inspection of the girth welds. The visual examinations performed on the 32-inch issue/receipt line revealed that the line will require some weld repairs to the internal welds but that pipe wall thickness was measured and found acceptable for the entire length of the pipe (indicates no backside corrosion). A pipe visual inspection camera was used to exam the 18-inch issue/receipt line. The camera examination of the 18-inch revealed multiple weld issues such as lack of fusion on the welds. Camera evaluation does not provide the same visual inspection capability that man entry into pipe provides because pipe wall thickness can only be verified at the accessible ends of the pipes which limits the information on possible backside corrosion. Based on limited camera examination capabilities and the inability to obtain pipe wall thickness reading for the entire lengths of the 18-inch pipe, EEI recommends the 18-inch pipe be taken out of service.

Additional mandatory repairs are described later in this report. Based on the findings during the inspection, repairs are required before returning Tank 5 back to service.

2.0 INSPECTION ASSESSMENT

A comprehensive table identifying tank features with findings and conclusions as appropriate is included as Attachment F. Attachment F also contains several tables with full reporting of data obtained. The following discussion only addresses key integrity issues.

The tank inspection revealed that mandatory repairs are required to return the tank to service. Mandatory Repairs are considered actions necessary to preserve or restore the structural and hydraulic integrity of the tank. This includes any condition which has or may breach the hydraulic or structural integrity of the tank prior to the next integrity inspection.

Hydraulic Integrity

Hydraulic integrity is the ability of the tank to hold product (until the next inspection) without compromising the boundaries of the floor, shell, and dome, and the piping to the first valve outside of the tank. The identified areas within the tank that affect the hydraulic integrity of the tank include the following:

- Previously ground areas where the remaining wall thickness was below the repair threshold.
- Backside corrosion over localized areas of the tank shell and upper dome.
- Multiple rounded or linear weld defects which could be less than recommended repair thickness.
- The condition of the circumferential welds on the 32-inch product line.

Structural Integrity

Structural integrity is the capability of the tank to remain freestanding, with or without product, under the conditions of its design basis. Structural attributes include the floor, shell, upper dome, and their attachments.

Inspection of the tank shell, bottom cone and floor, and the upper dome found no indications of damaged or deteriorated base structure of the tank. There were no other indications in the shell areas which may have indicated that there was an underlying structural issue with the tank.

A full tower inspection was performed by Hawaii Engineering Group (HEG). The inspection determined that the tower structure was suitable for continued service under the intended operating conditions once minor repairs were completed. Minor repairs included replacing missing bolts and tightening existing hardware.

Next Inspection

Based upon API 653 criteria, upon successful completion of mandatory repairs, Tank 5 must receive its next internal out of service inspection in 2038. The current tank shell liner corrosion assessment identified repairs that will result in a remaining metal thickness equal to or greater than 100 mil (one mil is one thousandth of an inch) at the next inspection. The 20-year interval is based on the date of the most recent corrosion scan, and not the return to service date.

3.0 INSPECTION METHODOLOGY

API 653 inspection criteria was followed in terms of procedure and evaluation to the greatest extent possible. Tank inspection included assessment of the upper dome, extension ring, under catwalk, entire

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course shells (barrel section), lower dome, floor appurtenances, access ways, and vents. All accessible interior surfaces of the upper and lower domes, floor, shell, and all welds were examined by one or more nondestructive testing (NDT) methods. NDT methods included:

- Electromagnetic Testing methods:
 - Low-Frequency Electromagnetic Testing (LFET) (utilized on liner plate surfaces)
 - Balanced Field Electromagnetic Testing (BFET) (utilized on liner plate welds)
- Ultrasonic Testing methods:
 - Straight-beam, Longitudinal Wave, Pulse-Echo Method (UT)
 - Phased Array Ultrasonic Testing (PAUT)
- Visual Testing (VT)
- Magnetic Particle Testing (MT)

TesTex Scanning

Initial inspection of Tank 5was performed by TesTex as a subcontractor to APTIM. The inspection can be broken down into three parts:

- Scanning 100% of accessible shell plates utilizing LFET technology
- Scanning 100% of accessible welds using BFET technology
- Visual inspection of accessible shell plates and welds

LFET was used to detect discontinuities caused by backside corrosion. While scanning the shell plates, technicians marked locations of discontinuities found using LFET. They then used UT to determine remaining wall thickness in the area. The threshold for remaining wall thickness was set as 200 mil and less.

BFET was used to detect surface and near surface discontinuities in the liner plate welds.

VT was performed to detect discontinuities in liner plate surfaces and welds. Discontinuities detected by VT were evaluated as porosity, undercut, lack-of-fusion, incomplete fill, dents, gouges, and bulges.

All relevant indications observed by TesTex were documented and provided to EEI for further investigation. Relevant indications were assigned unique identifiers for tracking purposes.

TesTex Personnel Qualifications

TesTex technicians performed a "blind" test consistent with API 653 Annex G requirements using the LFET equipment. Each technician scanned coated and uncoated test plates containing known defects. Discontinuity location was recorded and flaw characterization using UT was performed. All technicians passed the tests given to them. Test results are provided in Attachment K of this report.

EEI Prove-up (Flaw Characterization)

EEI provided an API 653 certified inspector during the Tank 5 inspection phase. During this time, the inspector reviewed all data provided by TesTex and performed a visual inspection of 100% of the accessible tank shell liner plates and welds. Prove-up of non-destructive examination (NDE) indications reported by TesTex was performed to verify the location and characterization of the indication and to collect any additional information required to provide a repair recommendation.

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Flaw characterization was performed to verify size, shape, location, and to verify interpretation (relevant, nonrelevant, or false) of each reported relevant indication. Repair recommendations were made when discontinuities were evaluated as defects.

For relevant indications associated with backside corrosion, flaw characterization was performed with PAUT. The PAUT transducers utilized were specifically designed to examine backside surfaces for corrosion damage. The areas of concern were scanned to determine the remaining wall thickness. Repairs were recommended for any area thinner than the repair threshold of 160 mil.

In areas where repairs were recommended due to backside corrosion, the surrounding areas of liner plate were also scanned to verify the area identified was correct and to determine the size of patch plate. Patch plates were designed to cover the entire defect as well as meet API 653 criteria for weld clearances and intersection requirements.

Discontinuities in welds identified by BFET were reported by TesTex and were inspected by EEI with MT to verify the extent of the discontinuity. During follow up investigations it was found that many of the discontinuities reported could be detected using VT. If the discontinuity was found visually and could be evaluated, no further inspection was performed. Weld repairs were designed and recorded for discontinuities evaluated as defects.

For all instances of backside corrosion, repairs were determined based on the repair threshold for remaining wall thickness. Many other repair recommendations were based on this same criterion, however, in some cases, exceptions occurred as described below.

Porosity and Undercut: Repairs were recommended for discontinuities where the bottom of the discontinuity was visually obscured or otherwise unable to be characterized. Areas lacking coating or where coating was present but damaged (peeling, blistering, or not tightly adhered) were also recommended for repair. Further discussion of discontinuities caused by rounded indications and acceptance criteria are provided in Attachment C.

Dents and Bulges: Repairs were recommended for discontinuities caused by sharp profile changes or creases that create a point of stress concentration. Repairs were not recommended for shallow, smooth profile discontinuities. The bulges reported by TesTex were found to have smooth transitions across the shell liner plate welds, were distributed uniformly around the tank, and presented with similar appearance (size and shape) in each shell course. It is thought that these features are artifacts of the original construction process.

Weld Defects: Both full penetration butt welds and fillet welds were evaluated. Common weld discontinuities that were identified in both types of welds included: porosity, undercut, lack of fusion, and incomplete fill. Discontinuity depth was evaluated where possible, that is, where the configuration of the defect or presence of coating did not significantly obscure the measurement. The criteria used to evaluate liner thickness was based on remaining thickness of the liner plate, as outlined in Attachment C. Locations called out for repair having porosity, incomplete fill, undercut, and other damage related to plate thickness did not meet the remaining thickness requirements for the required service interval.

In addition to the discontinuities reported by TesTex, EEI found defects based on the criteria and methods mentioned above. All relevant indication data (by both TesTex and EEI) were recorded for each plate and given a unique identifier locating the area relative to the lower left corner of the plate. A table of relevant indications and resulting defects is provided in Attachment F.

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API 653 Inspection

EEI performed a modified API 653 out-of-service inspection of Tank 5 in terms of procedure and evaluation to the greatest extent possible. The API 653 checklist was used to the extent of relevant content. The API 653 checklist was used to the extent of relevant content. The checklist is provided in Attachment A.

The nozzles at the top of the tank were visually inspected. The 24-inch vent line connects from the top of the tank to the ventilation system in the upper tunnel. An inspection of the vent line utilizing a motorized camera was performed because the majority of the line between the tank and upper tunnel is encased in concrete, which would otherwise limit visual inspection. The vent line is generally in good condition and no repairs to the vent line are recommended.

Tank 5 contains 32-inch and 18-inch product lines. These product lines were inspected via either direct or camera visual inspection. PAUT was performed in the 32-inch line. Internal pitting and weld quality were evaluated. The conditions of the lines were recorded in videos and photos.

Hansa Consult of North America, LLC (HCNA) performed a hydrostatic strength test of the 32-inch, 18-inch, and 18-inch casing tank nozzles. HCNA provided precision leak testing using a third-party certified procedure to test each of the lines from the tank. EEI provided quality assurance (QA) of the process. The HCNA test report has been included in Attachment J of this report.

Additional vacuum box and magnetic particle testing was performed on critical areas of Tank 5. Testing was done in accordance with API 653 specifications.

- Custom vacuum boxes were fabricated to examine 100% of the welds around the expansion joint, adjustment plate, strain gauge pipe cap covers, 8-inch drain cap, and center tower leg bases.
- Magnetic particle testing was utilized to inspect 100% of the strain gauge pipe cap covers as well as 50 expansion joint plug welds. Any indications that were found were recorded and a repair designated.

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4.0 INSPECTION FINDINGS

All instances of discontinuities resulting in relevant indications and recommended weld and patch plate repairs that were reported during the inspection phase are provided in Attachment F. Vacuum Box and MT test reports are provided in Attachment H. PAUT examination results are Provided in Attachment I.

Tank Nozzles

Visual inspection of the large bore product lines was conducted. The intent of the inspection was to provide condition information, quantify internal pitting, identify substandard girth welds, substantiate longitudinal weld conditions, identify backside corrosion (where possible), and establish geometric data for the inaccessible piping. The 32-inch line was physically accessed to look for pitting and to examine weld quality and suitability of prior repairs made by others. The 18-inch product line was not directly accessed. It was visually examined using remote video. To the greatest extent possible, the 18-inch and 32-inch nozzles were examined utilizing ultrasound techniques for presence of backside corrosion, and quality of girth and longitudinal manufacturing seams. Examination of the 18-inch line was limited to what can be accessed from each end of the line.

EEI has adopted the following numbering scheme for the purposes of locating pipe welds: girth weld numbering referenced in the following discussion starts at first flange outside the tank and increases toward the tank. Clock positions place 12 o'clock at the top of the pipe and 3 o'clock 90 degrees to the right when facing toward the tank.

The 32-inch line was inspected visually and with PAUT. Visual inspection of the 32-inch pipe found widely spaced pitting in the internal face of the pipe wall between Girth Welds 3 and 5. The pitting extended from the 5 o'clock to 7 o'clock positions. However, pit depths were shallow and did not require repair. PAUT was utilized to inspect 100% of the girth welds inside the pipe. Girth Weld 2 contained 7 inches of weld defects requiring repair. Girth Weld 3 contained 3 inches of weld defects requiring repair. Girth Weld 4 contained 14 inches of weld defects requiring repair. No indications were found in Girth Welds 5, 6, and 7. Defects found with PAUT included lack of fusion and linear indications.

The 18-inch product line was inspected with a remote video unit. Inspection of the 18-inch pipe found the following: Girth Welds 1 and 2 contained underfilled welds that would require repair. Since weld repair is not possible inside this line it is recommended to abandon the line. It should be noted that the recommendation to remove this line from service was based on visual evaluation of welds, as there was no remaining pipe wall thickness data collected for the line. An inline intelligent inspection tool (smart pig) was not run in the line to develop pipe wall information.

The 18-inch line and 32-inch line were hydrostatically tested by HCNA. Precision temperature compensated tests at 225 psig pressure for four-hour duration were performed. This strength test was chosen over specified 162.5 psig eight-hour duration test specified in scope of work because it provides more meaningful test parameters. In addition, a leak detection test in accordance with National Work Group on Leak Detection Evaluations (NWGLDE) was performed. Both lines passed the strength and leak tests. A test report for this examination is provided in Attachment J.

Tank Interior

Two types of welds were evaluated in relation to the hydraulic boundary of the tank. Full penetration butt welds connect the shell plates to each other to form the continuous steel liner. Penetrations through the liner (nozzles, for example) and insert plates are also welded to the liner with a full thickness weld. Fillet welds were utilized as the final interior seal between nozzle penetrations and patch plates to the interior

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liner. The original construction of the tank called for the liner plates of the upper dome to be joined by a full penetration butt weld with a backing bar located on the inside of the tank. The backing bars were subsequently fillet welded to the liner plates. While the full penetration butt weld would normally represent the hydraulic boundary of the liner, the configuration of the joint with a backing bar prohibits an examination of the weld from the inside of the tank. For this reason, the fillet weld joining the backing bars to the liner plates was evaluated as if it were a hydraulic boundary. This approach is conservative in that a breach in the fillet weld does not necessarily confirm a path through the liner of the tank.

Table 4-1 Tank Repairs by Area Summary							
Category	Basis for Percentage (Tank or Region)		Percentage (Tank		Barrel	Extension Ring	Upper Dome
	Tank	Region					
Percent of total relevant indications reported for assessment in Tank 5	х		3%	26%	10%	61%	
Percent of relevant indications that required repair (defects)		Х	86%	83%	68%	47%	
Percent of the total repairs recommended in Tank 5	х		4%	36%	12%	48%	
Percent of repairs due to backside corrosion in given area (lower dome, extension ring, upper dome or barrel)		х	0%	4.6%	34%	18.7%	

Lower Dome

The lower dome of Tank 5 was inspected using LFET, BFET, and visual techniques. Inspection of the lower dome identified 3% of the reportable indications in the tank. Flaw characterization resulted in 86% of the reported indications meeting repair criteria (defects), accounting for 4% of the total repairs in the tank. No defects due to backside corrosion were found in the lower dome. The repairs consist of weld and patch plates. See Attachment F for repair quantities in lower dome.

Vacuum Box testing was performed on the four center tower legs. Custom vacuum boxes were fabricated to fit the floor to leg welds. No relevant indications were found from the inspection. The 8-inch drain (slop) line cover plate was inspected by visual, vacuum box, and magnetic particle methods to verify the integrity of the seal welds. Defects were found that require repair by welding.

EEI also performed visual coating inspection and hammer testing on the floor of Tank 5. The coating was in good condition at the time of inspection. The hammer testing results were inconclusive. The test was very subjective but there appeared to be some hollow-sounding spots around the nozzles. Follow up ultrasonic thicknesses of the "hollow" areas surrounding the nozzles did not reveal any corrosion in these areas.

Barrel

Tank 5 barrel was inspected using LFET, BFET, and visual techniques. Inspection of the barrel plates identified 26% of the relevant indications in the tank. Flaw characterization resulted in 83% of the relevant indications meeting repair criteria (defects), accounting for 36% of all repairs in the tank. Repair methods include weld and patch plate repair. Approximately 4.6% of repairs are areas of backside corrosion. See Attachment F for locations and quantities.

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH EEI Project No.: 8877 Page 8 November 2019 EEI inspected the existing strain gauge nozzles. These nozzles are approximately 3-inch diameter and extend 3 inches from the tank shell. Vacuum Box and Magnetic Particle testing was performed for this inspection. No relevant indications were found.

Extension Ring

Tank 5 extension ring was inspected using LFET, BFET, and visual techniques. Inspection of the extension ring identified 10% of the relevant indications in the tank. Flaw characterization resulted in 68% of the indications requiring repair (defects), accounting for 12% of all repairs in the tank. The repairs consist of weld, patch plates, and pipe cap repairs. Approximately 34% of repairs are areas of backside corrosion. See Attachment F for repair quantities in upper dome.

Plug welds located on the upper and lower expansion joint ribs were inspected with magnetic particle methods. One hundred percent of the upper and lower expansion joint rib welds were leak tested using vacuum box apparatus.

The MT of the plug welds resulted in one required repair.

Vacuum Box testing of the expansion joint and adjustment plate welds produced no relevant indications.

Upper Dome

Tank 5 upper dome was inspected using LFET, BFET, and visual techniques. Inspection of the upper dome identified 61% of the relevant indications in the tank. Flaw characterization resulted in 47% of these indications requiring repair (defects), accounting for 48% of the repairs in the tank. The repairs consist of weld, and patch plate repairs. Approximately 18.7% of repairs are areas of backside corrosion. See Attachment F for repair quantities in upper dome.

Other Items of Concern

Product and/or water entrapment areas that can support corrosion were found. This occurred where the support brackets for sampling lines are not seal welded to the floor and at a section of an old stilling well that remains welded to the floor. All support brackets are recommended to be seal welded to prevent fuel from entering this area where direct inspection is not possible. The piece of old stilling well should be removed and a patch plate welded over the area.

There is minor damage to the lower dome coating in Tank 5. It is recommended to perform repairs to the coating at the bottom of the tank.

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5.0 REPAIR ITEMS

Based upon the API field inspection, engineering judgment, and knowledge of funding practices, repairs developed are listed below in the following tables as required (mandatory), non-mandatory and recommended for long term serviceability. Refer to Attachment B, "Assessment of Compliance with Military Criteria" for comprehensive comments and recommendations of the tank's compliance with military criteria.

Standard of Care

All repairs must meet the requirements of API 650 and API 653 regarding material, welding procedures, qualification of welders, and weld NDE and testing requirements. Obtaining hot work permits and developing the appropriate hot work procedure for the tank floor is the responsibility of the repair contractor and must consider that the tank has been in petroleum fuel service.

Mandatory Repairs

	Table 5-1 Mandatory Repairs					
	Finding	Repair	Photo			
	andatory repairs are repairs that are critica e tank to service.	l to the hydraulic and structural integr	rity of the tank and are required to return			
1.	Defects found requiring patch plate repairs are: Backside Corrosion Dents	Provide patch plate repairs. Plate size, location in tank, and overall quantities can be found in Attachment F.	AT MY			
2.	Thinning of 3-inch pipe caps covering the existing grout pipe and strain gauge at 5 locations was found in the extension ring.	Remove existing 3-inch pipe caps and provide patch plates. See Attachment F for quantity and locations				

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	Table 5-1 Mandatory Repairs						
	Finding	Repair	Photo				
3.	Defects found requiring weld repairs are: Weld Indications Porosity/Rounded Indications Lack of Fusion Insufficient Fill Gouges Undercut Other shell topside indications	Provide weld to repair defects. Weld length, location in tank, and overall quantities can be found in Attachment F.					
4.	The 8-inch drain line cover plate had 4 linear weld defects. The defects were found at the 3, 4, 6 and 10 o'clock positions and were approximately 1/8-inch in length.	Grind out defects and provide weld repair.					

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	Та	ble 5-1 Mandatory Repair	S
	Finding	Repair	Photo
5.	The 32-inch product line contains 10 linear weld defects throughout the line in its girth welds.	Grind out defects and provide weld repair.	

Non-Mandatory Repairs

	Table 5-2 Non-Mandatory Repairs					
	Finding	Repair	Photo			
	e repairs listed below are not mandatory p rformed if approved by the Government fo					
1.	Approximately 6 inches of the old stilling well is still welded to the floor.	Cut off the old stilling well flush with the tank floor and provide a 6-inch patch plate over the location.				
2.	The 18-inch tank product line passed strength and leak tightness tests, but the pipe wall thickness could not be evaluated for the entire pipe length. Welds could only be examined using a camera.	Remove 18-inch line from service. Modify piping in lower tunnel to reconnect tank 32-inch line to tunnel 18-inch line. Provide half-inch closure plate inside tank to isolate 18-inch tank line from tank				
3.	The steel channel supports for the drain line and sample piping are not welded to the tank all the way around the support. This allows product to fill under this area and is not accessible to inspect.	Seal weld all supports to the tank.	DESERVETY.			

Repairs for Long Term Serviceability

	Table 5-3 Repairs For Long Term Serviceability						
	Finding	Repair	Photo				
1.	The grout nozzles and strain gauges are covered by 3-inch pipe caps instead of ½-inch patch plates as noted on design drawings.	Remove pipe caps and provide patch plates to cover all locations. Location in tank, and overall quantities can be found in Attachment F.					

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH EEI Project No.: 8877 Page 13 November 2019

	Table 5-3 Repairs For Long Term Serviceability						
	Finding	Repair	Photo				
2.	The inside of the 32-inch line is not currently coated.	Once the 32-inch line is repaired, coat the inside of the line with Polysulfide modified Epoxy Novolac coating system used for lower dome coating. By doing so the line will be subject to less corrosion potential.					

Shell Repairs - General

Generally, welding repairs require surface preparation followed by welding of a tank seam or placement of a patch plate depending on the nature of the defect being repaired. Repairs by welding that involve the placement of a patch plate are further divided into two categories based on the patch size. Patches of a surface area of 2 square feet or less can be manipulated by hand utilizing the existing means of tank shell access. It is important to note that patch plates larger than 2 square feet will require additional consideration to both the means of moving and positioning the patch in place prior to welding and may also require further considerations regarding attachment to the underlying tank structure.

Instances of multiple defects in close proximity to each other that were reported and verified individually in the inspection process are combined into a single repair at some locations. This grouping of individual defects into single repairs is necessary to facilitate weld spacing requirements. The grouping of defects into a single repair may also provide a considerable time and material savings over addressing each indication separately. The approach for repair types are discussed below.

The overall repair methodology utilized in the determinations of repairs are outlined in API 653 and were utilized to the greatest extent possible.

Defects Caused by Rounded Indications

The recommended repair for these areas is to grind the affected area and apply a weld bead (or beads) to replace the deficient weld. Individual instances of porosity may be addressed by as little as 2 to 4 inches of weld repair while larger areas with numerous indications requiring several inches or more of repair.

Defects Caused by Dents, Gouges, Tear-Outs and Dent/Gouge Combinations

Repairs associated with these defects will be addressed with one of two methods depending on the severity and size of the defect. Tear-outs from the removal of temporary welds in the manufacture of the tank (or later) are typically repaired by filling the affected area with weld and then grinding the welded area to a flush condition with the surrounding plate. It is anticipated that these areas will require relatively short lengths of weld to correct the underlying discontinuity. The recommended repair for dents, gouges, and dent/gouge combinations is to apply a patch plate over the affected area and seal weld the patch to the surrounding plate with a multiple-pass fillet weld.

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BFET Indications

When the lateral extent of the defect could be seen, relevant indications identified by BFET methods were characterized by visual methods. BFET indications of discontinuities that were not easily characterized by visual methods were added to the repair list without further inspection. It was determined that further inspecting the weld requires a greater effort to definitively examine and characterize than would be required to provide a repair. These efforts include coating removal and grinding prior to evaluation. A typical repair involves preparation of the affected area by grinding followed by re-welding.

Local Backside Corrosion

Localized backside corrosion limited to an area that can be repaired with a smaller sized patch plate and is discussed within this section.

The recommended repair is the placement of a lap patch sized sufficiently to overlap affected area by at least 2 inches in all directions. In some instances, this overlap spacing requirement is not attainable within a single shell plate while maintaining weld-to-weld spacing requirements per the requirements outlined in API 653 for floor plate patch repairs. There are varied approaches that are recommended based on the situation.

In the presence of significant thickness loss in close proximity to a butt-welded seam, the patch is forced to extend onto the adjacent plate. In this case, the weld spacing requirements API 653 for lap patches on floors have been adopted.

When the patch plate is near or abuts a backing bar (a flat steel bar installed on the tank exterior, or the backside of the weld), the recommendation is to provide a tombstone shaped patch plate with sides of the plate intersecting the backing bar fillet weld at approximately 90 degrees. The size of the patch plate will influence the method by which it is positioned for welding.

General Backside Corrosion

General backside corrosion is such that the area affected is much larger than a localized corrosion area and requires a repair that is larger in size. Within Tank 5, there are approximately 37 repairs that fall under this category, and it is recommended to repair an area greater than 2 square feet in area for each location. Several of these repairs are full plate replacement repairs.

These repairs will be unlike any previous repairs done at the Red Hill Facility and will require extensive design and construction considerations. Repairs could include the removal of existing shell plates and inserting new plate or welding patch plates to cover the affected areas.

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6.0 COATING SYSTEM

Coating Requirements

EEI surveyed the floor coating condition and found the coating to be acceptable. Under a separate contract, APTIM is responsible for obtaining the services of an SSPC QP-5 certified firm, to provide a NACE Level 3 Coating Inspector to perform a coating condition survey. Results of this survey will be utilized to determine coating repair requirements.

7.0 SUITABILITY FOR SERVICE EVALUATION

Historical Inspection Information

Previous inspection reports were available for review. Past repair documentation includes:

- Willbros Government Services, LLC (WGS) Tank Inspection & Integrity Report dated November 22, 2010.
- WGS Warranty Repair & NDE Inspection Certification Report dated September 15, 2016.

Corrosion Rates

Corrosion rates were calculated per plate and full results are in Attachment G. Each rate is based on UT data collected in the field. The maximum corrosion rates for a single plate found in each tank section are as follows:

Upper Dome: 1.789 mils per year Extension Ring: 1.842 mils per year Barrel: 1.724 mils per year Lower Dome: 0.658 mils per year

Floor: Negligible – Plate thickness is within mill tolerance

The corrosion rates were calculated using an assumed original metal thickness of 250 mil, the remaining wall thickness and 75 years in service (1942 construction). The numbers listed above are the largest corrosion rate in each area. Please note that remaining wall thickness may have been a result of excessive grinding within the tank instead of corrosion. Utilizing these areas to calculate corrosion rate provides the most conservative rate calculation.

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8.0 CLOSURE

Conclusions

Mandatory repairs were identified that need to be performed prior to return-to-service. Pending completion of the mandatory repair items noted, Tank 5 will be suitable to return to service.

The repairs to Tank 5 primarily include weld and patch plate repairs. The patch plate repair designs should account for the grinding and removal of material which were completed by previous contractor.

Project Organization

Prime Contractor Enterprise Engineering, Inc.
Tank Inspection Enterprise Engineering, Inc.

Tank Scanning TesTex, Inc.

Pressure Testing Hansa Consult North America, LLC Coating Assessment FeO, Inc. (under separate contract)

Electrical Assessment BSE Engineering

Mechanical Services APTIM

EEI Project Team

Site Team

Doug J. Kieley, P.E. Project Manager, Inspector of Record

API 653 AST Inspector Certificate No. 40281 API 570 Piping Inspector Certificate No. 23161

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API 653 AST Inspector Certificate No. 40225 API 570 Piping Inspector Certificate No. 41177

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Tank 5 – API 653 Inspection

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Support Team

Stephen S. Brooks, P.E. Principal-in-Charge/ QA Review

API 653 AST Inspector Certificate No. 17 API 570 Piping Inspector No. 23663

Steve J. DiGregorio, P.E. Chief Structural Engineer,

API 653 AST Inspector Certificate No. 1113

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ATTACHMENT A TANK INSPECTION DATA SHEET AND EVALUATION ITEMS

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DLA ENERGY TANK CMP CONDITION FORM

TANK INSPECTION SUMMARY SHEET

Tank Location (Site Code): Red Hill Fuel Storage Facility, NAVSUP FLC, Joint Base Pearl Harbor-

Hickam, Hawaii (JBPHH)

Tank No.: 5
Facility No.: N/A

Inspection Date(s): October 2017 to January 2018
Tank Type: Mined Underground Storage Tank

Type of Inspection: Internal w/ Suitability for Service Evaluation

Contract Number, Task Order: N38430-15-D-1678, Task Order 0011

Prime Contractor Name: Enterprise Engineering, Inc.

400 US Route 1, North Suite B

Falmouth, ME 04105

(207) 869-8006 Inspector, Certificate No: Douglas J. Kieley, P.E.

API-653 AST Inspector Certificate No. 40281

Inspection Company: Enterprise Engineering, Inc.

400 US Route 1, North Suite B

Falmouth, ME 04105 (207) 869-8006

Manufacturer, Date, Design Standard Morrison Knudsen, 1942, Not Specified

Diameter: 100'-0"
Shell Height: 250'-6"
Product, Specific Gravity: JP-5, 0.82

Design Pressure / Temperature: 96.9 psi / 50 degrees F

Gross Capacity / Nominal Capacity: 300,000 Bbls

Safe Fill Height: Top of Shell Course A in the Upper Dome

GPS Latitude & Longitude: 8 Deg 43′ 38.04″ N, 167 Deg 44′ 15.57″ E (Source – Google Earth) **Foundation Configuration:** Concrete / Gunite encasement with embedded rebar & I-beams

Shell Configuration: Upper Dome: 5 courses, Butt Welded w/ Backing Bars

Extension Ring: 4 courses, Butt Welded w/ Backing Bars Barrel: 28 courses, Butt Welded

Lower Dome: 4 Courses, Butt Welded

Roof: Dome with Structural Steel

Floating Pan: Not Applicable
Cathodic Protection: None – Not Applicable
Stilling Wells: None, 6-inch ATG

Last Inspection (Type, Date): Out-of-Service, September 2010 by Wilbros Government Services, LLC

Last Coated Internally (Product): 1983 (Lower Dome only re-coated in 2010)

Last Coated Externally (Product): Not coated Externally

INSPECTION RESULTS

Can tank return to service?: No.

Deficiencies identified as mandatory repairs: Yes, see paragraph titled "Mandatory Repairs" in body of report

Deficiencies identified as recommended repairs: Yes, see paragraph titled "Non-Mandatory Repairs" in body of report.

Deficiencies identified as long term repairs: Yes, see paragraph titled "Long Term Repairs" in body of report.

Next Scheduled API Inspections (Type, Date): API 653 Out-of-Service: 2038 (20 Years)

Next Scheduled Tank Cleaning (UFC 3-460-03, 2016): Army, Navy, Marine Corps Tank (During OOS Inspection Unless

Required More Frequently due to Potential Fuel Quality Issues):

January 2038 Date

ADDITIONAL ITEMS

Change in Service: None As-Built Drawings, Specifications: Yes

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC JBPHH

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ATTACHMENT A, Tank Summary Sheet

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ATTACHMENT B ASSESSMENT OF COMPLIANCE WITH MILITARY CRITERIA

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ASSESSMENT OF COMPLIANCE WITH MILITARY CRITERIA

UFC 3-460-01, Table 8-1

(Complete UFC available at www.wbdg.org)

Requirements for Vertical Underground Storage Tank (V-U) Only

ITEM	APPURTENANCE (UFC REQUIREMENT)	COMP	NO	COMMENTS/RECOMMENDATION (A blank in comments column indicates UFC compliance)			
MANH	MANHOLE						
а	A 30-inch diameter manhole, a minimum of one manhole for tanks between 1,000 gallons and 5,000 gallons capacity, and a minimum of two manholes (both are to be at least 36 inches), for tanks larger than 5,000 gallons capacity.		х	Tank is equipped with one 24-inch and 8 foot manhole at the Upper Tunnel level and one 30-inch manhole on top of the tank. It is not compelling to provide 36-inch manholes.			
LADDE	R/STAIRS						
i	Internal ladders (in accordance with OSHA criteria) for tanks of 5,000 gallons or larger with floating pans.	Х		Internal ladder in good condition and compliant from bottom of tank to the top inside center tower.			
LEVEL	ALARMS						
Ī	An individual automatic level alarm system, independent of the gauging device or system for each tank. Include high, high-high, low and low-low level alarms.	Х		Tank contains high level and high-high level alarms which alarm separate from ATG system. The remainder of the Alarms are compliant with NAVSUP requirements for the Red Hill Facility.			
VENTS							
m	Open atmospheric vents with weather hoods and bird screens or pressure/vacuum vents in lieu of open vents. Comply with NFPA 30, host nation requirements, Chapter 2 of this UFC, API Std 650, API Std 2000, 29 CFR Part 1910.106, and DoD Standard Design AW 78-24-27, where applicable.	Х		Tank contains a single 24-inch spiral welded vent line from the top of the tank to the Upper Tunnel Vent spool. The remaining portions of the requirements are not applicable to Red Hill Tanks.			
n	Emergency relief venting with capacity in accordance with NFPA 30 and UL 142, as applicable or a weak roof-to-shell seam, as specified in API Std 650.	Х		No emergency relief venting required for Red Hill Tanks.			
GAUGE	/ /GAUGE HATCH/STILLING WELLS						
o	A liquid level gauge calibrated in 1/16-inch graduations mounted at 60 inches above the walking surface.	х		Tank is outfitted with an ATG system on the top of the tank.			
р	Automatic Tank Gauging (ATG) for all tanks with fuel managed through the Defense Logistics Agency's Business Modernization (BSM Enterprise Resource Programs (ERP) - Fuels section), that complies with API MPMS Chapter 3.	Х		Tank is outfitted with an ATG system on the top of the tank.			
q	A 4-inch gauge hatch with drop tube to within 3 inches of the bottom of the tank (lowest point in the tank, not the sump). A second 4-inch opening without a drop tube or gauge hatch.	х		Tank does contain a gauge hatch, but does not have a drop tube. Tank is compliant with NAVSUP requirements.			

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH

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ATTACHMENT B, Page 1

ASSESSMENT OF COMPLIANCE WITH MILITARY CRITERIA

UFC 3-460-01, Table 8-1

(Complete UFC available at www.wbdg.org)

Requirements for Vertical Underground Storage Tank (V-U) Only

	APPURTENANCE	сомр	LIANT	COMMENTS/RECOMMENDATION
ITEM	(UFC REQUIREMENT)	YES	NO	(A blank in comments column indicates UFC compliance)
r	One 10-inch roof flanged nozzle with an 8-inch aluminum, fully slotted, stilling well for ATG near the edge of the roof near the top of the stairway platform.	Х		A 6-inch Aluminum ATG system probe is mounted on a 10-inch nozzle. Tank is compliant with NAVSUP requirements.
S	One 8-inch roof flanged nozzle with a 6-inch aluminum, fully slotted, stilling well for temperature and water bottom sensor, as close to or in the tank sump as possible. See DoD Standard Design AW 78-24-27.	х		There is no separate stilling well for temperature and water bottom sensor. Tank is compliant with NAVSUP requirements.
t	One 10-inch roof nozzle and an aluminum, slotted stilling well extended to within 3 inches of the bottom of the tank* for gauging and sampling. A datum plate to establish a gauging zero point.	х		There is no stilling well for manual tank gauging. Tank is compliant with NAVSUP requirements.
PIPE CO	DNNECTION			
w	Inlet fill pipe with horizontal exit perpendicular to a tank radial. Discharge is approximately 4 inches above tank floor and enlarged to reduce fuel velocity. An inverted trap is placed in the line to serve as a liquid lock to prevent entry of fire or an explosion from outside the fill pipe.		X	32-inch pipe exits perpendicular to tank floor. 18-inch pipe exits perpendicular to tank radial at 2 feet above tank floor. No trap is placed in line. Design is Standard for Red Hill Tanks.
OVERF	ILL PROTECTION			
х	Overfill protection with a hydraulically operated diaphragm control valve.		Х	Not applicable to Red Hill Tanks.
WATER	R DRAW-OFF			
dd	A central sump pump.	Х		Tank is equipped with a 4-inch drain in center of tank. Drain line rises 10 feet to new 20-inch tank penetration pipe.
STRIKE	R PLATES			
gg	Striker plates under all openings used for manual gauging in steel tanks and all openings in fiberglass tanks.	х		No striker plate installed in Tank 5.
Additio	nal Military Criteria Items, Comments or Notes:			
None.				

END OF DATA

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH

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ATTACHMENT B, Page 2

ATTACHMENT C NON-DESTRUCTIVE EXAMINATION (NDE) AND EVALUATION CRITERIA

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OUT-OF-SERVICE INSPECTION

CODES AND STANDARDS

API Standard 653, 5th Edition, November 2014

API Standard 650, 12th Edition, March 2013, Addendum 2, January 2016

UFC 3-301-01 Structural Engineering, September 2016

NON DESTRUCTIVE EXAMINATION (NDE)

Tank Inspection (General)

API Standard 653 as applicable.

Visual Inspection

- 1. Inspection Items
 - In accordance with API Standard 653 and EEI STD for API 653 Out-of-Service Inspection
 - Floor, shell and upper dome welded joints (where accessible).
 - Floor, shell and upper dome surfaces.
 - Items affecting structural and hydraulic integrity

2. Method

- In accordance with API Standard 653.
- Special considerations for rounded indications:

Rounded indications are defined as surface-penetrating discontinuities whose length is less than three times the width. Rounded indications in existing work are subject to further examination when they are obscured by coating and/or debris or if, for any reason, the full extent of the included surface is obscured. Cleaning the area of interest to bare metal is performed prior to reevaluation of the indication. Removal of coating, serves multiple purposes, such as:

- Length and width can be accurately measured without the inclusion of an unknown coating thickness;
- False positive indications caused solely by coating defect can be easily evaluated;
- Other forms of indication or defect (slag inclusions, for example) can often be hidden by coating and cause the appearance of rounded indications in the coating.
- Remaining thickness-based criteria for evaluation of indications.

It is common practice to only bring historically constructed and service-tested equipment into compliance with current code when repair, upgrade or other new construction is performed. For this reason, criteria presented here for surface penetrating (but non-crack forming) indications that have a length component in the through-thickness direction are based on the calculated minimum remaining wall thickness. It is the goal of this criteria to identify and reject any

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH

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ATTACHMENT C, Page 1

discontinuity that penetrates the steel to a depth such that the remaining wall thickness is thinner than the calculated minimum based on the calculations presented in Attachment G.

3. Acceptance Criteria

Acceptance criteria are from the applicable clause in AWS D1.1 and section in API 650:

Indication Type	Acceptance Criteria
Crack	Unacceptable, regardless of size or location
Weld/Base Metal Fusion	Complete fusion shall exist between adjacent layers of weld metal and between weld metal and base metal.
Crater Cross Section	All craters shall be filled to provide the specified weld size, except for the ends of intermittent fillet welds outside of their effective length.
Weld Profiles	Must confirm to AWS D1.1 Subclause 5.23
Undersize Welds	The size of a fillet weld in any continuous weld may be less than the %-inch nominal size without correction by 3/32-inch. In all cases, the undersize portion of the weld shall not exceed 10% of the weld length.
Undercut	For existing welds (welds that have previously been in-service) the acceptance criteria for depth of undercut will be based on remaining wall thickness criteria, as calculated in Attachment G.
Porosity, Rounded Indications	Piping shall have no visible porosity. For all other welds porosity shall not exceed 1 indication in 4 inches and the maximum diameter shall not exceed 3/32-inch. In addition, acceptance criteria for depth of the discontinuity will be based on remaining wall thickness criteria, as calculated in Attachment G.

Ultrasonic Testing (UT)

Ultrasonic thickness measurements were taken to establish end of nozzle and floor plate thicknesses.

- 1. Inspection Items
 - In accordance with EEI NDE Procedure, EEI-UT-002, Ultrasonic Thickness Examination.
 - Floor plates
 - End of nozzles
- 2. Equipment
 - Olympus 38DL Plus / Olympus 45 MG
- 3. Method
 - Perform on a spot basis to determine thickness.
 - \bullet $\;$ Perform as follow-up to LFET indications to determine the remaining wall thickness.
- 4. Acceptance Criteria

Planar indications such as laminations shall be reported to the inspector of record for further review.

ATTACHMENT C, Page 2

Dual Linear Phased Array UT

Quantitative assessment of the tank shell and floor.

- 1. Inspection Items
 - In accordance with EEI NDE Procedure, EEI-PAUT-001, Ultrasonic Thickness Examination.
 - Shell plates
 - Upper dome plates
 - Floor plates (to prove up any findings from the LFET)
- 2. Equipment
 - Olympus OmniScan SX with 7.5 MHz Dual Linear Array Probe for corrosion inspection.
- 3. Method
 - Perform at follow-up to LFET indications found by TesTex to determine the nature of the indication.
 - Echo/Echo (E/E) or Thru Coat mode for determining metal thickness and backside corrosion on coated surfaces without including thickness of coating in reading.
- 4. Acceptance Criteria

Planar indications such as laminations shall be reported to the inspector of record for further review.

Phased Array UT

Quantitative assessment of welds.

- 1. Inspection Items
 - In accordance with EEI NDE Procedure, EEI-PAUT-002.
 - Circumferential welds of the 32-inch piping.
- 2. Equipment
 - Olympus OmniScan SX with 5MHz angle beam probe.
- 3. Method
 - Perform double-sided angle beam inspections of circumferential welds according to established scan plans developed for addressing the piping thickness and weld orientation.
- 4. Acceptance Criteria
 - ASME B31.3
 - A linear-type discontinuity is unacceptable if the amplitude of the indication exceeds the reference level and its length exceeds ¼ in. for pipe thickness less than or equal to ¾ in.

Low Frequency Electromagnetic Technique (LFET)

- 1. Inspection Items
 - In accordance with TesTex Inspection Procedure.

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2. Equipment

FALCON S (8-Channel), 18.10 KHz

The equipment utilizes magnetizing core that acts as a DC electromagnet to generate a strong magnetic field. The saturation lowers the permeability of the ferromagnetic material which allows the Eddy Current field to penetrate deeper into the material being tested. Any wall loss will result in a concentration of the magnetic field in the remaining wall, resulting in an increased magnetic flux density around and under the defect. The distortion of the magnetic field is measured as a change of phase and amplitude in the secondary voltage generated by the material. The signal amplitude of the defect indication is in direct proportion to the volume of the defect. The signal phase of the defect indication is used to differentiate top side or bottom side defects

3. Detection Capability

The equipment is calibrated on a 1/4-inch thick function test plate with three machined metal loss defects:

- 1/8-inch diameter hole in 1/4-inch thick plate
- A tapered hole drilled 40% backside metal loss of plate thickness on surface opposite the detection equipment
- A machined notch across the width of the function test plate

Any signal that can be clearly distinguished from background noise during floor scanning is marked for follow-up testing by ultrasonic A-Scan.

4. Acceptance Criteria

- Indication Full screen LED display in "red" zone requires follow-up ultrasonic testing to determine nature of the indication.
- 5. Areas Not Accessible to Scanning
 - Within 1-inch of tank shell
 - Within 1-inch of welded joints
 - Floor areas below interior piping and appurtenances where the equipment cannot fit
 - Sumps
 - Below column bases and pipe supports
 - Patch plates

Balanced Field Electromagnetic Technique (LFET)

- 1. Inspection Items
 - In accordance with TesTex Inspection Procedure.
- 2. Equipment
 - FALCON S (8-Channel), 18.10 KHz
 - Hawkeye probe

The Hawkeye probe creates a balanced field in which small changes in the electromagnetic field can be detected by reducing the noise through phase rotation of the horizontal and vertical component of the signal. This allows the Hawkeye probe to detect surface and subsurface cracking.

- 3. Detection Capability
 - The equipment is calibrated to TesTex standards.
- 4. Acceptance Criteria
 - Indication The flaw will appear as a differential signal

Pit Survey

- 1. Inspection Items
 - Tank floor
 - Tank shell
 - Tank Upper Dome
- 2. Equipment
 - Mechanical pit gauges

Magnetic Particle Testing (MT)

- 1. Inspection items
 - In accordance with EEI NDE Procedure, EEI-NDE-001
 - Mitered welds in the 32-inch
 - 8-inch drain cap
 - TesTex weld BFET indications
 - Plug welds in the adjustment plate and expansion joint
 - Strain gauges
- 2. Equipment
 - Magnaflux Y-1

The Magnaflux Y-1 is AC electromagnetic yoke.

3. Method

- The application of wet visible or fluorescent particles shall be by spraying or flowing the medium under the continuous magnetization technique; i.e., the magnetizing current remains on while the examination medium is being applied and while excess of the examination medium is being removed.
- At least two separate examinations shall be carried out at each location. During the second examination, the lines of magnetic flux shall be approximately perpendicular to those used during the first examination.

4. Acceptance Criteria

All surfaces to be examined shall be free of:

- Relevant linear indications;
- Relevant rounded indications greater than 3/16-inch;
- Four or more relevant rounded indications in a line separated by 3/16-inch or less, edge to edge.

Vacuum Box Testing (VBT)

- 1. Inspection Items
 - 8-inch drain cap
 - Strain gauges
 - Adjustment plate welds
 - Expansion joint welds
 - Tower leg welds

2. Equipment

• Custom vacuum boxes built in situ for different welds.

3. Method

- The application of a soap film solution is applied in accordance with API 650.
- Initial pressure of between 21 and 35 kPa in which the vacuum is formed.
- Increase and test under 56 to 70 kPa
- 4. Acceptance Criteria
 - Indications The continuous formation or growth of bubbles produced by air passing through the thickness is a through thickness leak indication. A large opening leak is indicated by the quick bursting bubbles or spitting response at initial pressure of vacuum.

Coating Thickness Measurements

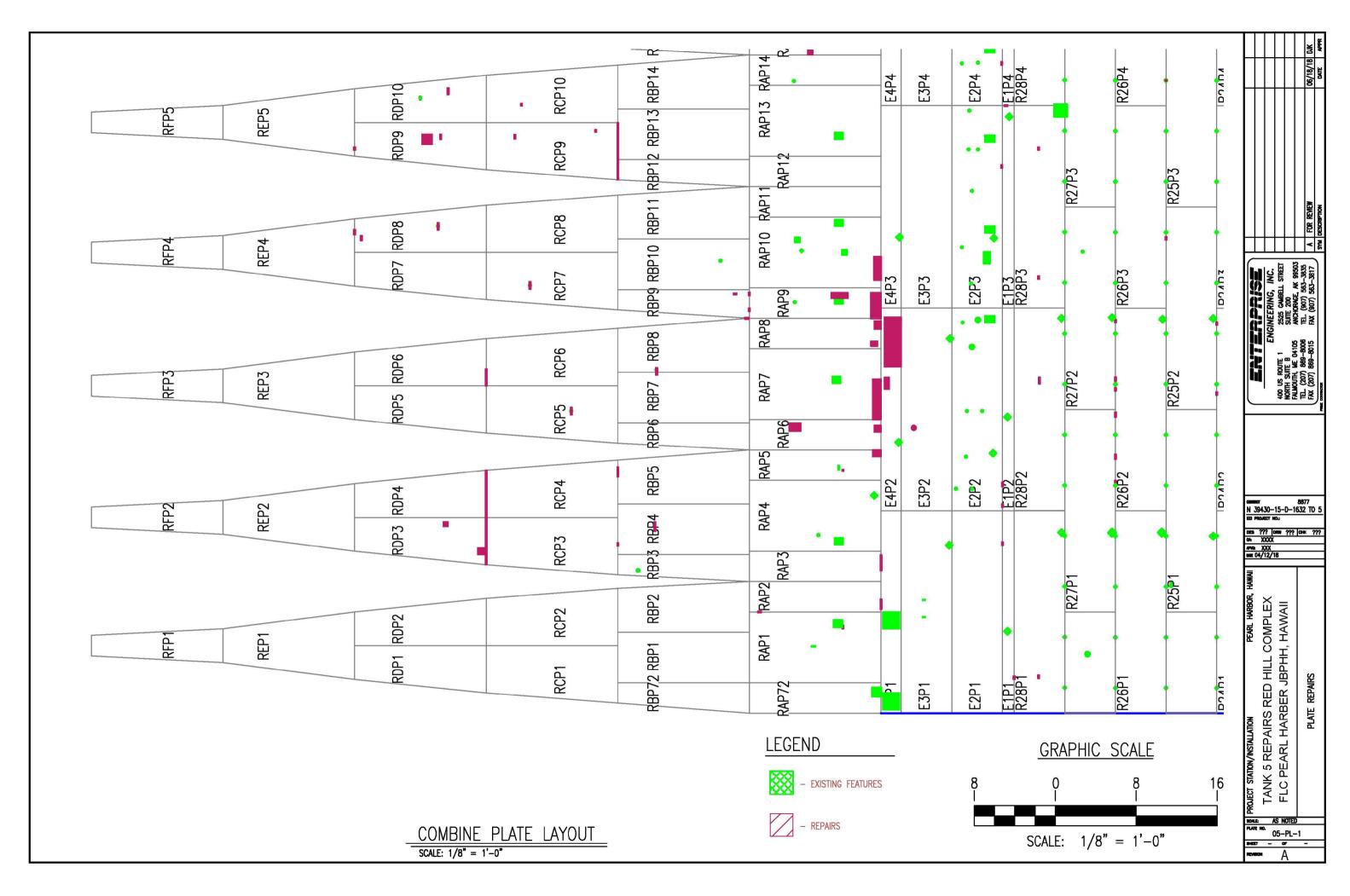
- 1. Equipment
 - PosiTector 6000 Thickness Gauge

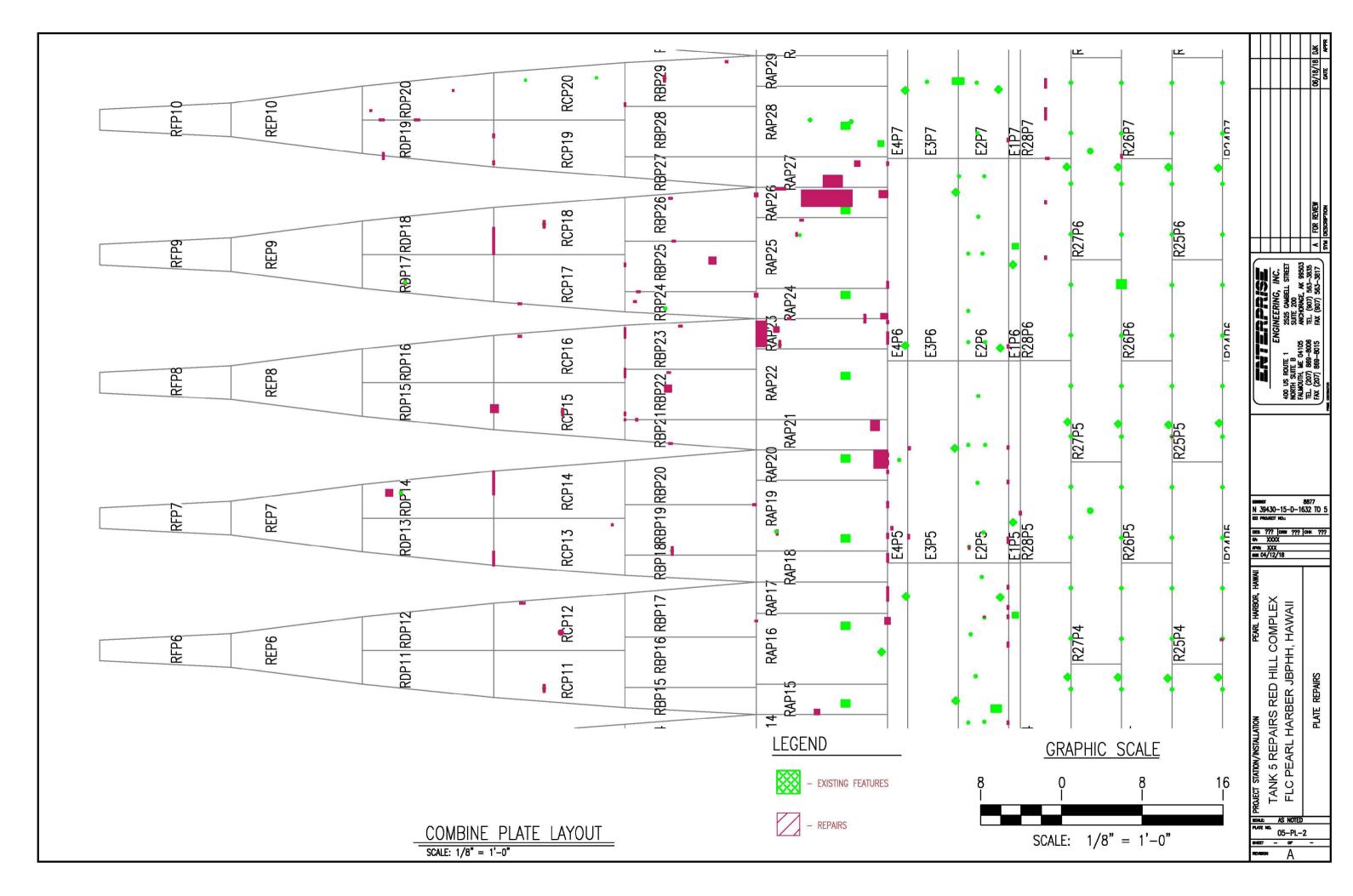
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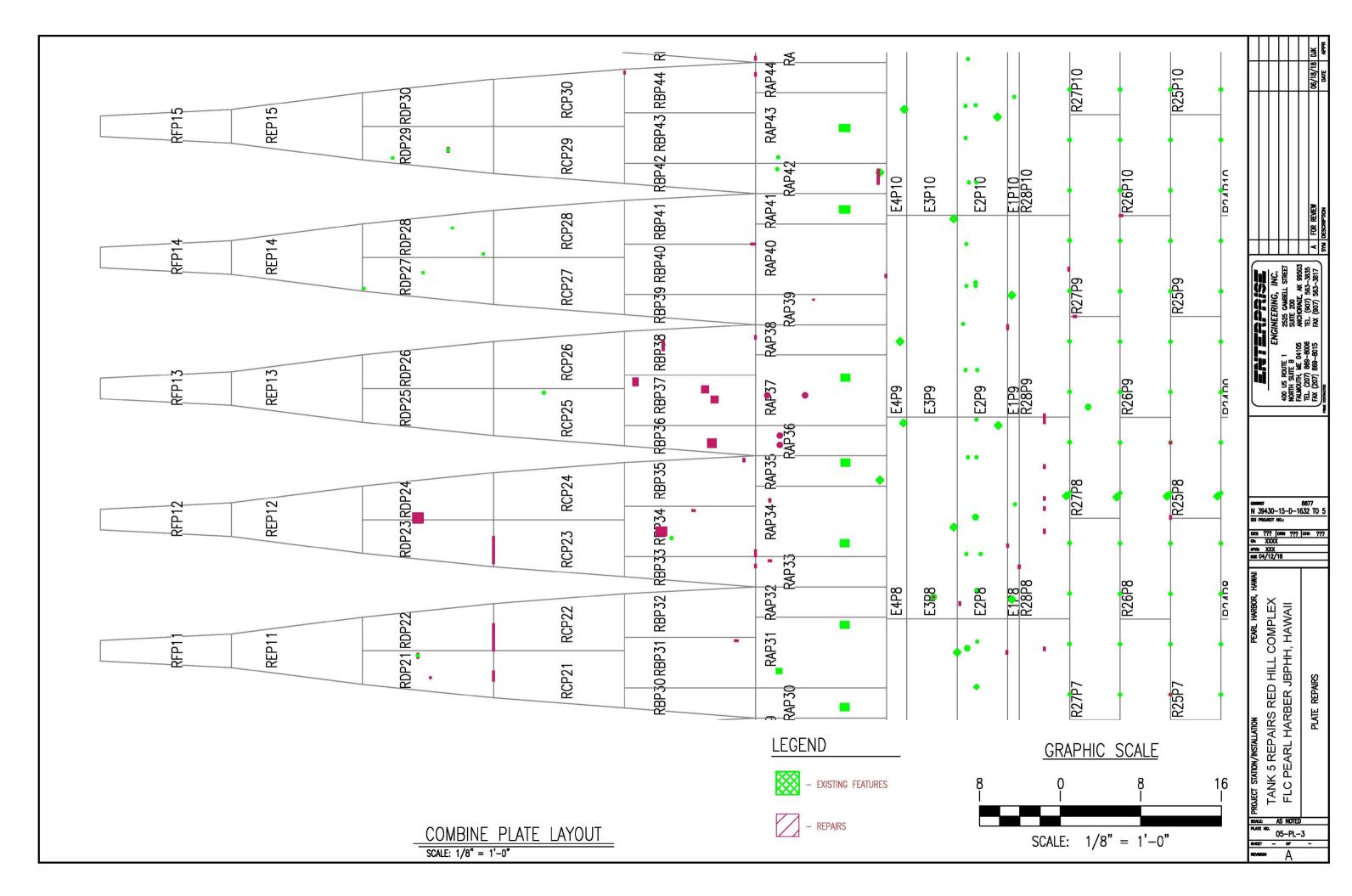
ATTACHMENT D TANK DRAWINGS

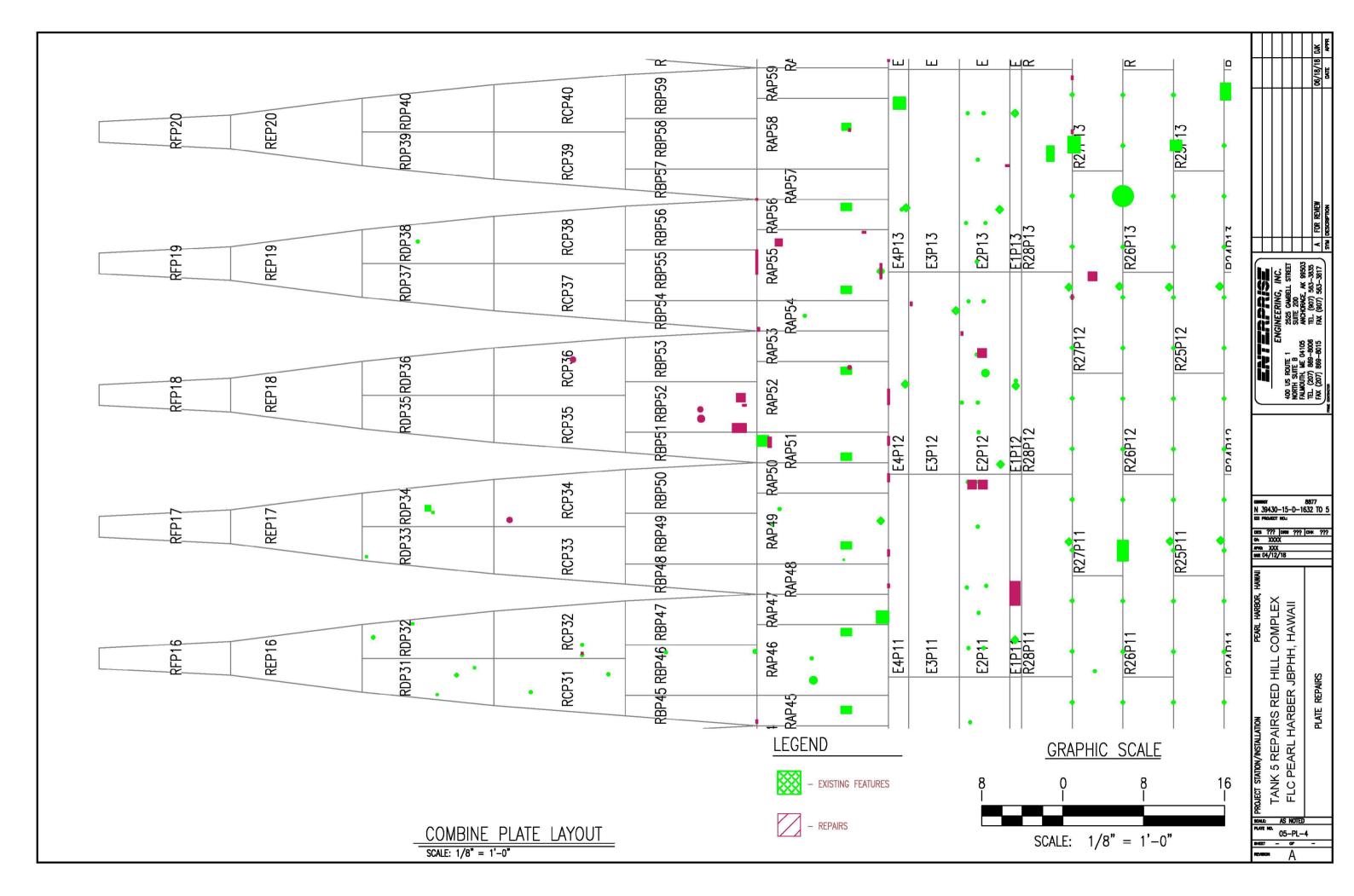
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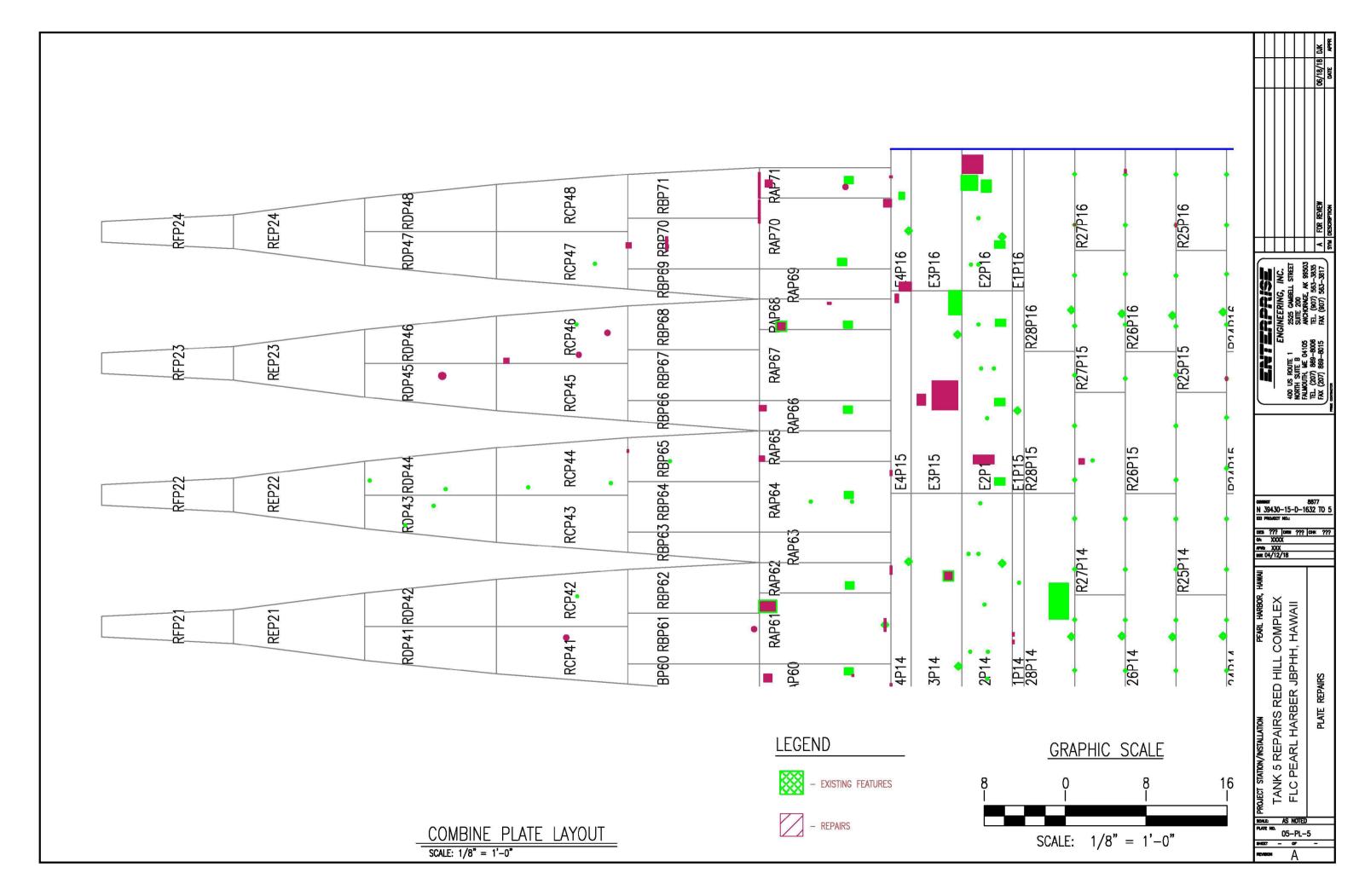
SEE DWG. 05-PL-5 MARKAN BOOM BOOM BOOM BOOM BOOM BOOM BOOM BOO				1503 A FOR REVIEW 06/18/18 DKT APPR 1000 B
SEE DWG. 05-PL-3				## CAD US ROUTE 1 2525 CAMBILI STR NORTH SUITE B SUITE 200 IF L (207) 869–8016 IE. (207) 869–8016 IE. (807) 565–38
SEE DWG. 05-PL-2	SEE DWG. 05-PL-9		MASTER PLATE LAYOUT SCALE: N.T.S.	PEARL HARBOR, HAWAIII TANK 5 REPAIRS RED HILL COMPLEX TANK 5 REPAIRS RED HILL COMPLEX 10 10 10 10 10 10 10 10 10 10 10 10 10 1

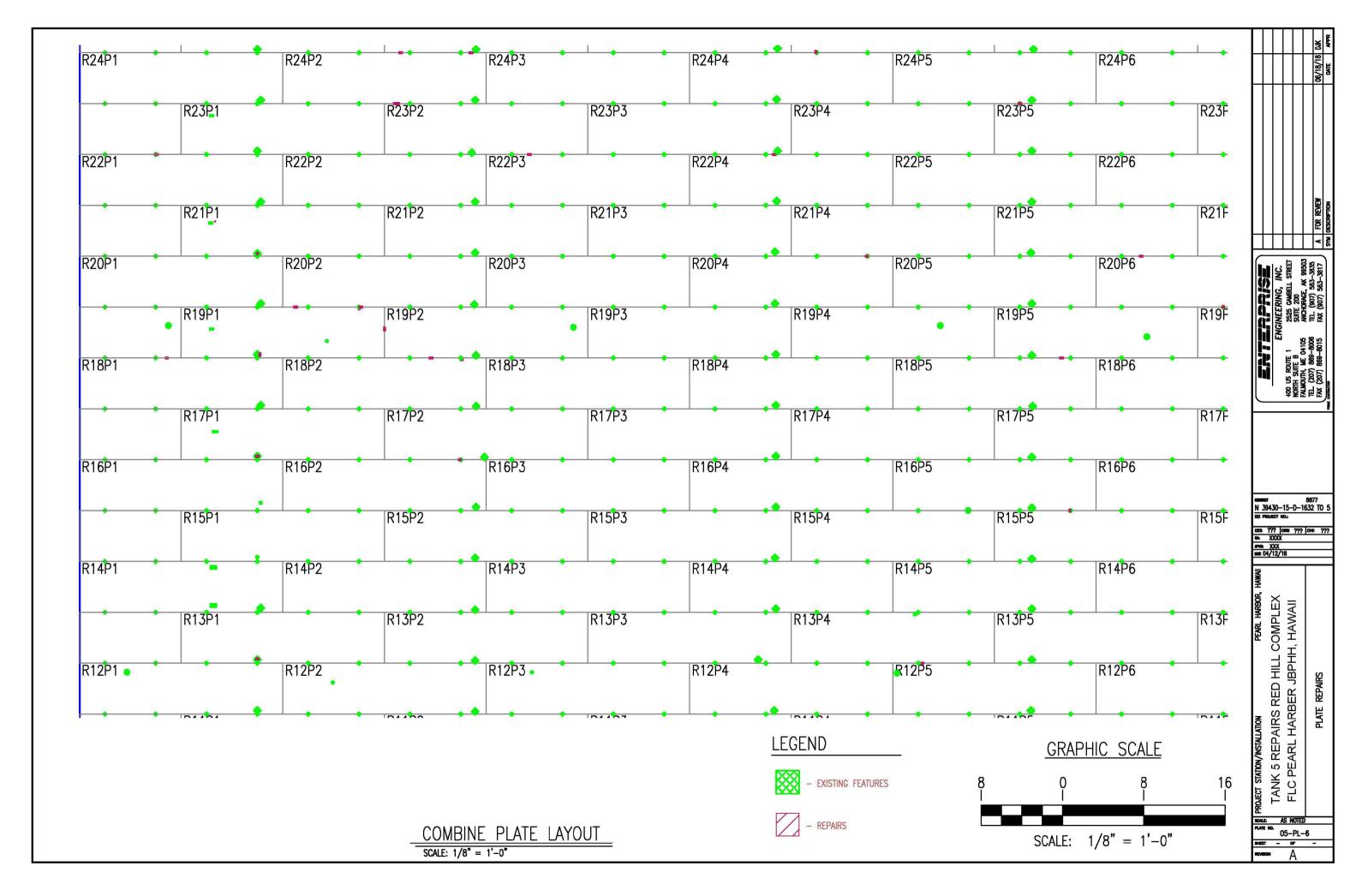


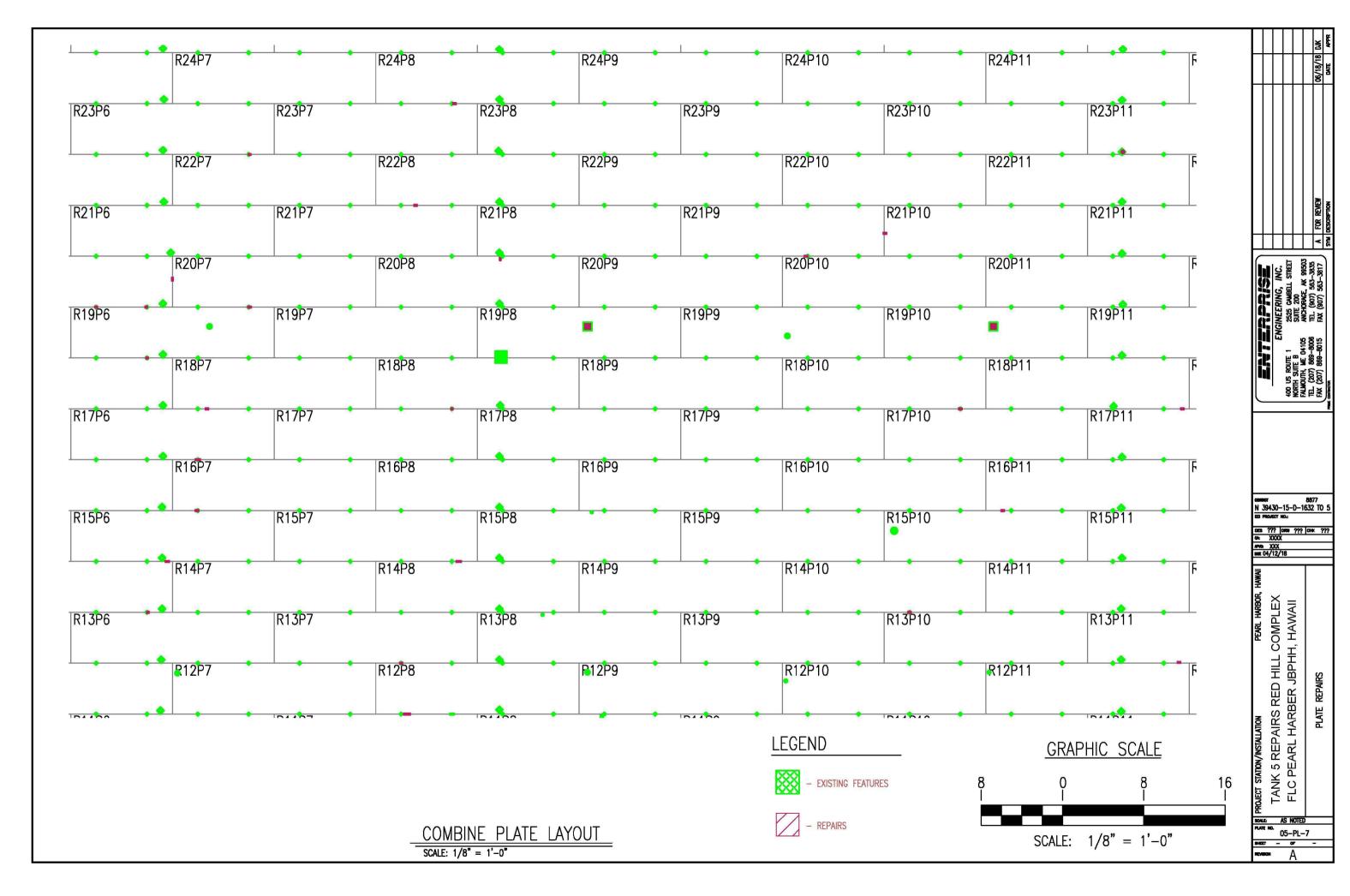


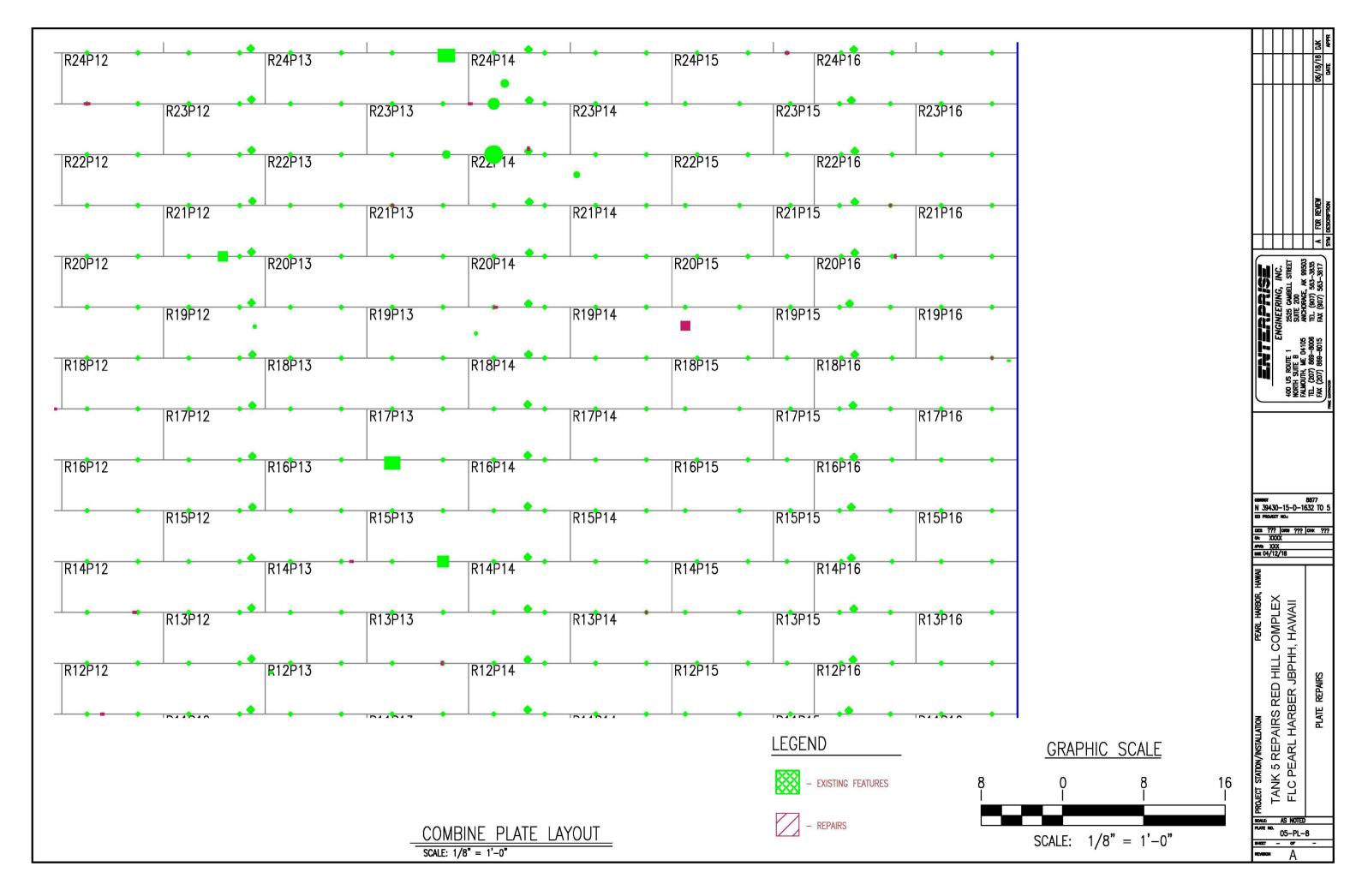


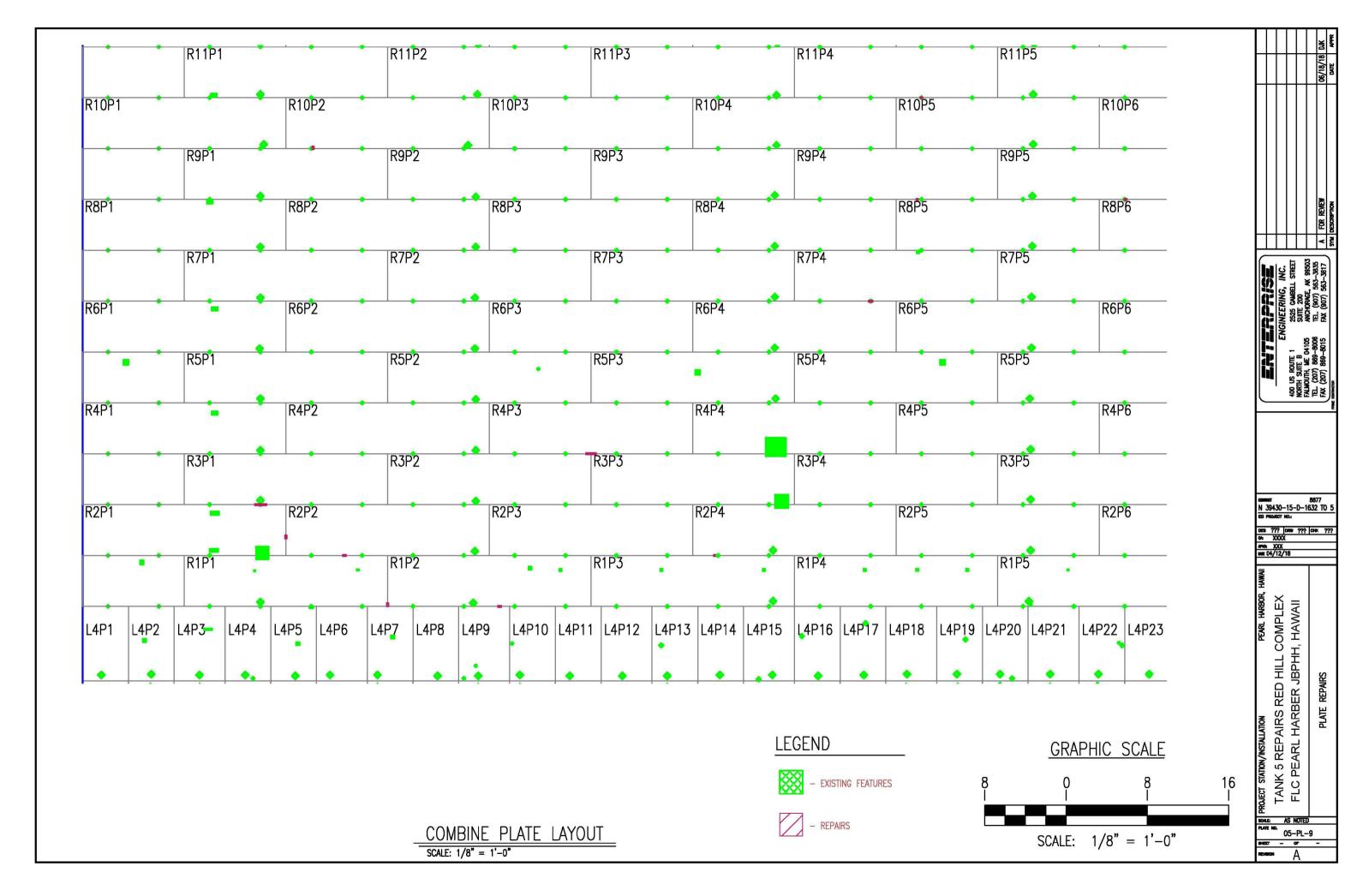


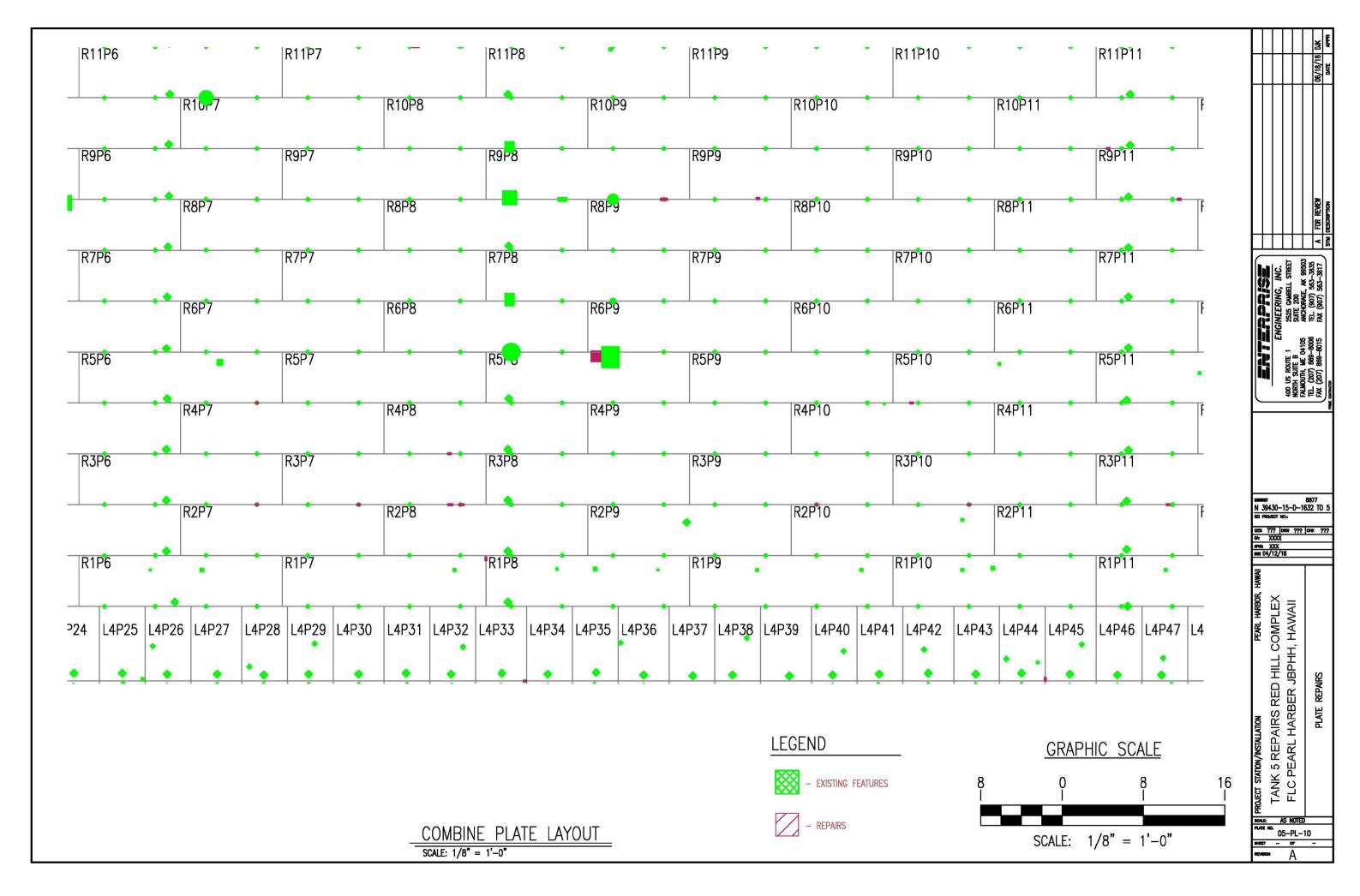


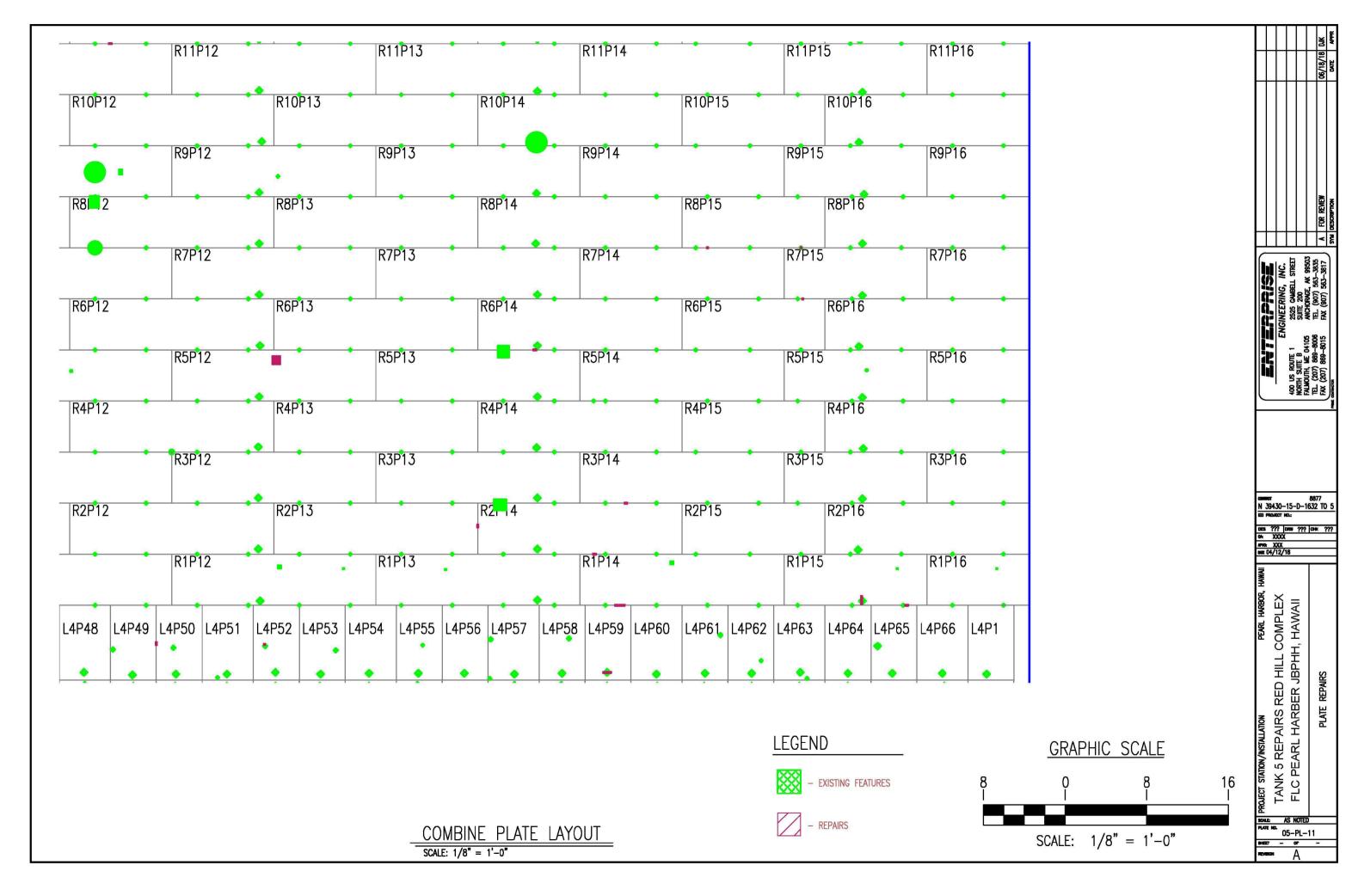


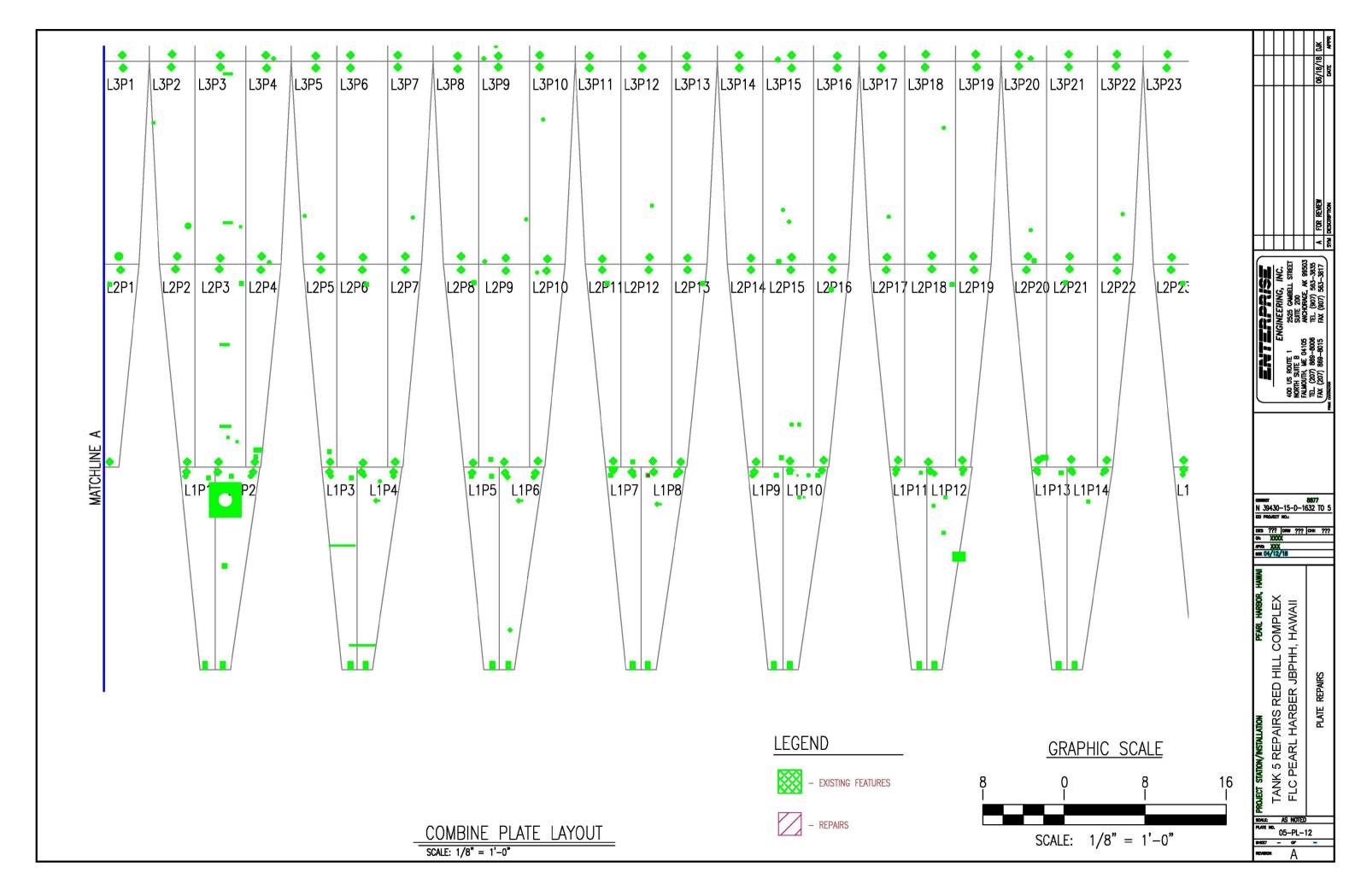


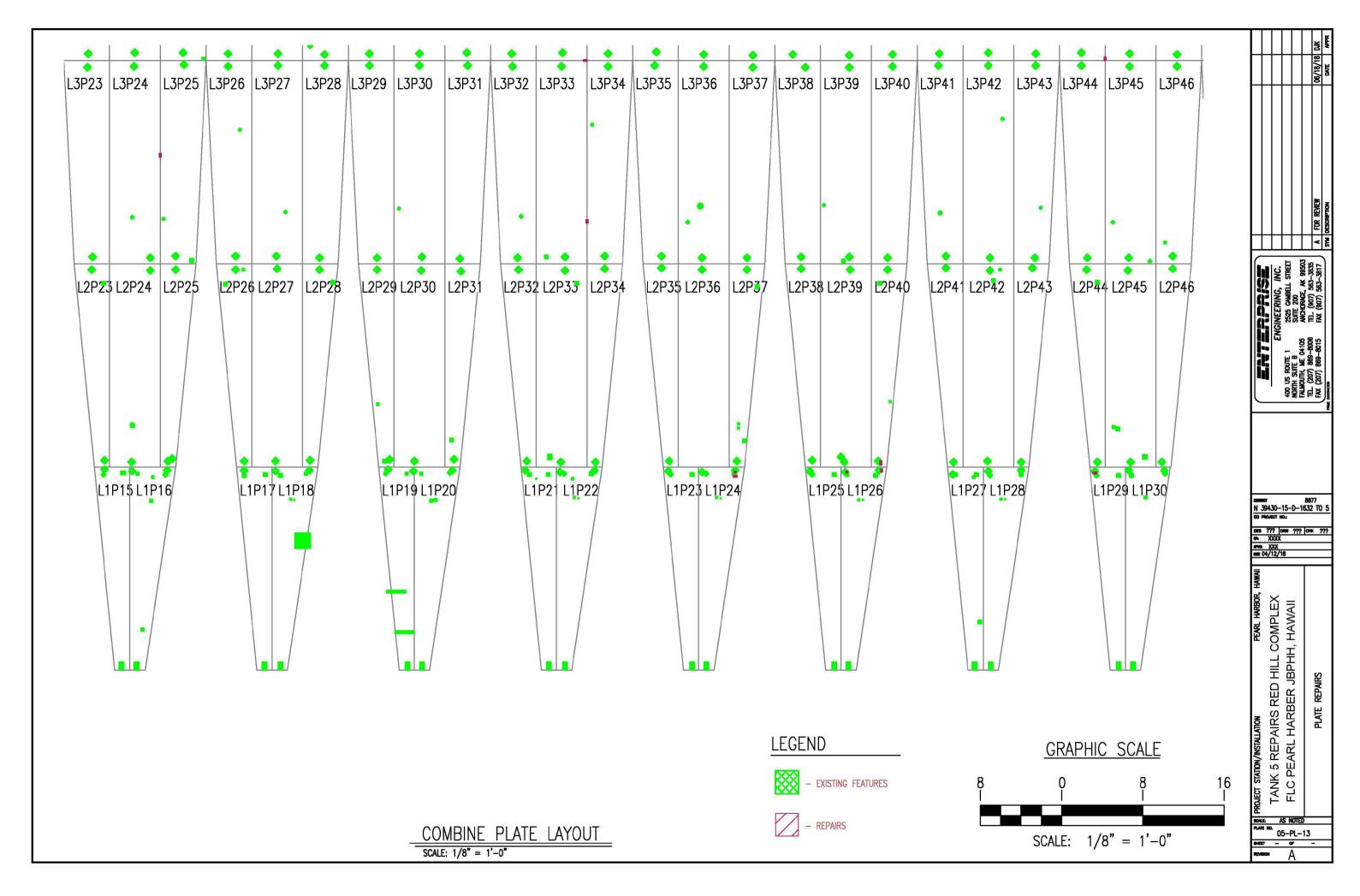


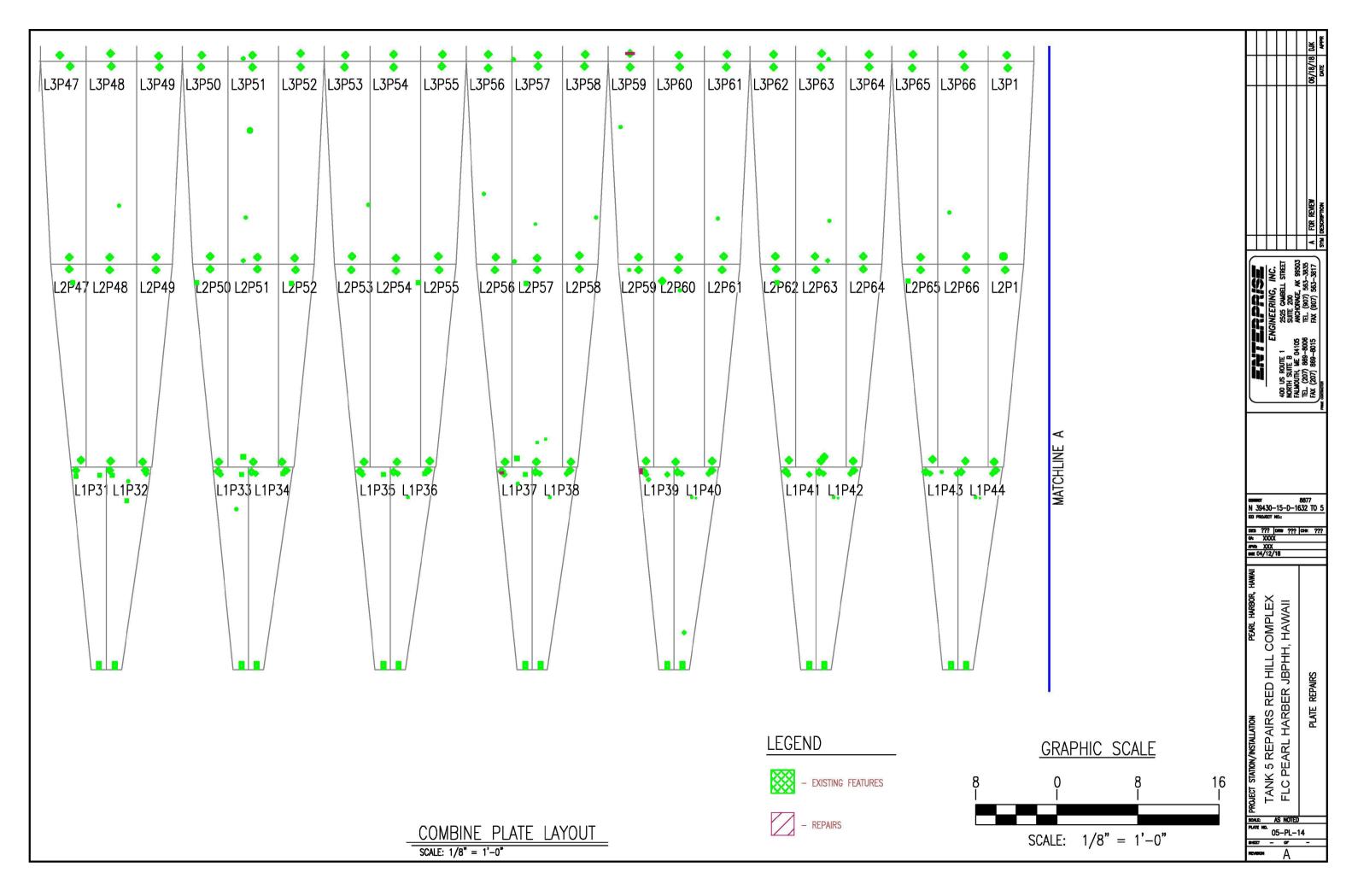












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ATTACHMENT E TANK PHOTOGRAPHS

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Photo 1: Upper Tunnel Manway



Photo 2: Catwalk and Center Tower



Photo 3: Tank Upper Dome



Photo 4: Tank Lower Dome & Barrel



Photo 5: Tank Floor



Photo 6: Tank Floor



Photo 7: Tank Drain Line Cap (Note: Indications found with Magnetic Particle Testing).



Photo 8: Drain and Sample Lines from new Tank Penetration



Photo 9: Tank Drain and Sample Lines



Photo 10: Sample Lines (Note: Supports not seal welded to tank floor).



Photo 11: Old stilling well still welded to floor



Photo 12: ATG Probe



Photo 13: Internal 18-inch Piping



Photo 14: Internal 32-inch Piping



Photo 15: Lower Tunnel Pipe Penetrations



Photo 16: 32-inch piping interior pitting



Photo 17: 32-inch pipe circumferential weld defects



Photo 18: 32-inch pipe with Insert Patch Plate



Photo 19: Tank Upper Access Area



Photo 20: Upper Access Manway



Photo 21: Roof Manhole with ATG



Photo 22: Upper Access Stairway (Note: Vent Pipe encased in concrete).



Photo 23: Upper Dome Course B



Photo 24: Upper Dome Course C



Photo 25: Upper Dome Course D



Photo 26: Extension Ring Plug Welds



Photo 27: Barrel Strain Gauge Pipe Cap



Photo 28: Backside Corrosion on existing ground areas



Photo 29: Backside Corrosion around existing patch plates

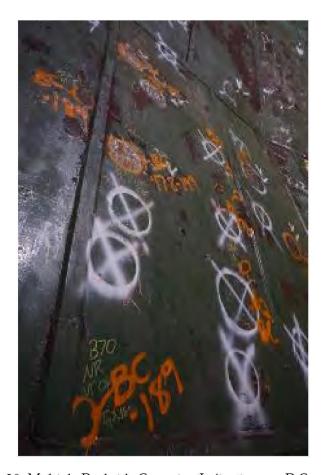


Photo 30: Multiple Backside Corrosion Indications on B Course Plate

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH EEI Project No.: 8877 ATTACHMENT E, Page 15



Photo 31: Typical Backside Corrosion Indication in D Course



Photo 32: Larger Backside Corrosion Indications in Extension Ring Plates



Photo 33: Pipe Cap covering existing grout nozzle with Backside Corrosion



Photo 34: Dent requiring repair in A Course



Photo 35: Undercut Indication in A Course



Photo 36: Rounded Indication

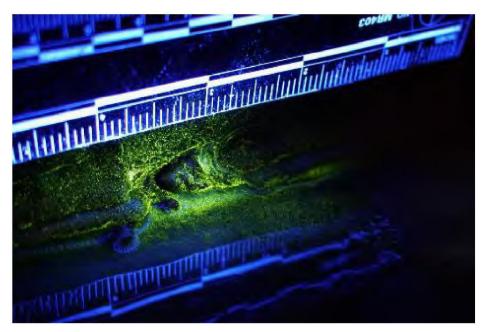


Photo 37: MT black light photo

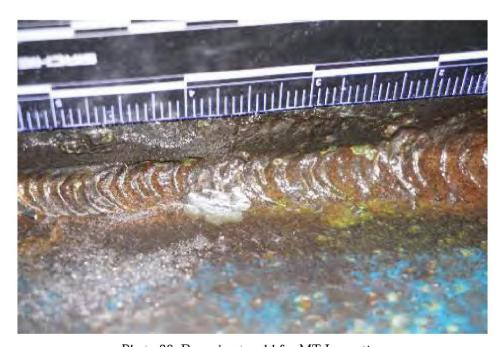


Photo 38: Burred out weld for MT Inspection



Photo 39: Vacuum Box EEI-001 for linear weld testing



Photo 40: Vacuum Box EEI-006 for small Patch Plate weld testing

ATTACHMENT F EEI/TESTEX MASTER SPREADSHEET OF FINDINGS AND REPAIRS

			Re	commended Repa	nirs	
		Number of Repairs	Linear Feet of Weld	Area of Patch Plate (sq. ft.)	Number of Patch Plates <= 2 sq. ft.	Number of Patch Plates > 2 sq. ft.
Upper Dome	Weld Repairs	15	9			
Course D	Patch Plate Repairs	6	17	3	6	0
Upper Dome	Weld Repairs	27	38			
Course C	Patch Plate Repairs	7	13	2	7	0
Upper Dome	Weld Repairs	38	20			
Course B	Patch Plate Repairs	13	35	6	13	0
Upper Dome	Weld Repairs	58	38			
Course A	Patch Plate Repairs	33	127	35	26	7
Extension Ring	Weld Repairs	32	11			
Extension King	Patch Plate Repairs	15	73	28	11	4
Barrell	Weld Repairs	144	50			
Barrell	Patch Plate Repairs	7	23	5	7	0
Lower Dome	Weld Repairs	19	8			
	Patch Plate Repairs	0	0	0	0	0
Floor	Weld Repairs	0	0			
Floor	Patch Plate Repairs	О	О	О	0	0

		Summary	y of Recommende	d Repairs	
	Number of Repairs	Linear Feet of Weld	Area of Patch Plate (sq. ft.)	Number of Patch Plates <= 2 sq. ft.	Number of Patch Plates > 2 sq. ft.
Weld Repairs	333	173			
Patch Plate Repairs	81		80	70	11
Totals	414	173	80	70	11

TOTAL RECOMM	1ENDED REPAIRS
Patch Plates	81
Weld Repairs	333
TOTAL	414

PROVE UP AND RESULTS	REPORTED BY TESTEX	POST-EEI PROVE- UP AND INSPECTION
Number of indications reported by TesTex	395	109
Total repairs of <u>individual indications</u> recommended by EEI after prove up (including TesTex reported indications)		423
BC below reporting minimum	200	60
Weld Indications	12	9
Bulges	4	0
Dents	24	21
Gouges	1	5
Other topside indications	10	6
Insufficient Fill	2	21
Lack of Fusion	3	52
Porosity (and/or Rounded Indications)	21	203
Undercut	7	46

Number of indications EEI validated for repair	109
Number of additional indications by EEI resulting in repair	314
Total Indications Requiring Repairs*	423

^{*} Several indications in close proximity were combined into a single repair - See Summary of Recommended Repairs for Final Repair count.

Ge	neral Tank Info	She	ell Locati	ion				TesT	ex NDE							EEI PRO	/E UP							Re	ecommendo	ed Repairs	5		Repair Type
No.		Gen	eral Loca	tion	cation ID		Reported n Location	TesTe	x NDE		n Wall is (in)	of Topside cation(in)	dication:	dication:)	po	Type	FIED IN TYPE	ndation	im Thickness (in)	(in)	of Repair: (in)	of Repair: ′ (in)	Oia (in)	(in)	Weld (in)	PP (sq in)		on Plate	
Tank	Overall ID	Location in Tank	Shell	Plate Number	TesTex Indication ID on Plate	X Coordinate (in)	Y Coordinate (in)	Method	Indication Type	SIMPLIFIED INDICATIO N TYPE	Minimum Thickness	Depth of T	Center of Ind X (in)	Center of Indi Y (in)	Meth	Indication	SIMPLIFIE	EEI Recomme (Repair	Minimum T	Depth (in)	Center of R X (in)	Center of Y (ir	Width or Dia (in)	Height (in)	Length of V	Area of PF	EEI repair No.	Repair No.	Repair Type (Patch, Weld, Other)
5 .	5-UD-D-3-55-48	UD	D	3	2	55	48	VT	DENT	D			55	48	VT	DENT	D	R			48	48	6	6	24	36	5-UD-D-3-48-48-1	1	TSPP
	5-UD-D-3-16-6	UD	D	3	3	16	6	UT	GA	BC	0.102		16	6	PAUT	GA	BC	R	0.121		16	6	8	8	32.00	64.00	5-UD-D-3-16-6-2	2	TSPP
	5-UD-D-8-31-57	UD	D	8									31	57	VT	LOF	LOF	R			31	57	9	0	9		5-UD-D-8-31-57-1	1	WR
	5-UD-D-8-17-148	UD	D	8									17	148	VT	UC	UC	R			17	148	6	0	6		5-UD-D-8-17-148-2	2	WR
	5-UD-D-8-24-156	UD	D	8	2	26	70	VT	DENT	D	ĺ		24	156	VT	UC	UC D	K		I	24	156	6	0	6 48.00	144.00	5-UD-D-8-24-156-3 5-UD-D-9-36-70-1	3	WR
	5-UD-D-9-36-70 5-UD-D-9-9-156	UD UD	D D	9	3	36	70	VI	DENT	U			36	70 156	VT VT	DENT	UC	R			36 9	70 156	12 4	12 0	48.00 4	144.00	5-UD-D-9-9-156-2	2	PP WR
	5-UD-D-9-39-54	UD	D	9									39	54	VT	UC	UC	R			39	54	9	0	9		5-UD-D-9-39-54-3	3	WR
	5-UD-D-10-29-78	UD	D	10									29	78	VT	UC	UC	R			29	78	4	0	4		5-UD-D-10-29-78-1	1	WR
	5-UD-D-10-37-45	UD	D	10									37	45	VT	POR	RI	R			37	45	8	0	8		5-UD-D-10-37-45-2	2	WR
5	5-UD-D-14-30-120	UD	D	14	2	30	120	VT	GA				30	120	VT	GA	GA	R	0.158		30	124	8	8	32.00	64.00	5-UD-D-14-30-124-1	1	PP
5	5-UD-D-14-30-110	UD	D	14									30	110	VT	UC	UC	R			30	110	9	0	9		5-UD-D-14-30-110-2	2	WR
5	5-UD-D-17-23-105	UD	D	17									23	105	VT	UC	UC	R			23	105	8	0	8		5-UD-D-17-23-105-1	1	WR
	5-UD-D-19-13-131	UD	D	19									13	131	VT	TSP	TS	R			13	131	8	0	8		5-UD-D-19-13-131-1	1	WR
	5-UD-D-19-56-91	UD	D	19									56	91	VT	UC	UC	R			56	91	0	6	6		5-UD-D-19-56-91-2	2	WR
	5-UD-D-20-0-133	UD	D	20									0	133	VT	POR	RI	R			0	133	0	6	6		5-UD-D-20-0-133-1	1	WR
	5-UD-D-21-50-90	UD	D	21									50	90	VT	LOF	LOF RI	K			50	90	9	0	9		5-UD-D-21-50-90-1	1	WR
	5-UD-D-21-24-75 5-UD-D-24-2-90	UD UD	D D	21 24	1	2	90	VT	DENT	D			24	75 90	VT VT	POR DENT	D	R			24 2	75 90	2 12	0 12	2 48	144	5-UD-D-21-24-75-2 5-UD-D-24-2-90-1	2 1	WR TSPP
	5-UD-D-29-28-54	UD	D	29	1	2	90	VI	DEINT	U			28	54	VT	POR	RI	R			28	54	10	0	10	144	5-UD-D-29-28-54-1	1	WR
	5-UD-D-45-41-64	UD	D	45	2	41	64	VT	DENT	D		0.160	41	64	VT	DENT	D	R			41	64	8	0	25.13	50.27	5-UD-D-45-41-64-1	1	PP
	5-UD-C-3-28-156	UD	C	3	-	1.1.	01		DEN			0.100	28	156	VT	LOF	LOF	R			28	156	56	0	56	30.27	5-UD-C-3-28-156-1	1	WR
	5-UD-C-3-36-0	UD	C	3									36	0	VT	UC	UC	R			36	0	4	0	4		5-UD-C-3-36-0-2	2	WR
5	5-UD-C-4-54-0	UD	C	4									54	0	VT	UC	UC	R			54	0	12	0	12		5-UD-C-4-54-0-1	1	WR
5	5-UD-C-4-28-156	UD	C	4									28	156	VT	LOF	LOF	R			28	156	56	0	56		5-UD-C-4-28-156-2	2	WR
5 .	5-UD-C-5-38-55	UD	C	5									38	55	VT	LOF	LOF	R			38	55	9	0	9		5-UD-C-5-38-55-1	1	WR
5	5-UD-C-6-10-156	UD	C	6									10	156	VT	LOF	LOF	R			10	156	20	0	20		5-UD-C-6-10-156-1	1	WR
	5-UD-C-7-29-104	UD	C	7									29	104	VT	LOF	LOF	R			29	104	9	0	9		5-UD-C-7-29-104-1	1	WR
	5-UD-C-9-51-122	UD	С	9									51	122	VT	LOF	LOF	R			51	122	5	0	5		5-UD-C-9-51-122-1	1	WR
	5-UD-C-9-58-26	UD	C	9									58	26	VT	LOF	LOF	R			58	26	3	0	3		5-UD-C-9-58-26-2	2	WR
	5-UD-C-9-34-0	UD	С	9	2	24	111	VCT	TC	TC		0.004	34	0	VT	LOF	LOF	R		0.425	34	0	68	0	68		5-UD-C-9-34-0-3	3	WR
	5-UD-C-10-21-114 5-UD-C-11-23-96	UD	C	10	2	21	114	VT	TC	TS		0.094	21	114	VT	TC	TS	K		0.125	21	114	2 9	0 0	9		5-UD-C-10-21-114-1 5-UD-C-11-23-96-1	1	WR
	5-UD-C-11-23-96 5-UD-C-12-21-76	UD UD	C C	11 12									23 21	96 76	VT VT	LOF DENT	LOF	R			23 21	96 76	6	0	18.85	28 27	5-UD-C-11-23-96-1 5-UD-C-12-21-76-1	1	WR PP
	5-UD-C-12-56-122	UD	c	12									56	122	VT	POR	RI	R			56	122	0	6	6	20.27	5-UD-C-12-56-122-2	2	WR
	5-UD-C-13-8-156	UD	C	13									8	156	VT	UC	UC	R			8	156	17	0	17		5-UD-C-13-8-156-1	1	WR
	5-UD-C-13-60-15	UD	C	13									60	15	VT	TSP	TS	R			60	15	2	0	2		5-UD-C-13-60-15-2	2	WR
5	5-UD-C-14-42-156	UD	C	14									42	156	VT	UC	UC	R			42	156	28	0	28		5-UD-C-14-42-156-1	1	WR
5 .	5-UD-C-15-37-155	UD	C	15	1	37	155	VT	DENT	D			37	155	VT	DENT	D	R			37	155	9	9	36	81	5-UD-C-15-37-155-1	1	TSPP
5 .	5-UD-C-15-33-74	UD	C	15									33	74	VT	LOF	LOF	R			33	74	9	0	9		5-UD-C-15-33-74-2	2	WR
	5-UD-C-16-55-125	UD	C	16	5	55	125	BFET	WI	WI			55	125	VT	WI	WI	R			55	125	0	4	4		5-UD-C-16-55-125-1	1	WR
	5-UD-C-17-0-125	UD	С	17									0	125	VT	POR	RI	R			0	125	0	4	4		5-UD-C-17-0-125-1	1	WR
	5-UD-C-18-36-96	UD	C	18									36	96	VT	LOF	LOF	R			36	96	9	0	9		5-UD-C-18-36-96-1	1	WR
	5-UD-C-18-16-156	UD	С	18									16	156	VT	POR	RI	R			16	156 156	32	0	32		5-UD-C-18-16-156-2	2	WR
	5-UD-C-19-5-156	UD	С	19									5	156 156	VT	POR	RI	R			5 27	156	4	0	4		5-UD-C-19-5-156-1	1	WR
	5-UD-C-19-37-156 5-UD-C-21-38-156	UD	C C	19 21									37 38	156 156	VT	LOF UC	LOF UC	K			37 38	156 156	4 12	0 0	4 12		5-UD-C-19-37-156-2 5-UD-C-21-38-156-1	2	WR WR
	5-UD-C-21-38-156 5-UD-C-22-16-156	UD UD	C	21									38 16	156 156	VT	LOF	LOF	R			38 16	156 156	12 32	0	12 32		5-UD-C-21-38-156-1 5-UD-C-22-16-156-1	1	WR
	5-UD-C-23-32-156	UD	C	23									32	156	VT	UC	UC	R			32	156	32	0	32		5-UD-C-23-32-156-1	1	WR
	5-UD-C-32-6-51	UD	С	32									6	51	VT	RI	RI	R			6	51	2	0	2		5-UD-C-32-6-51-1	1	WR
	5-UD-C-34-8-137	UD	C	34									8	137	VT	DENT	D	R			8	137	6	0	18.85	28.27	5-UD-C-34-8-137-1	1	PP
	5-UD-C-41-54-73	UD	c	41	3	51-56	73	LFET	BC	ВС	0.177		54	73	PAUT	BC	BC	R	0.154		55	73	6	0	18.85	28.27	5-UD-C-41-55-73-1	1	PP
	5-UD-C-46-36-24	UD	C	46	1	33-39	24	VT	DENT	D	- 60000 6	0.040	36	24	VT	DENT	D	R			36	24	6	0	18.85		5-UD-C-46-36-24-1	1	PP
	5-UD-C-46-7-60	UD	C	46	2	4-10	60	LFET	BC	BC	0.178		7	60	PAUT	BC	BC	R	0.149		10	58	6	0	18.85		5-UD-C-46-10-58-2	2	PP
					•																								

Part Control	General Tank Info	Shell Location				Tes	Tex NDE							EEI PRO	VE UP						F	Recommend	led Repairs	s		Repair
Second Column			<u></u>	TovTo	v Donastad			<u> </u>		40	: <u>:</u>	: <u>.</u>			101	SS			l	antinosin.	I	1	1	T		Type `
S	0 0	General Location	ation	land to make	and the same of th	TesT	ex NDE		s (in)	opside n(in)	<u>.</u>	l ö	þ	Туре	IED N TYP		(in)	Repair	Repair	oia (in)	(ij)	/eld (ii	ni ps)		on Pla	(Patc
2 Supplementary 100 0 C 44	ne A Overall ID	Location in Tank Shell Course Plate		× ordina	Y Coordinate (in)	Method	Indication Type	CATI	Minimum Thicknes	Depth of T	enter of X	Center of Ind Y (in)	Metho	Indication	SIMPLIF	ER Common Repair imum (ir	Depth (enter of X (ir	Center of F Y (in)	idth or	Height	ngth of	و ا	EEI repair No.	pair No.	Repair Type (Patch, Weld, Other)
5 - SUMPLIAN STATE							•										0.14			-	-		36			TSPP
5 SUBSPEACE US B 9 S SUBSPEACE US B 9 S SUBSPEACE US B 9 S SUBSPEACE US B 10 S SUBSPEACE US B SUBSPEACE US B 10 S SUBSPEACE US					110	V.CT	DOD				50.24204.11							33			_					WR
5 SMORANDA UN			2	1	110	VI	POR	Р										20		-	0	-				WR WR
1														10,000	0.00						0				100	WR
S SLUB 17-19 W 17-19																			-		5	**				WR
5 SUD-25-26-26-26-26-26-26-26-26-26-26-26-26-26-											19	0	VT		RI	R		19	0	0	3	3			1	WR
5 5-00-2-2-7-3-5	5 5-UD-B-19-5-100	UD B 19									5	100	VT	LOF	LOF	R		5	100	10	0	10		5-UD-B-19-5-100-1	1	WR
5 3-00-22-5-15	5 5-UD-B-20-0-2	UD B 20									0	2	VT	LOF	LOF	R		0	2	0	4	4		5-UD-B-20-0-2-1	1	WR
5 5 Web 24-528 We 9 2 22 5 Web 24-528 We 9 2 22 5 Web 24-524 We 9 25 Web 24-524 W	5 5-UD-B-21-0-102	UD B 21									0	102	VT	LOF	LOF	R		0	102	0	4	4		5-UD-B-21-0-102-1	1	WR
S SUMP-27-24-156 UN S 22 S SUMP-27-25-156 UN S 22 S SUMP-27-25-156 UN S 22 S SUMP-27-25-156 UN S 23 S SUMP-27-25-156 UN S 23 S S S S S S S S S																5.5				2	2	4				WR
No.											3							3			0	-				WR
5 Subb 23-25-250 UD 6 8 22 5 Subb 23-25-250 UD 6 8 28 5 Subb 23-25-250 UD 6 8 29 5 Subb 23-25-250 UD 6 8 29 5 Subb 23-25-250 UD 6 8 29 5 Subb 23-25-250 UD 6 8 25 5 Subb 23-25-250 UD 6 8 29 5 Subb 23-25-250 UD 6											KMC 7/002					5.5					0					WR
5 S-U09-23-26-104 UO 8 8 23																K					0		6.1			WR PP
5 S-U0-32-34-3156 UD 0 8 23 S-U0-32-35-36 UD 0 8 25 S-U0-32-35-36 UD 0 8 26 S-																R					1		04			WR
5 5 100 23 20 156															2.00						0					WR
5 S-LD-8-2-2-3-3-90 UD 8 2 28 S S-LD-8-2-2-3-3-90 UD 8 2 28 S S-LD-8-2-2-3-3-90 UD 8 2 24 S S-LD-8-2-2-3-3-90 UD 8 2 24 S S-LD-8-2-3-3-3-90 UD 8 2 24 S S-LD-8-2-3-3-3-90 UD 8 2 25 S-LD-8-2-3-3-3-90 UD 8 2 26 S S-LD-8-2-3-3-3-90 UD 8 2 2											1000					1 Total					2					WR
5 SUB-824-78-00 UD 8 74 SUB-824-78-00 UD 8 75 SUB-824-78-00 UD 8 7											51		VT		RI	R		51		0	4	4			3	WR
5 S-U0B-25-21-169 UD 8 8 25 S-U0B-25-22-156 UD 8 8 25 S-U0B-25-22-156 UD 8 8 25 S-U0B-25-23-25 S-UD 8 8 25 S-U0B-25-23-25 S-UD 8 8 32 S-UD 8 25-23-25 S-UD 8 2	5 5-UD-B-24-20-144	UD B 24									20	144	VT	POR	RI	R		20	144	O	3	3		5-UD-B-24-20-144-1	1	WR
\$ \$-S-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	5 5-UD-B-24-28-0	UD B 24									28	0	VT	POR	RI	R		28	0	4	4	8		5-UD-B-24-28-0-2	2	WR
5 5 UID-R-25-75-72 UD 8 2550 D 00 8 26 5 5 UID-R-25-75-72 UD 8 25 5 5 UID-R-25-102 UD 8 26 5 5 UID-R-25-102 UD 8 26 5 5 UID-R-25-103 UD 8 34 5 5 UID-R-25-103 UD 8 36 5 5 UID-R-25-103 UD 8 52 5 UID-R-25-103 UD 8	5 5-UD-B-25-0-140	UD B 25									0	140	VT	LOF	LOF	R		0	140	1	4	5		5-UD-B-25-0-140-1	1	WR
5 5.UD-8.265-5.0 UD	5 5-UD-B-25-32-156	UD B 25									32	156	VT	LOF	LOF	R		32	156	4	0	4		5-UD-B-25-32-156-2	2	WR
5 5-UD-82-0-2-98 5 5-UD-82-0-3-3-109 5 5-UD-82-3-3-3-109 5 UD 8 20 5 5-UD-82-3-3-3-109 5																R				8	8		64			PP
5 5-UD-8-25-1-10 UD B 26 75 5-UD-8-25-1-10 UD B 26 75 5-UD-8-25-1-10 UD B 27 75 5-UD-8-23-1-35 UD B 27 8 5-UD-8-23-1-35 UD B 27 8 5-UD-8-23-1-35 UD B 27 8 5-UD-8-23-1-35 UD B 31 1											0.000		2 (2			R			-	4	4					WR
5 S-UD-829-3-156																				_	4					WR
5 S-UD-B293-3109 UD 8 29 5 S-UD-B293-3109 UD 8 29 5 S-UD-B293-3109 UD 8 29 5 S-UD-B293-3109 UD 8 31 5 S-UD-B293-3109 UD 8 34 5 S-UD-B293-3109 UD 8 35 S-UD-B293-3109 UD 8 36 S-UD-B293-3109 UD 8 36 S-UD-B293-3109 UD 8 37 S-UD-B293-3109 UD 8 38 S-UD-B293-3109 UD 8 38 S-UD-B293-3109 UD 8 S-UD-B											KASA 34										4					WR
5 S-UD-B-29-33-35																					0					WR WR
5 S-UD-8-34-5-23 UD 8 31													8 6			5.0					3					WR
5 S-UD-834-4-81 UD													1.5			R				4	0				1	WR
5 S-UDB-34-33-74 UD B 34 UD B 34 S-UDB-34-33-74 UD B 3 34 UD B 34 S-UDB-34-33-74 UD B 3 34 S-UDB-34-33-74 UD B 3 34 S-UDB-34-33-74 UD B 3 35 S-UDB-35-5-14 UD B 3 35 S-UDB-35-5-14 UD B 3 36 S-UDB-34-33-74 UD B 3 37 S-UDB-34-34-33 S-UDB-34-34-34 UD B 3 37 S-UDB-34-34-34-34 UD B 3 37 S-UDB-34-34-34-34 UD B 3 37 S-UDB-34-34											4		25 17 180			R		4		8	ō	2000			1	WR
5 S-UD-B-37-55-14 UD B 35 S UD B-37-55-14 UD B 36 S UD B-37-55-14 UD B 37 S UD B-37-55-14 UD B 37 S UD B-37-35-14 UD B 37 S UD B-37-35-10 UD B 37 S UD B-37-35-14 UD B 38 S UD B-37-35-14 UD B 59 UD B-37-35-15 UD B 59 UD B-37-35-14 UD B 59 UD B-37-35-15 UD B 59 UD B-57-35-15 UD B 50 UD B-37-35-15											30		VT		RI	R		30	112	12	10		120			PP
5 5-UD-B-37-52-11 UD B 37 1 49-55 141 LFET BC BC 0.194 5 5-UD-B-37-52-141 UD B 37 1 49-55 141 LFET BC BC 0.194 5 5-UD-B-37-31-49 UD B 37 2 0.332 49 VT DENT D D 0.140 31 49 VT DENT D R 31 49 8 8 32 64 5-UD-B-37-52-143-1 1 2 0.140 31 49 VT DENT D R 31 49 8 8 32 64 5-UD-B-37-31-49-2 2 0.100 B 37 3 42-44 60 VT DENT D R 31 49 8 8 32 64 5-UD-B-37-31-49-2 2 0.100 B 37 3 42-44 60 VT DENT D R 31 49 8 8 32 64 5-UD-B-37-31-49-2 2 0.100 B 37 3 42-44 60 VT DENT D R 31 49 8 8 32 64 5-UD-B-37-31-49-2 2 0.100 B 38 5 1 10 VT DENT D R S 110 VT DE	5 5-UD-B-34-33-74	UD B 34									33	74	VT	POR	RI	R		33		0	4	4			3	WR
5 5-UD-B-37-52-141 UD B 37 2 30-32 49 VT DENT D CHAT D CHA	5 5-UD-B-35-55-14	UD B 35									55	14	VT	POR	RI	R		55	14	4	0	4		5-UD-B-35-55-14-1	1	WR
5 5-UD-B-37-31-49 UD B 37 3 42-44 60 VT DENT D A37-31-49-2 2 5 5-UD-B-37-31-49 UD B 37 5 42-44 60 VT DENT D BAT D	5 5-UD-B-36-15-52	UD B 36	2	15	52	VT	DENT	D			15	52	VT	DENT	D	R		15	52	10	10	40	100	5-UD-B-36-15-52-1	1	PP
5 5-UD-B-37-43-60 UD B 37	5 5-UD-B-37-52-141	UD B 37	1	49-55	141	LFET	BC	BC	0.194		52	141	PAUT	BC	BC	R 0.144		52	143	9	6	30	54	5-UD-B-37-52-143-1	1	PP
5 5-UD-B-38-35-110 UD B 38 38				30-32				-			31					R		31		8	8		64			PP
5 5-UD-8-44-8-156 UD B 44			3	42-44	60	VT	DENT	D		0.125											8		64			PP
5 5-UD-B-52-15-70 UD B 44 5 5-UD-B-52-15-70 UD B 52 5 5-UD-B-52-17-72 UD B 52 5 5-UD-B-52-4-11 UD B 52 5 5-UD-B-52-4-11 UD B 52 5 5-UD-B-52-4-11 UD B 52 5 5-UD-B-52-32-15 UD B 55 5 5-UD-B-52-32-15 UD B 55 5 5-UD-B-51-4-10 UD B 55 5 5-UD-B-65-36-156 UD B 65 5 5-UD-B-65-36-156 UD B 70 5 5-UD-B-70-30-110 UD																										WR
5 5-UD-B-52-15-70 UD B 5 52 3 10-20 70 LFET BC BC BC 0.169 5 5-UD-B-52-27-72 UD B 5 52 3 22-32 72 LFET BC BC BC 0.170 5 5-UD-B-52-4-21 UD B 5 52 5 UD-B-52-4-21 UD B 5 52 5 UD-B-52-4-21 UD B 5 52 5 UD-B-52-4-19 UD B 5 52 5 UD-B-52-32-15 UD B 5 52 5 UD-B-52-32-15 UD B 5 55 5-UD-B-52-32-15 UD B 6 61 1 37-55 12-24 LFET BC BC BC 0.152 BC 0											100=0					1821					_					WR
5 5-UD-B-52-27-72 UD B 5 52 3 22-32 72 LFET BC BC BC 0.170 5 5-UD-B-52-4-21 UD B 5 52 5 1-7 18-24 LFET BC BC BC 0.178 18-24 LFET BC			2	10.20	70	LECT	DC.	DC.	0.160													_	E0 26549			WR PP
5 5-UD-B-52-4-21 UD B 52 5 1-7 18-24 LFET BC BC BC 0.178 4 21 PAUT BC BC BC R < 0.160 5 21 10 16 52 160 5-UD-B-52-52-1-3 3 5 5-UD-B-52-41-19 UD B 52 5-UD-B-52-32-15 UD B 52 5-UD-B-52-32-15 UD B 52 5-UD-B-52-32-15 UD B 55 5-UD-B-55-44-0 UD B 55 5-UD-B-55-44-0 UD B 61 1 37-55 12-24 LFET BC BC BC 0.152 41 18 PAUT BC BC BC R 0.144 41 19 10 10 40 100 5-UD-B-52-41-19-4 4									100000000000000000000000000000000000000		1000					11 0.13					•					PP
5 5-UD-B-52-41-19								1			4										_					PP
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5 5-UD-B-55-44-0 UD B 55																										WR
5 5-UD-B-61-41-18 UD B 61 1 37-55 12-24 LFET BC BC 0.152 41 18 PAUT BC BC R 0.144 41 6 6 0 18.849556 28.27433 5-UD-B-61-41-6-1 1 5 5-UD-B-65-36-156 UD B 65 5-UD-B-70-30-110 UD B 70 5-UD-B-70-28-155 UD B 70 6 6 70 18.849556 28.27433 5-UD-B-61-41-6-1 1 36 156 VT POR RI R 30 110 16 0 16 5-UD-B-70-30-110-1 1 28 155 VT UF IF R 28 155 6 6 24 36 5-UD-B-70-28-155-2 2																										WR
5 5-UD-B-65-36-156 UD B 65 5 5-UD-B-70-30-110 UD B 70 5 5-UD-B-70-28-155 UD B 70 8 36 156 VT POR RI R 36 156 4 0 4 5-UD-B-65-36-156-1 1 30 110 VT UF IF R 30 110 16 0 16 5-UD-B-70-30-110-1 1 28 155 VT UF IF R 28 155 6 6 24 36 5-UD-B-70-28-155-2 2			1	37-55	12-24	LFET	BC	BC	0.152		41					R 0.144			6		0		5 28.27433			PP
5 5-UD-B-70-28-155 UD B 70 28 155 VT UF IF R 28 155 6 6 24 36 5-UD-B-70-28-155-2 2	5 5-UD-B-65-36-156										36	156	VT	POR	RI	R		36	156	4	0	4		5-UD-B-65-36-156-1	1	WR
11 100 100 100 100 100 100 100 100 100	5 5-UD-B-70-30-110	UD B 70									30	110	VT	UF	IF	R		30	110	16	0	16		5-UD-B-70-30-110-1	1	WR
5 5-UD-A-1-66-45 UD A 1 66 45 VT UF IF R 66 45 4 0 4 5-UD-A-1-66-45-1 1	5 5-UD-B-70-28-155	UD B 70									28	155	VT	UF	IF	R		28	155	6	6	24	36	5-UD-B-70-28-155-2	2	TSPP
											66										0	4				WR
5 5-UD-A-2-0-144 UD A 2 0 144 0 4 4 5-UD-A-2-0-144-1 1																		2			4					WR
5 5-UD-A-2-9-0 UD A 2	5 5-UD-A-2-9-0	UD A 2	1							I	9	0	VT	UC	UC	R		9	0	12	0	12		5-UD-A-2-9-0-2	2	WR

G	eneral Tank Info	She	ell Locati	ion				TesT	ex NDE							EEI PRO	/E UP						R	tecommend	led Repairs	5		Repair Type
No.		Gene	eral Loca	tion	ex Indication ID on Plate		Reported n Location	TesTe	ex NDE		n Wall ss (in)	of Topside cation(in)	idication:	Indication: (in)	po	n Type	FIED IN TYPE	EEI Imendation Dair or No	(in)	of Repair: (in)	of Repair: ′ (in)	· Dia (in)	(in)	Weld (in)	PP (sq in)		on Plate	pair Type (Patch,
Tank	Overall ID	Location in Tank	Shell Course	Plate Number	TesTex Indi on Pl	X Coordinate (in)	Y Coordinate (in)	Method	Indication Type	SIMPLIFIED INDICATIO N TYPE	Minimum Thickness	Depth of Tindication	Center of Ind X (in)	Center of Ir	Meth	Indication	SIMPLIFIE	EE Recomme (Repair Minimum T	U U	Center of R X (in)	Center of Y (ir	Width or	Height (in)	Length of \	Area of PF	EEI repair No.	Repair No.	Repair Typ. Weld, C
	5-UD-A-3-22-0	UD	A	3		24	-		5	0	0.40		22	0	VT	UC	UC	R	4.00	22	0	19	0	19		5-UD-A-3-22-0-1	1	WR
	5-UD-A-5-31-7 5-UD-A-5-12-45	UD UD	Α	5 5	3	31	7	LFET	BC	BC	0.18		31 12	7 45	PAUT VT	BC RI	BC RI	K <u< td=""><td>0.160</td><td>32 12</td><td>5 45</td><td>8</td><td>10 0</td><td>36 2</td><td>80</td><td>5-UD-A-5-32-5-1 5-UD-A-5-12-45-2</td><td>2</td><td>PP WR</td></u<>	0.160	32 12	5 4 5	8	10 0	36 2	80	5-UD-A-5-32-5-1 5-UD-A-5-12-45-2	2	PP WR
	5-UD-A-5-12-43 5-UD-A-6-27-102	UD	Α	6	1	27	102	LFET	ВС	ВС	0.152		27	102	PAUT	BC	BC	R < 0	0.160	27	101	10	14	48	140	5-UD-A-6-27-101-1	1	PP
	5-UD-A-6-32-1	UD	Α	6	2	32	1	LFET	BC	BC	0.174		32	1	PAUT	BC	ВС		0.160	25	4	8	8	32	64	5-UD-A-6-25-4-2	2	PP
	5-UD-A-6-27-102	UD	Α	6									27	102	VT	RI	RI	R		27	101	10	14	48	140	5-UD-A-6-27-101-1	1	PP
5	5-UD-A-7-4-2	UD	Α	7	1	4	2	LFET	BC	BC	0.168		4	2	PAUT	BC	BC	R < C	.160	24	5	48	10	116	480	5-UD-A-7-24-5-1	1	PP
5	5-UD-A-7-41-2	UD	Α	7	2	41	2	LFET	BC	BC	0.1		41	2	PAUT	BC	BC	R < 0	0.160	24	5	48	10	116	480	5-UD-A-7-24-5-1	1	PP
5	5-UD-A-8-7-4	UD	Α	8	1	0-15	4	LFET	BC	BC	0.17		7	4	PAUT	BC	BC	R < C	0.160	8	4	6	8	28	48	5-UD-A-8-8-4-1	1	TSPP
	5-UD-A-8-32-1	UD	Α	8	2	32	0-3	LFET	BC	BC	0.15		32	1	PAUT	BC	BC		0.160	28	4	10	8	36	80	5-UD-A-8-28-4-2	2	PP
	5-UD-A-9-18-51	UD	A	9	1	4-32	42-60	LFET	BC	BC	0.17		18	51	PAUT	BC	BC		0.160	27	49	7	20	54	140	5-UD-A-9-27-49-1	1	PP
	5-UD-A-9-10-4	UD	A	9	2	2-18	0-8	LFET	BC	BC	0.17		10	4	PAUT	BC	BC		0.160	15 15	6	31	12	86	372	5-UD-A-9-15-6-2	2	PP
	5-UD-A-9-30-5 5-UD-A-9-29-156	UD UD	Α Λ	9	3	26-34	0-10	LFET	BC	BC	0.105		30 29	5 156	PAUT VT	BC RI	BC RI	K <u< td=""><td>0.160</td><td>15 29</td><td>6 156</td><td>31 4</td><td>12 0</td><td>86 4</td><td>372</td><td>5-UD-A-9-15-6-2 5-UD-A-9-29-156-3</td><td>2</td><td>PP WR</td></u<>	0.160	15 29	6 156	31 4	12 0	86 4	372	5-UD-A-9-15-6-2 5-UD-A-9-29-156-3	2	PP WR
	5-UD-A-9-29-150 5-UD-A-10-33-6	UD	Δ	10	1	0-66	0-12	LFET	ВС	ВС	0.15		33	6	PAUT	BC	BC	R < C	0.160	23	4	28	9	74	252	5-UD-A-10-23-4-1	1	PP
	5-UD-A-15-6-84	UD	A	15	1	6	84	VT	DENT	D	0.13		6	84	VT	DENT	D	R	100	3	84	6	6	24	36	5-UD-A-15-3-84-1	1	TSPP
	5-UD-A-16-75-2	UD	Α	16	1	72-78	0-4	LFET	BC	BC	0.168		75	2	PAUT	BC	BC	R 0.	140	75	0	8	6	28	48	5-UD-A-16-75-0-1	1	TSPP
	5-UD-A-16-75-0	UD	Α	16	3	74-76	0	VT	UC	UC		0.094	75	0	VT	UC	UC	R		75	0	8	6	28	48	5-UD-A-16-75-0-1	1	TSPP
5	5-UD-A-17-22-0	UD	Α	17	1	22	0	VT	UC	UC		0.094	22	0	VT	UC	UC	R		23	0	17	0	17		5-UD-A-17-23-0-1	1	WR
5	5-UD-A-17-31-0	UD	Α	17	2	31	0	BFET	WI	WI			31	0	VT	WI	WI	R		23	0	17	0	17		5-UD-A-17-23-0-1	1	WR
5	5-UD-A-18-26-0	UD	Α	18	2	26	0	BFET	WI	WI			26	0	VT	WI	WI	R		29	0	10	0	10		5-UD-A-18-29-0-1	1	WR
5	5-UD-A-19-25-0	UD	Α	19	1	16-34	0	VT	UC	UC		0.094	25	0	VT	UC	UC	R		18	0	6	0	6		5-UD-A-19-18-0-1	1	WR
	5-UD-A-19-57-0	UD	Α	19	2	53-60	0	VT	UC	UC		0.094	57	0	VT	UC	UC	R		55	0	7	0	7		5-UD-A-19-55-0-2	2	WR
	5-UD-A-19-22-131	UD	Α	19	9	2722			2.5		2 1 2 2		22	131	VT	POR	RI	R	0.000	22	131	6	0	6	0.010	5-UD-A-19-22-131-3	3	WR
	5-UD-A-20-18-7	UD	A	20	1	0-36	7	LFET	BC	BC	0.137		18	7	PAUT	BC	BC	R <0	0.160	25	8	21	16	74	336	5-UD-A-20-25-8-1	1	PP
	5-UD-A-20-10-0 5-UD-A-20-21-0	UD	Α .	20	3	10	0	BFET	WI	WI		0.004	10	0	VT VT	WI	WI	K		10	0 0	4 5	0 0	4 5		5-UD-A-20-10-0-2 5-UD-A-20-21-0-3	2	WR
	5-UD-A-20-21-0 5-UD-A-20-30-0	UD UD	Α Δ	20 20	5	21	U	VT	UC	UC		0.094	21 30	0	VT	UC	UC UC	R		21 30	0	<i>3</i>	0	<i>3</i>		5-UD-A-20-30-0-4	3	WR WR
	5-UD-A-21-14-18	UD	Δ	21	1	10-18	7-29	LFET	BC	ВС	0.178		14	18	PAUT	BC	ВС	R < C	0.160	29	15	12	10	44	120	5-UD-A-21-29-15-1	1	PP
	5-UD-A-23-6-0	UD	A	23	1	6	0	BFET	WI	WI	0.170		6	0	VT	WI	WI	R		13	0	14	0	14	120	5-UD-A-23-13-0-1	1	WR
	5-UD-A-23-12-0	UD	Α	23	2	12	0	VT	UC	UC		0.094	12	0	VT	UC	UC	R		13	0	14	0	14		5-UD-A-23-13-0-1	1	WR
	5-UD-A-23-32-0	UD	Α	23	3	32	O	BFET	WI	WI		100,000,000,000	32	0	VT	WI	WI	R		32	0	4	0	4		5-UD-A-23-32-0-2	2	WR
5	5-UD-A-23-18-140	UD	Α	23	5	0-36	126-154	LFET	BC	BC	0.147		18	140	PAUT	BC	BC	R < C	0.160	18	150	30	12	84	360	5-UD-A-23-18-150-3	3	PP
5	5-UD-A-23-6-128	UD	Α	23	6	6	128	BFET	WI	WI			6	128	VT	WI	WI	R		6	128	8	0	8		5-UD-A-23-6-128-4	4	WR
	5-UD-A-23-23-132	UD	Α	23	7	23	132	VT	DENT	D			23	132	VT	DENT	D	R		23	132	6	6	24	36	5-UD-A-23-23-132-5	5	PP
	5-UD-A-23-0-24	UD	Α	23	1914	100	100		Section 1		NAME OF TAXABLE PARTY.		0	24	VT	RI	RI	R		0	24	0	4	4		5-UD-A-23-0-24-6	6	WR
	5-UD-A-24-1-1	UD	Α	24	1	1	1	LFET	BC	BC	0.179		1	1	PAUT	BC	BC	R < C	.160	3	4	6	8	28	48	5-UD-A-24-3-4-1	1	PP
	5-UD-A-24-0-27	UD	A	24	2	0	27	BFET	WI	WI			0	27	VT	WI	WI	K		0	27 117	10	0	10		5-UD-A-24-0-27-2	2	WR
	5-UD-A-24-0-117 5-UD-A-25-64-108	UD UD	A	24 25	2	64	108	VT	UC	UC		0.094	64	117 108	VT VT	POR UC	RI UC	R		0 64	117 108	0	4 0	4 л		5-UD-A-24-0-117-3 5-UD-A-25-64-108-1	5 1	WR WR
	5-UD-A-25-64-108 5-UD-A-25-4-0	UD	Δ	25 25	Z	04	100	VI	UC	UC		0.034	4	0	VT	UC	UC	R		04 Д	0	8	0	8		5-UD-A-25-64-108-1 5-UD-A-25-4-0-2	2	WR
	5-UD-A-25-81-102	UD	A	25									81	102	VT	RI	RI	R		81	102	0	4	4		5-UD-A-25-81-102-3	3	WR
	5-UD-A-26-30-5	UD	A	26	1	24-36	0-10	LFET	ВС	ВС	0.129		30	5	PAUT	BC	BC	R < 0	0.160	28	5	8	10	36	80	5-UD-A-26-28-5-1	1	PP
	5-UD-A-26-20-71	UD	Α	26	2	7-34	45-97	LFET	BC	BC	0.138		20	71	PAUT	BC	BC		0.160	23	72	19	60	158		5-UD-A-26-23-72-2	2	PP
	5-UD-A-26-34-127	UD	Α	26	3	34	122-132	BFET	WI	WI			34	127	VT	WI	WI	R		34	127	0	12	12		5-UD-A-26-34-127-3	3	WR
5	5-UD-A-27-28-36	UD	Α	27	2	28	36	VT	DENT	D			28	36	VT	DENT	D	R		28	36	6	6	24	36	5-UD-A-27-28-36-1	1	PP
5	5-UD-A-27-6-68	UD	Α	27	3	2-10	60-76	LFET	BC	BC	0.158		6	68	PAUT	ВС	BC	R < C	0.160	7	65	14	22	72	308	5-UD-A-27-7-65-2	2	PP
	5-UD-A-27-28-0	UD	Α	27									28	0	VT	UC	UC	R		28	0	4	0	4		5-UD-A-27-28-0-3	3	WR
	5-UD-A-28-42-43	UD	Α	28									42	43	VT	LOF	LOF	R		42	43	4	0	4		5-UD-A-28-42-43-1	1	WR
	5-UD-A-33-25-156	UD	Α	33									25	156	VT	RI	RI	R		25	156	4	0	4		5-UD-A-33-25-156-1	1	WR
	5-UD-A-33-31-139	UD	A	33									31	139	VT	RI	RI	R		31	139	0	4	4		5-UD-A-33-31-139-2	2	WR
	5-UD-A-34-67-139	UD	A	34	_	4.0	40.5				0.40		67	139	VT	POR	RI	R	454	67	139	4	0	4	20.27	5-UD-A-34-67-139-1	1	WR
	5-UD-A-36-12-134	UD	A	36 26	1	12	134	LFET	BC	BC	0.18		12	134	PAUT	BC	BC		154	13	127	6	6	37.7 27.7		5-UD-A-36-13-127-1	1	PP
	5-UD-A-36-22-128 5-UD-A-37-36-142	UD UD	A A	36 37	2	22 36-37	128 142	LFET VT	BC DENT	BC D	0.178	0.06	22 36	128 142	PAUT VT	BC DENT	BC D	R U.	114	24 36	127 142	6 6	6 6	37.7 18 849556		5-UD-A-36-24-127-2 5-UD-A-37-36-142-1	2 1	PP PP
э	J-0D-M-37-30-142	UD	A	31	1	30-37	142	VI	DENT	D	I I	0.06	30	142	VI	DEINT	D	18		30	142	O	O	10.049336	20.2/433	J-UD-M-37-30-142-1	1	rr

Control Cont	General Tank Info	Shell Loca	cation				TesT	Гех NDE							EEI PRO	/E UP							1	Recommend	ed Repairs	i		Repair
5 School-School 1	90	General Loc	ocation	ation ID	200	The state of the s	TesTe	ex NDE		s (in)	opside n(in)	dication:)	dication:	pc	Туре	1ED N TYPE		hickness	(in)	Repair:	Repair:	Oia (in)	(in)	eld	(sq in)		on Plate	(Patch, ther)
Second Content of the content of t	A Overall ID	- 0	Course Plate Number	TesTex Indic on Pla	8		Method	Indication Type		= •	Depth of T Indicatio	o ×	Center of In	Meth	Indication	SIMPLIF	E Sch	E I	Depth	enter	nter	0	Height	of	of l	EEI repair No.	air No.	Repair Type (Patc Weld, Other)
5 - Sub-Assesser 7 00																_	R					-	-		28.27433			PP
5 SULPH-REPAIR DU D. A. 40 5 2 22 3 W UP D. P. C. S.			200,0000		20	0.7	V.CT	TC	TC		0.425				0.00		R					4	_					WR
5 Sub-Ad-Al-2-Sin				1				100000	11204		0.125						R				8/	1	-	_				WR WR
5 Subschedules Un A 48				1		100			100					2 15			R				10	18	-					WR
5 SUD-A-SE-SIZE UD A 45 SUD-A-SE-SIZE UD A 46 SUD-A-SE-SIZE UD A 5 SUD-A				-	20	10		1011									R						_					WR
\$ \$ \$100.453-150 \$100 \$100 \$4 \$40 \$50 \$1 \$100.450 \$150 \$100 \$100 \$40 \$100 \$100 \$40 \$100 \$100												5			RI		R			5		4	0	4			_	WR
5 SLDA-543500 LD A 50	5 5-UD-A-48-10-0	UD A	48									10	0	VT	UC	UC	R			10	0	4	0	4		5-UD-A-48-10-0-1	1	WR
5 SUD-AS-25-255 00 A 5 51 5 SUD-AS-25-255 00 A 5 51 5 SUD-AS-25-256 00 A 5 51 5 SUD-AS-25-256 00 A 5 52 5 SUD-AS-25-256 00	5 5-UD-A-49-13-0	UD A	49									13	0	VT	UC	UC	R		0.125	13	0	7	0	7		5-UD-A-49-13-0-1	1	WR
5 SLDA-50-7-7-46 UD A 52 I 5 SLDA-50-7-7-1-46 UD A 52 I 5 SLDA-50-7-1-46 UD A 62 I 5 SLD	5 5-UD-A-50-18-0	UD A	50		PATE 1740				The second second			18	0	VT	UC	UC	R			18	0	9	0	9		5-UD-A-50-18-0-1	1	WR
\$ 54,045,474.46 UD A 52 54,045,474.46 UD A 52 54,045,474.46 UD A 52 54,045,474.46 UD A 52 54,045,474.46 UD A 54 1 2 154 VT POB P 0.05 GB 10 UD A 54 1 2 154 VT POB P 0.05 GB 110 VT INT INT ID B 1 B 1 B 2 2 GB SUDA, 50,074.56 I 1 I 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				1	19-30	130-140	LFET	BC	BC	0.15							R	0.159					-		48			PP
5 S-UD-ASS-2-15 UD A 55 1 1 2 154 VT FOR P P C 2 156 VT FOR P P C 2 157 VT FOR B B 2 2 158 4 0 4 S-UD-ASS-2-1564 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1																	R				_		_					WR
5 SUDA-SE-2156 UO D A 54 31 109 1300 VT DENT D C C C C C C C C C C C C C C C C C C																	R				5051		100					WR
5 S-UD-ASS-94-120 UO A 55 UD ASS-94-120 UO A 55 UD ASS-95-120 UO A 50 UD A 55 UD ASS-95-120 UO A 50 UD A 50				1	2	154	VT	DOD	D			42					K D			42	-	18						WR WR
5 S-UD-ASS-\$19 UO A 55 S-UD-ASS-\$219 UO A 57 S-UD-ASS-\$219 UO A 57 S-UD-ASS-\$219 UO A 58 S-UD-ASS-\$219 UO A 59 S-UD-ASS-\$219 UO A 50				1	109			Mark Construction of the Construction			0.05	69					R			69		8		•	64			PP
S 5 UDA 658379 UD A 55 5 5 UDA 659379 UD A 55 5 UDA 659379 UD A 58 5 UDA 659379 UD A 59 5 UDA				•	103	150	VI	DEIVI			0.03					1	R					J			04		_	WR
5 S-UDA-570-358																	R				_							WR
5 S.LDA-Sh-84-64 6 UD A 58 5 LDA-Sh-84-64 6 UD A 58 5 LDA-Sh-553 46 UD A 58 5 LDA-Sh-553 46 UD A 58 5 LDA-Sh-553 46 UD A 58 5 LDA-Sh-561-6317 UD A 60 D 1 13-20 147 UET BC BC BC 0.174 126 117 PAUT BC BC BC B B 0.119 19 146 9 9 3 36 81 5 UD-Sh-60-1946 1 1 1 5 5 LDA-Sh-62-45 UD A 61 1 63-75 142-149 1FT BC BC BC 0.14 66 34 6 14 21 70 299 5 UD-Sh-61-63-61 1 1 5 5 LDA-Sh-62-45 UD A 61 1 63-75 142-149 1FT BC BC BC 0.14 66 34 6 14 21 70 299 5 UD-Sh-61-63-61 1 1 1 5 5 LDA-Sh-62-45 UD A 61 1 63-75 142-149 1FT BC BC BC 0.14 66 34 6 14 21 70 299 5 UD-Sh-61-63-61 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			10000000									0.00		VT			R					10	0	10			4	WR
5 S.UDA-685346 UD A 58 I 1 13 26 147 LFT BC BC D.174 SUDA-685346 UD A 60 D 1 13 26 147 LFT BC BC D.174 SUDA-68510-10-1 UD A 60 D 5 S-UDA-68510-10-1 UD A 60 D 5 S-UDA-6852-10-1 UD A 60 D 5 S-UDA-6852-10-1 UD A 60 D 5 S-UDA-6852-10-1 UD A 60 D 7 S-UDA-682-10-1 UD A 60 D 7	5 5-UD-A-57-0-156	UD A	57									0	156	VT	RI	RI	R			0	156	2	0	2		5-UD-A-57-0-156-1	1	WR
5 5-UDA-6-0-16-147 UD A 60 1 1 32.0 147 IFIT BC 0C 0.74	5 5-UD-A-58-46-46	UD A	58									46	46	VT	LOF	LOF	R			46	46	3	0	3		5-UD-A-58-46-46-1	1	WR
5 S-UD-A-69-1-0-0 UD A 60 1 5 S-UD-A-69-1-0-0-2 UD A 60 1 5 S-UD-A-69-1-0-0-2 UD A 61 1 65-75 142-1489 LIFE BC BC D.14 66 PAUT BC BC BC B D.14 66 PAUT BC BC BC B D.14 66 PAUT BC BC BC B D.14 BC PAUT BC BC BC B D.15 148 LIFE BC BC D.15 148 LIFE BC BC D.15 15 S-UD-A-69-1-0-0-1 D S-UD-A-69-1-0-0-0-1 D S-UD-A-69-1-0-0-1 D S-UD-A	5 5-UD-A-58-53-46	UD A	58									53	46	VT	RI	RI	R			53	46	2	0	2		5-UD-A-58-53-46-2	2	WR
5 5-U0-A-60-22-45 UD A 60 1 1 63-75 142-149 LET BC BC 0.14 69 31-6 PAUT BC BC BC 0.15 S-U0-A-60-46-77 UD A 61 1 63-75 142-149 LET BC BC 0.14 69 31-6 PAUT BC BC BC BC BC 0.15 S-U0-A-60-46-72 UD A 61 1 0 4 154 LET BC BC 0.19 70 0 VT UC UC B 7 0.0 6 0 15 S-U0-A-61-46-72 2 V			10000000	1	13-20	147	LFET	BC	BC	0.174		16	147				R	0.119			146	9	9		81			PP
5 5-UD-A-01-69-1-06 UID A 61 2 5-UD-A-01-69-1-06 UID A 61 2 5-UD-A-01-69-1-06 UID A 62 5-UD-A-01-69-1-06 UID A 62 5-UD-A-01-69-1-06 UID A 64 5-UD-A-01-69-1-06 UID A 64 5-UD-A-01-69-1-06 UID A 64 5-UD-A-01-69-1-06 UID A 64 5-UD-A-01-69-1-06 UID A 65 12 5-UD-A-01-69-1-06 UID A 68 5-UD-A-01-69-1-06 UID A 70 5-UD-A-01-69																	R				_	5	_					WR
5 SUD-A61-46-7 UD A 61				21	100 000	4.0 4.0				2.22				0.10			R	0.445				-	-	_				WR
5 S-UD-A-67-27-0 UD A 62 S UD-A-67-27-0 UD A 62 S UD-A-67-27-0 UD A 62 S UD-A-68-2-15-1 UD A 62 S UD-A-68-2-15-1 UD A 68 S UD-A-68-2-15-1 UD A 70 S UD-A-71-2-5-1 UD A 71 S UD-A-71-2-5-1				1	63-75	142-149	LFET	BC	BC	0.14							R	0.145							294			PP
5 S-UD-A64-70-0 UD A 664 5 UD A 665 5 UD A667-2154 UD A 665 5 UD A667-2154 UD A 665 5 UD A667-2154 UD A 666 1 25-29 154 LEFT BC 8C 0.181 2 154 PAUT BC 8C 8 <0.160 2 7 154 PAUT BC 8C 8 <0.160 2 7 152 6 8 2 8 8 S-UD-A68-31-53-1 1 5 S-UD-A68-31-73 UD A 68 5 UD A-864-130 UD A 68 5 UD A-864-130 UD A 68 7 1 7 4 5-6 LEFT BC 8C 0.135 5 S-UD-A68-31-73 UD A 68 5 S-UD-A68-31-73 UD A 70 5 S-UD-A70-74-5 UD A 71 5 S-UD-A70-74-5 UD A 70 6 8 156 VI CL IF R 8 8 156 27 0 27 5 S-UD-A70-74-5 UD A 71 5 S-UD-A70-74-5 UD A 71 5 S-UD-A70-74-5 UD A 71 5 S-UD-A71-14-5 UD A 71 5												- 12 T					K D						200					WR WR
S S-UDA-66-27-154 UD A 66 1 25-29 154 LFET BC BC 0.19 27 154 PAUT BC BC R <0.160 3 153 6 6 24 36 S-UDA-66-27-152-1 1 1 5 S-UDA-70-68-153-1 1 1 5 S-UDA-70-68-153-1 1 1 5 S-UDA-70-68-153-1 1 1 5 S-UDA-70-68-156 UD A 70 1 1 74 5-6 LFET BC BC BC 0.135																	R				-		=					WR
5 S-UD-A-66-27-154 UD A 668 1				1	0-4	154	LEFT	BC	BC	0.19		2	_				R	< 0.160		3	_	_	_		36			PP
5 S-UDA-68-4-130 UD A 68 5 S-UDA-68-31-73 UD A 68 5 S-UDA-68-31-73 UD A 68 5 S-UDA-70-74-5 UD A 70 1 74 5-6 LFET BC BC 0.135 5 S-UDA-70-74-5 UD A 70 1 1 74 5-6 LFET BC BC 0.135 5 S-UDA-70-68-156 UD A 70 5 S-UDA-70-68-156 UD A 71 1 1 15-18 145-146 VT DENT D B 0.187 5 S-UDA-70-74-5 UD A 71 5 S-UDA-70-74-5 UD A 71 5 S-UDA-70-74-5 UD A 71 5 S-UDA-70-68-156 UD A 71 5 S-UDA-71-17-185 UD A 71 5 S-UDA-71-18-185 U			20000	1	2000000							27								27		15	15					PP
5 S-UD-A-70-74-5 UD A 70 5 S-UD-A-70-74-5 UD A 70 5 S-UD-A-71-17-145 UD A 71 1 15-18 145-146 VT DENT D BC				==	CC-10	1 TO 1 TO 1			9. 7 676			4					R			4		12			-		1	WR
5 5-UD-A-71-17-145 UD A 70												31		VT	POR		R			31		0					2	WR
5 5-UD-A-71-17-185 UD A 71 2 10-14 51-56 LFET BC BC 0.154 12 53 PAUT BC BC R 0.154 13 54 6 0 18.84956 28.2743 3-UD-A-71-18-15-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 5-UD-A-70-74-5	UD A	70	1	74	5-6	LFET	BC	BC	0.135		74	5	PAUT	BC	BC	R	0.119		78	4	9	9	36	81	5-UD-A-70-78-4-1	1	PP
5 5-UD-A-71-12-53 UD A 71	5 5-UD-A-70-68-156	UD A	70									68	156	VT	CL	IF	R			68	156	27	0	27		5-UD-A-70-68-156-2	2	WR
5 5-UDA-71-12-5-54 UD A 71 5 5-UDA-71-13-156		UD A	71	1	15-18			DENT	D		0.187	17	145	VT	DENT	D	R			17	145	8	8	32	64	5-UD-A-71-17-145-1	1	PP
5 5-UD-A-71-15-156 UD A 71 5 5-ER-4-2-150-23 ER 4 2 1 150 23 LFET BC BC 0.184 5 5-ER-4-2-150-23 ER 4 2 2 180-210 1-24 LFET BC BC 0.157 5 -ER-4-2-101-15 ER 4 15 5 -ER-4-5-41-19 ER 4 5 5 -ER-4-15-17-15 ER 4 16 5 -ER-3-15-16-28 ER 3 5 5 -ER-3-5-13-6-58 ER 3 5 5 -ER-3-5-13-6-58 ER 3 5 5 -ER-3-15-12-20-57 ER 3 15 5 -ER-3-15-114-49 ER 3 15 5 -ER-3-15-116-21 ER 3 15 5 -ER-3-15-116-20 ER 3 15 5 -ER-3-15-1114-9 ER 4 2 2 180-210 1-24 LFET BC BC 0.184 150				2	10-14	51-56	LFET	BC	BC	0.154							R	0.154					(=)		28.27433			PP
5 5-ER-4-2-150-23 ER 4 2 1 150 23 LFET BC BC 0.184 150 23 LFET BC BC 0.184 150 23 PAUT BC BC R 0.110 151 17 14 6 40.00 84.00 5-ER-4-2-151-17-1 1 TO 5 5-ER-4-2-200-12 ER 4 2 2 180-210 1-24 LFET BC BC 0.157 200 12 PAUT BC BC R 0.114 200 10 59 20 158.00 158.00 5-ER-4-2-200-10-2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1																	R											WR
5 5-ER-4-2-200-12 ER 4 2 2 180-210 1-24 LFET BC BC BC 0.157				4	450	22	Leer	DC	DC	0.101							R	0.440							04.00			WR
5 5-ER-4-5-41-19 ER 4 5 5 5-ER-4-15-228-16 ER 4 15 1 228 14-18 LFET BC BC 0.16 5 5-ER-4-15-228-16 ER 4 15 1 228 14-18 LFET BC BC 0.16 5 5-ER-4-16-170-15 ER 4 16 3 170 15 LFET BC BC 0.181 170 15 PAUT BC BC R 0.156 178 18 8 6 28.00 40.00 5-ER-4-15-231-17-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1																												TSPP
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5 5-ER-4-16-170-15 ER 4 16 3 170 15 LFET BC BC BC 0.181 5 5-ER-3-2-100-50 ER 3 2 1 100 50 LFET BC BC BC 0.197 100 50 PAUT BC BC R 0.156 178 18 8 6 28.00 48.00 5-ER-4-16-178-18-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				1	228	14-18	LEFT	BC	BC	0.16							R	0.139					100		40.00			PP
5 S-ER-3-2-100-50 ER 3 2 1 100 50 LFET BC BC 0.197 5 S-ER-3-5-31-59 ER 3 5 5																	R						-					PP
5 5-ER-3-5-31-59 ER 3 5 5 5-ER-3-5-136-58 ER 3 5 5 5-ER-3-8-26-28 ER 3 8 1 26 28 VT TS TS TS 0.094 26 28 VT DENT D R 26 28 6 0 18.85 28.27 5-ER-3-8-26-28-1 1 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 257 4 0 4 5-ER-3-12-202-57-1 1 VR 20 20 257 VT LOF LOF R 20 20 20 20 257 VT LOF LOF R 20 20 20 20 257 VT LOF LOF R 20 20 20 20 20 20 20 20 20 20 20 20 20																	R					=	-					PP
5 5-ER-3-5-136-58 ER 3 5 5 5-ER-3-8-26-28 ER 3 5 5 5-ER-3-8-26-28 ER 3 8 1 26 28 VT TS TS TS D.0.094 D				17 1	(FICE)	10717		(Telfal	(CE)ES								R					5						WR
5 5-ER-3-8-26-28 ER 3 8 1 26 28 VT TS TS TS D.094 26 28 VT DENT D R 26 28 6 0 18.85 28.27 5-ER-3-8-26-28-1 1 5 5-ER-3-12-202-57 ER 3 12 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 4 0 4 5-ER-3-12-202-57-1 1 V 202 57 VT LOF LOF R 202 57 VT LOF												0.000					R					4	0					WR
5 5-ER-3-14-142-14 ER 3 14 2 142 14 LFET BC BC 0.187 142 14 PAUT BC BC R 0.150 147 16 12 12 48.00 144.00 5-ER-3-14-147-16-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 5-ER-3-8-26-28		8	1	26	28	VT	TS	TS		0.094			VT	DENT		R			26	28	6	0	18.85	28.27	5-ER-3-8-26-28-1		PP
5 5-ER-3-15-120-21 ER 3 15 1 96-144 5-38 LFET BC BC 0.19 120 21 PAUT BC BC R 0.139 116 20 34 30 128.00 1020.00 5-ER-3-15-116-20-1 1 5 5-ER-3-15-114-49 ER 3 15 2 114 47-52 LFET BC BC 0.16 114 49 PAUT BC BC R 0.160 111 48 13 10 46.00 130.00 5-ER-3-15-111-48-2 2	5 5-ER-3-12-202-57	ER 3	12									202	57	VT	LOF	LOF	R			202	57	4	0	4		5-ER-3-12-202-57-1	1	WR
5 5-ER-3-15-114-49 ER 3 15 2 114 47-52 LFET BC BC 0.16 114 49 PAUT BC BC R 0.160 111 48 13 10 46.00 130.00 5-ER-3-15-111-48-2 2	5 5-ER-3-14-142-14	ER 3	14	2	1			BC	BC	0.187		142	14	PAUT	BC		R	0.150				12		48.00	144.00	5-ER-3-14-147-16-1	1	PP
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E E E D 2 4 I 4 I 17C 20 VE TC I TC I I 2004 I 17C 20 VE COUCE C D 47C 20 4 0 4 5 5 5 5 5 6 4 7 5 6 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7				2				Property and the second	200	0.16		N. P. C. C.					R	0.160				13			130.00			PP
	5 5-ER-2-4-176-29	ER 2	4	1	176	29	VT	TS	TS		0.094	176	29	VT	GOUGE	G	R			176	29	1	0	1		5-ER-2-4-176-29-1	1	WR
												18					R			18								WR
5 5-ER-2-8-8-57 ER 2 8 8 57 VT RI RI R 8 57 4 0 4 5-ER-2-8-8-57-1 1 \	5 5-EK-2-8-8-5/	ЕК 2	8		L				I	I	L	8	5/	VI	KI	KI	К			8	5/	4	U	4		J-EK-Z-8-8-5/-1	1	WR

G	eneral Tank Info	She	ell Locat	ion				TesT	ex NDE							EEI PRO	/E UP							R	ecommend	ed Repairs	5		Repair Type
No.		Gen	eral Loca	ation	cation ID ate		Reported n Location	TesTe	ex NDE		n Wall ss (in)	of Topside cation(in)	Indication: (in)	Indication: (in)	po	n Type	FIED ON TYPE	l Indation or No	Im Thickness (in)	(in)	of Repair: (in)	of Repair: (in)	· Dia (in)	(in)	Weld (in)	PP (sq in)		on Plate	
Tank	Overall ID	Location in Tank	Shell	Plate Number	TesTex Indication ID on Plate	X Coordinate (in)	Y Coordinate (in)	Method	Indication Type	SIMPLIFIED INDICATIO N TYPE	Minimum Thickness	Depth of Indicati	Center of Ir	Center of Ir Y (i	Meth	Indication	SIMPLIFIE	EE Recomme (Repair		Depth (in)	Center of X (i	Center of Y (ii	Width or	Height (in)	Length of	Area of P	EEI repair No.	Repair No.	Repair Type (Patch, Weld, Other)
	5-ER-2-8-87-0	ER	2	8									87	0	VT	RI	RI	R			87	0	4	0	4		5-ER-2-8-87-0-2	2	WR
	5-ER-2-11-228-45	ER	2	11	1	228	45	UT	BC	BC	0.143		228	45	UT	BC	BC	R	0.139		228	45	10	10	40.00		5-ER-2-11-228-45-1	1	PP
	5-ER-2-11-228-32 5-ER-2-12-144-33	ER ER	2 2	11 12	2	228 144	32 33	UT UT	BC BC	BC BC	0.152 0.15		228 144	32 33	UT	BC BC	BC BC	K P	0.143 0.146		228 144	32 33	10 10	10 10	40.00 40.00		5-ER-2-11-228-32-2 5-ER-2-12-144-33-2	2 2	PP PP
	5-ER-2-12-167-57	ER	2	12	_	144	33	01	ВС	ВС	0.13		167	57	VT	RI	RI	R	0.140		167	57	4	0	40.00	100.00	5-ER-2-12-167-57-1	1	WR
	5-ER-2-13-126-3	ER	2	13									126	3	VT	POR	RI	R			126	3	o	4	4		5-ER-2-13-126-3-1	1	WR
	5-ER-2-15-36-33	ER	2	15	1	36	33	UT	ВС	ВС	0.158		40	41	UT	ВС	BC	R	0.145		40	34	10	24	68.00	240.00	5-ER-2-15-40-34-1	1	PP
5	5-ER-2-15-36-21	ER	2	15	2	36	21	UT	BC	BC	0.19		40	28	UT	BC	BC	R	0.144		40	34	10	24	68.00	240.00	5-ER-2-15-40-34-1	1	PP
5	5-ER-2-16-147-36	ER	2	16	3	147	31-40	LFET	BC	BC	0.188		147	36	PAUT	BC	BC	R	0.150		150	47	21	24	90.00	504.00	5-ER-2-16-150-47-1	1	PP
	5-ER-2-16-137-43	ER	2	16	4	137	34-53	LFET	BC	BC	0.14		137	43	PAUT	BC	BC	R	0.150		150	47	21	24	90.00	504.00	5-ER-2-16-150-47-1	1	PP
	5-ER-1-1-42-0	ER	1	1									42	0	VT	RI	RI	R			42	0	4	0	4		5-ER-1-1-42-0-1	1	WR
	5-ER-1-1-201-14	ER	1	1									201	14	VT	RI	RI	R			201	14	4	0	4		5-ER-1-1-201-14-2	2	WR
	5-ER-1-2-6-14 5-ER-1-2-31-14	ER	1	2									6	14	VT VT	RI RI	RI RI	K			6	14	4 5	0 0	4		5-ER-1-2-6-14-1 5-ER-1-2-31-14-2	1	WR
	5-ER-1-3-168-15	ER ER	1	3									31 168	14 15	VT	RI	RI	R			31 168	14 15	э /I	0	э /I		5-ER-1-2-31-14-2 5-ER-1-3-168-15-1	1	WR WR
	5-ER-1-4-0-10	ER	1	4	1	0	10	VT	POR	р			0	10	VT	POR	RI	R			0	10	0	4	4		5-ER-1-4-0-10-1	1	WR
	5-ER-1-4-50-15	ER	1	4	-		10		7 011				50	15	VT	RI	RI	R			50	15	4	0	4		5-ER-1-4-50-15-2	2	WR
	5-ER-1-4-143-15	ER	1	4									143	15	VT	RI	RI	R			143	15	6	0	6		5-ER-1-4-143-15-3	3	WR
5	5-ER-1-4-211-15	ER	1	4									211	15	VT	RI	RI	R			211	15	4	0	4		5-ER-1-4-211-15-4	4	WR
5	5-ER-1-4-187-15	ER	1	4									187	15	VT	RI	RI	R			187	15	4	0	4		5-ER-1-4-187-15-5	5	WR
5	5-ER-1-4-176-15	ER	1	4									176	15	VT	RI	RI	R			176	15	4	0	4		5-ER-1-4-176-15-6	6	WR
	5-ER-1-5-27-15	ER	1	5									27	15	VT	RI	RI	R			27	15	7	0	7		5-ER-1-5-27-15-1	1	WR
	5-ER-1-5-96-15	ER	1	5									96	15	VT	RI	RI	R			96	15	4	0	4		5-ER-1-5-96-15-2	2	WR
	5-ER-1-5-59-0	ER	1	5									59	0	VT	RI	RI	R			59	0	4	0	4		5-ER-1-5-59-0-3	3	WR
	5-ER-1-5-137-15 5-ER-1-6-17-15	ER ER	1	5 6									137 17	15 15	VT VT	RI RI	RI RI	K			137 17	15 15	4	0	4		5-ER-1-5-137-15-4 5-ER-1-6-17-15-1	4	WR WR
	5-ER-1-0-17-15 5-ER-1-7-22-15	ER	1	7									22	15	VT	RI	RI	R			22	15 15	4	0	4		5-ER-1-7-13-1 5-ER-1-7-22-15-1	1	WR
	5-ER-1-7-200-15	ER	1	7									200	15	VT	RI	RI	R			200	15 15	4	0	4		5-ER-1-7-200-15-2	2	WR
	5-ER-1-8-62-0	ER	1	8									62	0	VT	RI	RI	R			62	0	4	0	4		5-ER-1-8-62-0-1	1	WR
	5-ER-1-9-107-14	ER	1	9									107	14	VT	RI	RI	R			107	14	6	0	6		5-ER-1-9-107-14-1	1	WR
5	5-ER-1-11-98-2	ER	1	11	1	98	1-4	LFET	BC	BC	0.158		98	2	PAUT	BC	BC	R	< 0.160		99	8	28	12	80.00	336.00	5-ER-1-11-99-8-1	1	PP
5	5-ER-1-14-64-13	ER	1	14									64	13	VT	RI	RI	R			64	13	4	0	4		5-ER-1-14-64-13-1	1	WR
	5-ER-1-14-73-13	ER	1	14									73	13	VT	RI	RI	R			73	13	4	0	4		5-ER-1-14-73-13-2	2	WR
	5-BA-28-1-43-31	BA	28	1									43	31	VT	RI	RI	R			43	31	4	0	4		5-BA-28-1-43-31-1	1	WR
	5-BA-28-2-154-30	BA	28	2	3	154	30	VT	POR	Р			154	30	VT	LOF	LOF	R			154	30	8	0	8		5-BA-28-2-154-30-1	1	WR
	5-BA-28-3-36-31 5-BA-28-3-189-31	BA	28	3									36	31	VT VT	LOF RI	LOF RI	K			36 180	31 31	4	0 0	4		5-BA-28-3-36-31-1 5-BA-28-3-189-31-2	1 2	WR
	5-BA-28-3-189-31 5-BA-28-6-188-30	BA BA	28 28	3 6	1	188	30	VT	POR	p			189 188	31 30	VT	POR	RI	R			189 188	30	4	0	4 1		5-BA-28-3-189-31-2 5-BA-28-6-188-30-1	Z 1	WR WR
	5-BA-28-6-122-30	BA	28	6	1	100	30	VI	FUN				122	30	VT	RI	RI	R			122	30	4	0	4		5-BA-28-6-122-30-2	2	WR
	5-BA-28-7-0-28	BA	28	7									0	28	VT	RI	RI	R			0	28	0	4	4		5-BA-28-7-0-28-1	1	WR
	5-BA-28-7-53-30	BA	28	7									53	30	VT	RI	RI	R			53	30	14	0	14		5-BA-28-7-53-30-2	2	WR
	5-BA-28-7-89-30	ВА	28	7									89	30	VT	UF	IF	R			89	30	11	0	11		5-BA-28-7-89-30-3	3	WR
5	5-BA-28-7-204-30	BA	28	7									204	30	VT	RI	RI	R			204	30	4	0	4		5-BA-28-7-204-30-4	4	WR
	5-BA-28-8-104-30	BA	28	8									104	30	VT	LOF	LOF	R			104	30	5	0	5		5-BA-28-8-104-30-1	1	WR
	5-BA-28-8-131-30	BA	28	8									131	30	VT	RI	RI	R			131	30	4	0	4		5-BA-28-8-131-30-2	2	WR
	5-BA-28-8-143-30	BA	28	8									143	30	VT	RI	RI	R			143	30	4	0	4		5-BA-28-8-143-30-3	3	WR
	5-BA-28-8-181-30	BA	28	8									181	30	VT	RI	RI	R			181	30	4	0	4		5-BA-28-8-181-30-4	4	WR
	5-BA-28-8-238-30	BA	28	8	1	170	-1	VT	DOD	р			238	30	VT	RI	RI	K			238	30 1	11	0	11		5-BA-28-8-238-30-5	5 1	WR
	5-BA-28-9-176-1 5-BA-28-12-210-0	BA BA	28	9 12	1	176	1	VT	POR				176 210	1 0	VT VT	POR UF	RI IF	K			176 210	0	4 5	0 0	4 5		5-BA-28-9-176-1-1 5-BA-28-12-210-0-1	1	WR WR
	5-BA-28-12-210-0 5-BA-28-13-166-0	BA BA	28 28	12 13									210 166	0	VT	RI	IF RI	R			210 166	0	э //	0	э /I		5-BA-28-12-210-0-1 5-BA-28-13-166-0-1	1	WR WR
	5-BA-28-13-166-0 5-BA-28-13-230-0	BA	28	13									230	0	VT	RI	RI	R			230	0	4	0	4		5-BA-28-13-166-0-1 5-BA-28-13-230-0-2	2	WR
	5-BA-28-16-150-0	BA	28	16									150	0	VT	RI	RI	R			150	0	2	0	2		5-BA-28-16-150-0-1	1	WR
	5-BA-27-1-154-0	BA	27	1									154	0	VT	POR	RI	R			154	0	4	0	4		5-BA-27-1-154-0-1	1	WR
	5-BA-27-1-184-0	BA	27	1									184	0	VT	POR	RI	R			184	0	6	0	6		5-BA-27-1-184-0-2	2	WR
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G	eneral Tank Info	She	ell Locati	on				TesT	ex NDE							EEI PRO	/E UP							Re	ecommendo	ed Repairs	ī		Repair Type
No.		Gen	eral Loca	tion	TesTex Indication ID on Plate	TexTex F	n Location	TesTe	ex NDE		n Wall ss (in)	of Topside cation(in)	Indication: (in)	Indication: (in)	poi	n Type	FIED ON TYPE	ndation or No Thickness	(in)	of Repair:	(iii)	of Repair: (in)	Dia (in)	t (in)	Weld (in)	PP (sq in)		on Plate	
Tank	Overall ID	Location in Tank	Shell Course	Plate Number	TesTex Ind on Pl	X Coordinate (in)	γ Coordinate (in)	Method	Indication Type	SIMPLIFIED INDICATIO N TYPE	Minimum Thickness	Depth of Indicati	Center of II	Center of II Y (i	Meth	Indication	SIMPLIFIE	Recomme (Repair Minimum	(in)	Center of	*	Center of Y (i	Width or Dia (in)	Height (in)	Length of	Area of P	EEI repair No.	Repair No.	Repair Type (Patch, Weld, Other)
	5-BA-27-1-234-0	BA	27	1									234	0	VT	CL	IF	R		23		0	6	0	6		5-BA-27-1-234-0-3	3	WR
	5-BA-27-2-24-0 5-BA-27-2-36-0	BA BA	27 27	2									24 36	0	VT VT	RI RI	RI RI	R R		2. 3		0 0	4 5	0	4 5		5-BA-27-2-24-0-1 5-BA-27-2-36-0-2	2	WR WR
	5-BA-27-2-105-0	BA	27	2									105	0	VT	POR	RI	R		10		0	4	0	4		5-BA-27-2-105-0-3	3	WR
	5-BA-27-6-123-0	ВА	27	6									123	0	VT	RI	RI	R		12		0	4	0	4		5-BA-27-6-123-0-1	1	WR
5	5-BA-27-9-0-54	BA	27	9									0	54	VT	RI	RI	R		C		54	0	4	4		5-BA-27-9-0-54-1	1	WR
5	5-BA-27-12-115-36	BA	27	12									115	36	UT	BC	BC	R 0.	148	11	5	36	10	10	40.00	100.00	5-BA-27-12-115-36-1	1	PP
5	5-BA-27-14-158-52	BA	27	14	1	158	52	LFET	BC	BC	0.146		158	52	PAUT	BC	BC	R 0.	119	15	8	52	6	6	24.00	36.00	5-BA-27-14-158-52-1	1	TSPP
	5-BA-27-16-94-0	BA	27	16									94	0	VT	RI	RI	R		9.		0	4	0	4		5-BA-27-16-94-0-1	1	WR
	5-BA-26-3-83-0	BA	26	3									83	0	VT	RI	RI	R		8		0	4	0	4		5-BA-26-3-83-0-2	2	WR
	5-BA-26-4-30-0	BA	26	4									30	0	VT	RI RI	RI RI	R		3		0	2	0	2		5-BA-26-4-30-0-1 5-BA-26-5-150-0-1	1	WR
	5-BA-26-5-150-0 5-BA-26-7-150-0	BA BA	26 26	5 7									150 150	0	VT VT	RI	RI RI	R		15 15		0	2	0	3		5-BA-26-7-150-0-1	1	WR WR
	5-BA-26-8-121-0	BA	26	8									121	0	VT	RI	RI	R		12		0	4	0	4		5-BA-26-8-121-0-1	1	WR
	5-BA-26-8-210-0	BA	26	8									210	0	VT	LOF	LOF	R		21		0	0	3	3		5-BA-26-8-210-0-2	2	WR
	5-BA-26-10-0-59	ВА	26	10									0	59	VT	RI	RI	R		C		59	0	4	4		5-BA-26-10-0-59-1	1	WR
5	5-BA-26-16-150-0	BA	26	16									150	0	VT	RI	RI	R		15	0	0	4	0	4		5-BA-26-16-150-0-1	1	WR
5	5-BA-25-1-90-5	BA	25	1									90	5	VT	UF	IF	R		9)	5	0	5	5		5-BA-25-1-90-5-1	1	WR
	5-BA-25-2-19-0	BA	25	2									19	0	VT	RI	RI	R		1		0	4	0	4		5-BA-25-2-19-0-1	1	WR
	5-BA-25-2-102-0	BA	25	2									102	0	VT	RI	RI	R		10		0	4	0	4		5-BA-25-2-102-0-2	2	WR
	5-BA-25-4-29-1	BA	25	4									29	1	VT	RI	RI	R		2'		2	0	3	3		5-BA-25-4-29-2-1	1	WR
	5-BA-25-15-16-0	BA	25	15									16	0	VT	RI	RI	R		1		0	4	0	4		5-BA-25-15-16-0-1	1	WR
	5-BA-24-2-134-0 5-BA-24-5-150-0	BA BA	24 24	2 5									134 150	0	VT VT	UC POR	UC RI	K D		13 15		0	1	0 0	1		5-BA-24-2-134-0-1 5-BA-24-5-150-0-1	1	WR WR
	5-BA-24-8-93-0	BA	24	8									93	0	VT	RI	RI	R		9		0	4	0	4		5-BA-24-8-93-0-1	1	WR
	5-BA-24-12-30-0	BA	24	12									30	0	VT	RI	RI	R		3		0	6	0	6		5-BA-24-12-30-0-1	1	WR
	5-BA-24-14-2-0	BA	24	14									2	0	VT	RI	RI	R		2		0	4	0	4		5-BA-24-14-2-0-1	1	WR
	5-BA-23-2-171-0	ВА	23	2									171	0	VT	RI	RI	R		17	1	0	4	0	4		5-BA-23-2-171-0-1	1	WR
5	5-BA-23-3-220-0	BA	23	3									220	0	VT	LOF	LOF	R		22	0	0	4	0	4		5-BA-23-3-220-0-2	2	WR
5	5-BA-23-6-211-0	BA	23	6									211	0	VT	RI	RI	R		21	1	0	3	0	3		5-BA-23-6-211-0-1	1	WR
5	5-BA-23-11-42-3	BA	23	11									42	3	VT	RI	RI	R		4	!	3	4	0	4		5-BA-23-11-42-3-1	1	WR
	5-BA-23-13-191-7	BA	23	13									191	7	VT	RI	RI	R		19		7	0	3	3		5-BA-23-13-191-7-1	1	WR
	5-BA-23-16-211-0	BA	23	16									211	0	VT	LOF	LOF	R		21		0	4	0	4		5-BA-23-16-211-0-1	1	WR
	5-BA-22-8-47-0 5-BA-22-13-150-0	BA	22	8									47 150	0	VT VT	RI RI	RI RI	K		4		0 0	4	0 0	4 3		5-BA-22-8-47-0-1 5-BA-22-13-150-0-1	1	WR
	5-BA-22-16-90-0	BA BA	22 22	13 16									150 90	0	VT	RI	RI	R		15 9		0	2	0	2		5-BA-22-16-90-0-1	1	WR WR
	5-BA-21-1-40-41	BA BA	21	1									40	41	VT	GOUGE	G	R		4		41	1	0	1		5-BA-22-16-90-0-1 5-BA-21-1-40-41-1	1	WR
	5-BA-21-1-90-3	BA	21	1									90	3	VT	UF	IF	R		9		3	0	2	2		5-BA-21-1-90-3-2	2	WR
	5-BA-21-4-89-0	ВА	21	4									89	0	VT	RI	RI	R		8		0	0	3	3		5-BA-21-4-89-0-1	1	WR
5	5-BA-21-5-173-0	BA	21	5									173	0	VT	RI	RI	R		17	3	0	4	0	4		5-BA-21-5-173-0-1	1	WR
5	5-BA-21-9-148-0	BA	21	9									148	0	VT	RI	RI	R		14	8	0	4	0	4		5-BA-21-9-148-0-1	1	WR
	5-BA-21-10-1-27	BA	21	10	1	1	26-27	VT	LOF	LOF			1	27	VT	LOF	LOF	R		1		27	4	0	4		5-BA-21-10-1-27-1	1	WR
	5-BA-21-15-144-0	BA	21	15									144	0	VT	RI	RI	R		14		0	0	4	4		5-BA-21-15-144-0-1	1	WR
	5-BA-20-2-15-0	BA	20	2									15	0	VT	RI	RI	R		1		0	4	0	4		5-BA-20-2-15-0-1	1	WR
	5-BA-20-2-92-0	BA	20	2									92	0	VT	RI	RI	K		10		0	4	0	4		5-BA-20-2-102-0-2	2	WR
	5-BA-20-6-150-0 5-BA-20-6-209-0	BA BA	20 20	6 6									150 209	0	VT VT	RI RI	RI RI	R		15 20		0 0	3 3	0	3 2		5-BA-20-6-150-0-1 5-BA-20-6-209-0-2	1 2	WR WR
	5-BA-20-7-0-33	BA BA	20	7	1	0	33	VT	POR	Р			0	33	VT	POR	RI	R		20		33	0	4	<i>3</i>		5-BA-20-7-0-33-1	1	WR
	5-BA-20-7-91-0	BA	20	7	_		33		7 ON				91	0	VT	RI	RI	R		9		0	4	0	4		5-BA-20-7-91-0-2	2	WR
	5-BA-20-8-147-57	BA	20	8									147	57	VT	RI	RI	R		14		57	0	4	4		5-BA-20-8-147-57-1	1	WR
	5-BA-20-14-32-0	ВА	20	14									32	O	VT	RI	RI	R		3		0	3	О	3		5-BA-20-14-32-0-1	1	WR
5	5-BA-19-1-93-4	BA	19	1									93	4	VT	UF	IF	R		9	1	4	0	4	4		5-BA-19-1-93-4-1	1	WR
	5-BA-19-1-210-58	BA	19	1									210	58	VT	POR	RI	R		21	0	58	2	0	2		5-BA-19-1-210-58-2	2	WR
	5-BA-19-2-0-34	BA	19	2	1	0	34	LFET	WI	WI			0	34	VT	UC	UC	R		C		34	O	4	4		5-BA-19-2-0-34-1	1	WR
5	5-BA-19-2-55-0	BA	19	2		I					l		55	0	VT	RI	RI	R		5.		0	4	0	4		5-BA-19-2-55-0-2	2	WR

General Tank Info	Shell	Location				Tes	Гех NDE							EEI PRO	VE UP							R	ecommend	ed Repairs			Repair
o d	Gener	al Location	ation ID	TexTex R	teported Location	TesT	ex NDE		s (in)	of Topside cation(in)	dication:)	dication:)	pc	Type	IED N TYPE	ndation or No	Thickness (1	(in)	of Repair: (in)	of Repair: ′ (in)	·Dia (in)	(in)	/eld (in)	PP (sq in)		on Plate	Her)
Y E Overall ID	Location in Tank	Shell Course Plate Number	TesTex Indication ID on Plate	X Coordinate (in)	Y Coordinate (in)	Method	Indication Type	SIMPLIFIED INDICATIO N TYPE	Minimum Thickness	Depth of T Indicatio	Center of Ind X (in)	Center of Indi Y (in)	Method	Indication Type	SIMPLIFIED INDICATION TYPE	EF mm spair	Minimum Ti (in)	Depth (in)	Center of I	Center of R Y (in)	Width or [Height (in)	Length of W	Area of PP	EEI repair No.	Repair No.	Repair Type (Patc Weld, Other)
5 5-BA-19-5-79-0	BA	19 5									79	0	VT	RI	RI	R			79	0	4	0	4		5-BA-19-5-79-0-1	1	WR
5 5-BA-19-6-90-0 5 5-BA-19-8-130-37	BA BA	19 6 19 8	1	130	37	UT	ВС	ВС	0.155		90 130	0 37	VT UT	RI BC	RI BC	R R	< 0.160		90 130	0 37	3 10	0 10	3 40.00	100.00	5-BA-19-6-90-0-1 5-BA-19-8-130-37-1	1 1	WR PP
5 5-BA-19-10-126-38	BA	19 10	1	126	38	UT	BC	BC	0.151		126	38	UT	BC	BC		< 0.160		126	38	10	10	40.00		5-BA-19-10-126-38-1	1	PP
5 5-BA-19-14-136-38	ВА	19 14	1	136	38	UT	ВС	ВС	0.155		136	38	UT	ВС	ВС		< 0.160		136	38	10	10	40.00		5-BA-19-14-136-38-1	1	PP
5 5-BA-19-16-90-0	BA	19 16									90	0	VT	RI	RI	R			90	0	2	0	2		5-BA-19-16-90-0-1	1	WR
5 5-BA-19-16-223-0	BA	19 16									223	0	VT	UF	IF	R			223	0	3	0	3		5-BA-19-16-223-0-2	2	WR
5 5-BA-18-2-211-58	BA	18 2									211	58	VT	RI	RI	R			211	58	2	0	2		5-BA-18-2-211-58-2	2	WR
5 5-BA-18-7-41-0	BA	18 7									41	0	VT	RI	RI	R			41	0	4	0	4		5-BA-18-7-41-0-1	1	WR
5 5-BA-18-8-90-0	BA	18 8									90	0	VT	UF	IF LOT	R			90	0	3	0	3		5-BA-18-8-90-0-1	1	WR
5 5-BA-18-10-210-0	BA BA	18 10 18 11									210 232	0	VT VT	LOF RI	LOF RI	K P			210 232	0	4	0 0	4 4		5-BA-18-10-210-0-1 5-BA-18-11-232-0-1	1 1	WR WR
5 5-BA-18-11-232-0 5 5-BA-17-1-90-4	BA	17 1									90	4	VT	UF	IF	R			90	4	4	0	3		5-BA-17-1-90-4-2	2	WR
5 5-BA-17-2-89-0	BA	17 1									89	0	VT	RI	RI	R			89	0	0	3	3		5-BA-17-1-90-4-2 5-BA-17-2-89-0-2	2	WR
5 5-BA-17-6-150-0	BA	17 6	1	150	0	VT	POR	Р			150	0	VT	POR	RI	R			150	0	6	0	6		5-BA-17-6-150-0-1	1	WR
5 5-BA-16-5-209-0	ВА	16 5									209	0	VT	LOF	LOF	R			209	0	0	3	3		5-BA-16-5-209-0-1	1	WR
5 5-BA-16-7-29-0	BA	16 7									29	0	VT	RI	RI	R			29	0	4	0	4		5-BA-16-7-29-0-1	1	WR
5 5-BA-16-11-20-0	BA	16 11									20	0	VT	RI	RI	R			20	0	4	0	4		5-BA-16-11-20-0-1	1	WR
5 5-BA-15-6-114-0	BA	15 6									114	0	VT	LOF	LOF	R			114	0	4	0	4		5-BA-15-6-114-0-1	1	WR
5 5-BA-15-7-218-0	BA	15 7									218	0	VT	LOF	LOF	R			218	0	6	0	6		5-BA-15-7-218-0-1	1	WR
5 5-BA-14-6-211-0	BA	14 6									211	0	VT	RI	RI	R			211	0	3	0	3		5-BA-14-6-211-0-1	1	WR
5 5-BA-14-10-150-0 5 5-BA-14-12-86-0	BA BA	14 10 14 12									150 86	0	VT VT	RI RI	RI RI	K D			150 86	0	4	0	4 4		5-BA-14-10-150-0-1 5-BA-14-12-86-0-1	1 1	WR WR
5 5-BA-14-13-102-60	BA	14 12	1	102	60	VT	POR	Р			102	60	VT	POR	RI	R			102	60	4	0	4		5-BA-14-13-102-60-1	1	WR
5 5-BA-14-14-210-0	BA	14 14	*	102	00	VI	TON				210	0	VT	RI	RI	R			210	0	2	0	2		5-BA-14-14-210-0-1	1	WR
5 5-BA-13-1-90-5	BA	13 1									90	5	VT	UF	IF	R			90	5	4	0	4		5-BA-13-1-90-5-1	1	WR
5 5-BA-13-4-155-0	ВА	13 4									155	0	VT	RI	RI	R			155	0	3	0	3		5-BA-13-4-155-0-1	1	WR
5 5-BA-13-7-210-0	BA	13 7									210	0	VT	RI	RI	R			210	0	0	4	4		5-BA-13-7-210-0-1	1	WR
5 5-BA-13-11-108-1	BA	13 11	1	108	1	VT	POR	P			108	1	VT	POR	RI	R			108	1	4	0	4		5-BA-13-11-108-1-1	1	WR
5 5-BA-13-13-89-0	BA	13 13									89	0	VT	RI	RI	R			89	0	0	4	4		5-BA-13-13-89-0-1	1	WR
5 5-BA-12-8-37-0	BA	12 8									37	0	VT	LOF	LOF	R			37	0	8	0	8		5-BA-12-8-37-0-1	1	WR
5 5-BA-12-12-48-0	BA	12 12									48	0	VT	RI	RI	R			48	0	4	0	4		5-BA-12-12-48-0-1	1	WR
5 5-BA-11-4-150-0	BA	11 4									150	0	VT	RI	RI	K			150 150	0 0	3 4	0	3 4		5-BA-11-4-150-0-1	1	WR
5 5-BA-11-10-150-0 5 5-BA-10-2-32-1	BA BA	11 10 10 2									150 32	0 1	VT VT	RI RI	RI RI	R D			150 32	1	0	4	4		5-BA-11-10-150-0-1 5-BA-10-2-32-1-2	1 2	WR WR
5 5-BA-10-2-32-1 5 5-BA-10-11-33-60	BA	10 2	1	33	60	VT	TS	TS		0.19	33	60	VT	TS	TS	R			33	60	4	0	4		5-BA-10-2-32-1-2 5-BA-10-11-33-60-1	1	WR
5 5-BA-10-11-134-0	BA	10 11	•	33	00		, ,			0.13	134	0	VT	RI	RI	R			134	0	4	0	4		5-BA-10-11-134-0-2	2	WR
5 5-BA-9-3-220-5	ВА	9 3									220	5	VT	LOF	LOF	R			220	5	5	0	5		5-BA-9-3-220-5-1	1	WR
5 5-BA-9-4-145-0	BA	9 4									145	0	VT	RI	RI	R			145	0	2	0	2		5-BA-9-4-145-0-1	1	WR
5 5-BA-9-5-151-0	BA	9 5									151	0	VT	RI	RI	R			151	0	0	3	3		5-BA-9-5-151-0-1	1	WR
5 5-BA-9-8-208-0	BA	9 8									208	0	VT	UF	IF	R			208	0	4	0	4		5-BA-9-8-208-0-1	1	WR
5 5-BA-9-8-212-0	BA	9 8									212	0	VT	UC	UC	R			212	0	4	0	4		5-BA-9-8-212-0-2	2	WR
5 5-BA-9-9-81-1	BA	9 9									81	1	VT	RI	RI	R			81	1	4	0	4		5-BA-9-9-81-1-1	1	WR
5 5-BA-9-11-98-0	BA	9 11									98	0	VT	RI	RI	R			98	0	4	0	4		5-BA-9-11-98-0-1	1	WR
5 5-BA-8-15-140-0	BA BA	8 15 9 15									140	0	VT	RI RI	RI RI	K			140 30	0	2	0	2 2		5-BA-8-15-140-0-1 5-BA-8-15-30-0-2	1	WR
5 5-BA-8-15-30-0 5 5-BA-7-4-90-0	BA BA	8 15 7 4									30 90	0	VT VT	RI	RI RI	R			30 90	0	2 5	0 0	2 5		5-BA-8-15-30-0-2 5-BA-7-4-90-0-1	2 1	WR WR
5 5-BA-7-15-22-0	BA	7 15									22	0	VT	RI	RI	R			22	0	2	0	2		5-BA-7-4-90-0-1 5-BA-7-15-22-0-1	1	WR
5 5-BA-6-14-67-0	BA	6 14									67	0	VT	RI	RI	R			67	0	4	0	4		5-BA-6-14-67-0-1	1	WR
5 5-BA-5-6-210-0	BA	5 6									210	0	VT	RI	RI	R			210	0	3	0	3		5-BA-5-6-210-0-1	1	WR
5 5-BA-5-8-137-56	ВА	5 8	2	137	56	LFET	BC	ВС	0.184		137	56	PAUT	ВС	ВС	R	0.149		130	55	12	12	48.00	144.00	5-BA-5-8-130-55-1	1	PP
5 5-BA-5-10-22-0	BA	5 10									22	0	VT	RI	RI	R			22	0	4	0	4		5-BA-5-10-22-0-1	1	WR
5 5-BA-5-12-123-48	BA	5 12	1	123	48	UT	BC	ВС	0.155		123	48	UT	BC	BC	R <	< 0.160		123	48	10	10	40.00	100.00	5-BA-5-12-123-48-2	2	PP
5 5-BA-5-12-123-48	BA	5 12									123	48	VT	POR	RI	R			123	48	10	10	40.00	100.00	5-BA-5-12-123-48-2	2	PP
5 5-BA-4-3-120-0	BA	4 3	l								120	0	VT	UC	UC	R			120	0	12	0	12		5-BA-4-3-120-0-1	1	WR

General Tank Info	Shell Location			TesTex NDE							EEI PRO	VE UP						R	ecommend	ed Repairs			Repair Type
오 Overall ID	General Location	ex Indication ID on Plate	TexTex Reported Indication Location	TesTex NDE	ED 10 E	um Wall ess (in)	of Topside ation(in)	Indication: (in)	Indication: (in)	Method	ion Type	SIMPLIFIED INDICATION TYPE	EEI mendation air or No m Thickness (in)	Depth (in)	er of Repair: X (in)	of Repair: / (in)	or Dia (in)	Height (in)	f Weld (in)	PP (sq in)	EEI repair No.	o. on Plate	pair Type (Patch, Weld, Other)
Tan	Location i Tank Shell Course Plate	TesTex In	X Coordinat (in) Y Coordinat	Method Indication Type	SIMPLIFIE INDICATION N TYPE	Minimum	Depth of Indicati	Center of	Center of Y (Me	Indication	SIMP	Recomm (Repai Minimum	Dept	Center o	Center o	Width o	Heig	Length of	Area of I	2277696117107	Repair No.	Repair Ty Weld,
5 5-BA-4-8-77-0	BA 4 8							77	0	VT	RI	RI	R		77	0	4	0	4		5-BA-4-8-77-0-1	1	WR
5 5-BA-3-1-90-0	BA 3 1							90	0	VT	LOF	LOF	R		90	0	14	0	14		5-BA-3-1-90-0-1	1	WR
5 5-BA-3-6-210-0	BA 3 6							210	0	VT	LOF	LOF	R		210	0	3	0	3		5-BA-3-6-210-0-1	1	WR
5 5-BA-3-7-90-0	BA 3 7							90	0	VT	RI	RI	R		90	0	4	0	4		5-BA-3-7-90-0-1	1	WR
5 5-BA-3-7-198-0	BA 3 7							198	0	VT	RI	RI	R		198	0	6	0	6		5-BA-3-7-198-0-2	2	WR
5 5-BA-3-7-211-0	BA 3 7							211	0	VT	LOF	LOF	R		211	0	6	0	6		5-BA-3-7-211-0-3	3	WR
5 5-BA-3-9-210-0	BA 3 9							210	0	VT	RI	RI	R		210	0	4	0	4		5-BA-3-9-210-0-1	1	WR
5 5-BA-3-10-90-0	BA 3 10							90	0	VT	RI	RI	R		90	0	4	0	4		5-BA-3-10-90-0-1	1	WR
5 5-BA-3-11-85-0	BA 3 11							85	0	VT	RI	RI	R		85	0	4	0	4		5-BA-3-11-85-0-1	1	WR
5 5-BA-3-14-54-0	BA 3 14							54	0	VT	RI	RI	R		54	0	4	0	4		5-BA-3-14-54-0-1	1	WR
5 5-BA-2-2-0-22	BA 2 2							0	22	VT	POR	RI	R		0	22	0	4	4		5-BA-2-2-0-22-1	1	WR
5 5-BA-2-2-69-0	BA 2 2							69	0	VT	RI	RI	R		69	0	4	0	4		5-BA-2-2-69-0-2	2	WR
5 5-BA-2-4-27-0	BA 2 4							27	0	VT	RI	RI	R		27	0	4	0	4		5-BA-2-4-27-0-1	1	WR
5 5-BA-2-14-137-0	BA 2 14							137	0	VT	RI	RI	R		137	0	4	0	4		5-BA-2-14-137-0-1	1	WR
5 5-BA-2-14-0-33	BA 2 14							0	33	VT	UF	IF	R		0	33	0	4	4		5-BA-2-14-0-33-2	2	WR
5 5-BA-1-2-0-2	BA 1 2							0	2	VT	RI	RI	R		0	0	0	4	4		5-BA-1-2-0-0-1	1	WR
5 5-BA-1-2-132-0	BA 1 2							132	0	VT	RI	RI	R		132	0	4	0	4		5-BA-1-2-132-0-2	2	WR
5 5-BA-1-8-0-56	BA 1 8							0	56	VT	RI	RI	R		0	56	0	4	4		5-BA-1-8-0-56-1	1	WR
5 5-BA-1-15-144-0	BA 1 15							144	0	VT	RI	RI	R		144	0	4	0	4		5-BA-1-15-144-0-1	1	WR
5 5-BA-1-15-91-6	BA 1 15							91	6	VT	IF	IF	R		91	6	0	10	10		5-BA-1-15-91-6-2	2	WR
5 5-LD-4-5-48-87	LD 4 5							48	87	VT	RI	RI	R		48	87	5	0	5		5-LD-4-5-48-87-1	1	WR
5 5-LD-4-33-58-0	LD 4 33							58	0	VT	RI	RI	R		58	0	4	0	4		5-LD-4-33-58-0-1	1	WR
5 5-LD-4-45-0-2	LD 4 45							0	2	VT	RI	RI	R		0	2	0	4	4		5-LD-4-45-0-2-1	1	WR
5 5-LD-4-50-0-43	LD 4 50							0	43	VT	RI	RI	R		0	43	0	1	4		5-LD-4-50-0-43-1	1	WR
5 5-LD-4-52-13-42	LD 4 52							13	42	VT	RI	RI	R		13	42	2	2	4		5-LD-4-52-13-42-1	1	WR
5 5-LD-4-59-26-9	LD 4 59							26	9	VT	IF	IF	R		26	9	10	0	10		5-LD-4-59-26-9-1	1	WR
5 5-LD-4-59-41-88	LD 4 59							41	88	VT	RI	RI	R		41	88	12	0	12		5-LD-4-59-41-88-2	2	WR
5 5-LD-3-25-0-128	LD 3 25							0	128	VT	RI	RI	R		0	128	0	4	4		5-LD-3-25-0-128-1	1	WR
5 5-LD-3-34-0-50	LD 3 34							0	50	VT	RI	RI	R		0	50	0	4	4		5-LD-3-23-0-120-1 5-LD-3-34-0-50-1	1	WR
	LD 3 34 LD 2 40								7	VT	RI	RI	R		11	7	0	-	.5		5-LD-2-40-11-7-1	1	WR
5 5-LD-2-40-11-7 5 5-LD-1-7-9-239	LD 2 40							11 9	239	VT	UC	UC	R		9	239	9	0	9		5-LD-2-40-11-7-1 5-LD-1-7-9-239-1	1	WR
								8		VT	POR	RI	R		8		0	2	2			1	
5 5-LD-1-8-8-230								0,000	230	VT			R		10-00	230	2	0	2		5-LD-1-8-8-230-1		WR
5 5-LD-1-24-43-234	LD 1 24 LD 1 24							43	234 229	VT	LOF	LOF UC	R R		43	234 229	4	0	4		5-LD-1-24-43-234-1 5-LD-1-24-43-229-2	1 2	WR
5 5-LD-1-24-43-229								43		VT	UC	RI	R R		43 7		0	2	2				WR
5 5-LD-1-26-7-234	LD 1 26								234		RI	RI				234	_	Z A	_		5-LD-1-26-7-234-1	1	WR
5 5-LD-1-26-48-236	LD 1 26							48	236	VT VT	RI	2.00	R R		48	236	0	4	4		5-LD-1-26-48-236-2	2	WR
5 5-LD-1-29-6-233	LD 1 29							6	233		LOF	LOF			6	233	4	0	4		5-LD-1-29-6-233-1	1	WR
5 5-LD-1-37-6-233	LD 1 37							6	233	VT	RI	RI	R		6	233	4	Ü	4		5-LD-1-37-6-233-1	1	WR
5 5-LD-1-39-3-235	LD 1 39	1			1			3	235	VT	UC	UC	R		3	235	0	6	6		5-LD-1-39-3-235-1	1	WR

Glossary of Abbreviations used in the Master Table

BA Barrell
BB Backing Bar

BC Bottom or back side corrosion indication

Balanced Field Electromagnetic Testing (an eddy current technique, TexTex occasionally referrs to this as "Hawkeye" after

BFET their instrumentation model that utilizes the technique)

B, Bulge Bulge

Bracket Existing bracket

Dent Dent

ER Extension Ring
G Gouge

GA "Ground Area" Areas found to be cleared of coating by grinding.

IF Incomplete Fill Incomplete Penetration

L, Linear Linear indication having length greater than three times width

LAM, Lamination Lamination (original plate manufacture defect)

LD Lower Dome

LFET Low Frequency Electromagnetic Testing (an eddy current technique)

LOF Lack of Fusion

MT Magnetic Particle Testing

N Nozzle (A Pipe Cap installed over an original construction feature such as grout nozzle, strain gauge nozzle, etc.)

N/A Not Applicable

As found in EEI Recommendation Column: "No Repair" An indication that met reporting criteria but, following prove-up, did

NR not meet criteria for providing a repair.

NRI No Recordable Indication
Porosity (also denoted by "POR")

PA Plate Anchor

PAUT Phased Array Ultrasound Testing

Pipe Cap: A method repair by which a short length of pipe with an attached end cap is placed over the affected area and welded in place around the circumference with a full fillet weld. Existing repairs of this type are marked "N" in the Master

PC Table.

POR Porosity (also denoted by "P")
PP Patch Plate (see also TSPP)

As found in EEI Recommendation Column: "Repair" An indication that met reporting criteria and, following prove-up, met

R criteria for providing a repair.

RI Rounded Indication (width to length ratio 3 or less)

SG Strain Gauge Fitting
SP Shell Plate
TC Top side corrosion
TO Tear or Tear Out

TS Top Side indication: a general term to identify an indication on the surface facing the examiner.

TSP Top Side Pit

TSPP Tombstone patch plate, as described in API 653

TTH Telltale Penetration UC Undercut

UD Upper Dome
UF "under fill", also see IF
UT Ultrasound Testing
VB Vacuum Box Testing
VT Visual Testing

W Weld

WC Weld Cover: often an channel section placed over backing bars in the upper dome

Weld Indication: A generic term reported by TesTex to identify an indication found in a weld, typically found with an eddy

WI current method

Weld Repair: A repair made solely by the application of weld filler and appropriate grinding. No patch plate or other additional

WR metal other than filler is added.

Enterprise Engineering Inc. Red Hill Tank 17 Inspection Printed 11/19/2019
File Master Features Tank 5 for EXWC krs

GLOSSARY Page 11

ATTACHMENT G CALCULATIONS

1.0 TANK 5 CORROSION RATES

Overview

EEI is providing the information below as formulas for calculating corrosion rates for the steel liner. See Clean Inspect Repair TANKS 4 AND 13 (TO 004) Clean Inspect Repair Tanks 14, 17, AND 18 (TO 005) Design Analysis – Basis of Design document, Rev 3.0 dated October 2017 which establishes remaining minimum remaining wall thickness accept/reject criteria.

Record drawings of the Red Hill tanks indicate the steel liner plates in the upper dome, barrel, and lower dome in all of the tanks are 250 mils thick plate nominal. The floor (referred to as "base plate" on record drawings) of the lower dome in all of the tanks is indicated as 500 mils thick plate. Record drawings indicate formed cover plates were installed circa 2002 over the backing bars of the upper dome welds. This document prepared by EEI provides a calculation of corrosion rates for 250 mils thick steel liner plates and formed cover plates of the upper dome.

2.0 MAXIMUM CALCULATED CORROSION RATES FOR TANK 5

Maximum calculated corrosion rates for Tank 5 based on wall plate with least remaining wall thickness is as follows:

Upper Dome – Maximum wall loss was 134 mils of metal which occurred in 75 years of service making the corrosion rate:

• Corrosion Rate = 134 mils / 75 years = 1.789 mils / year

Extension Ring – Maximum wall loss was 138.15 mils of metal which occurred in 75 years of service making the corrosion rate:

• Corrosion Rate = 138.15 mils / 75 years = 1.842 mils / year

Barrel – Maximum wall loss was 129.3 mils of metal which occurred in 75 years of service making the corrosion rate:

• Corrosion Rate = 129.3 mils / 75 years = 1.724 mils / year

Lower Dome – Maximum wall loss was 49.35 mils of metal which occurred in 75 years of service making the corrosion rate:

• Corrosion Rate = 49.35 mils / 75 years = 0.658 mils / year

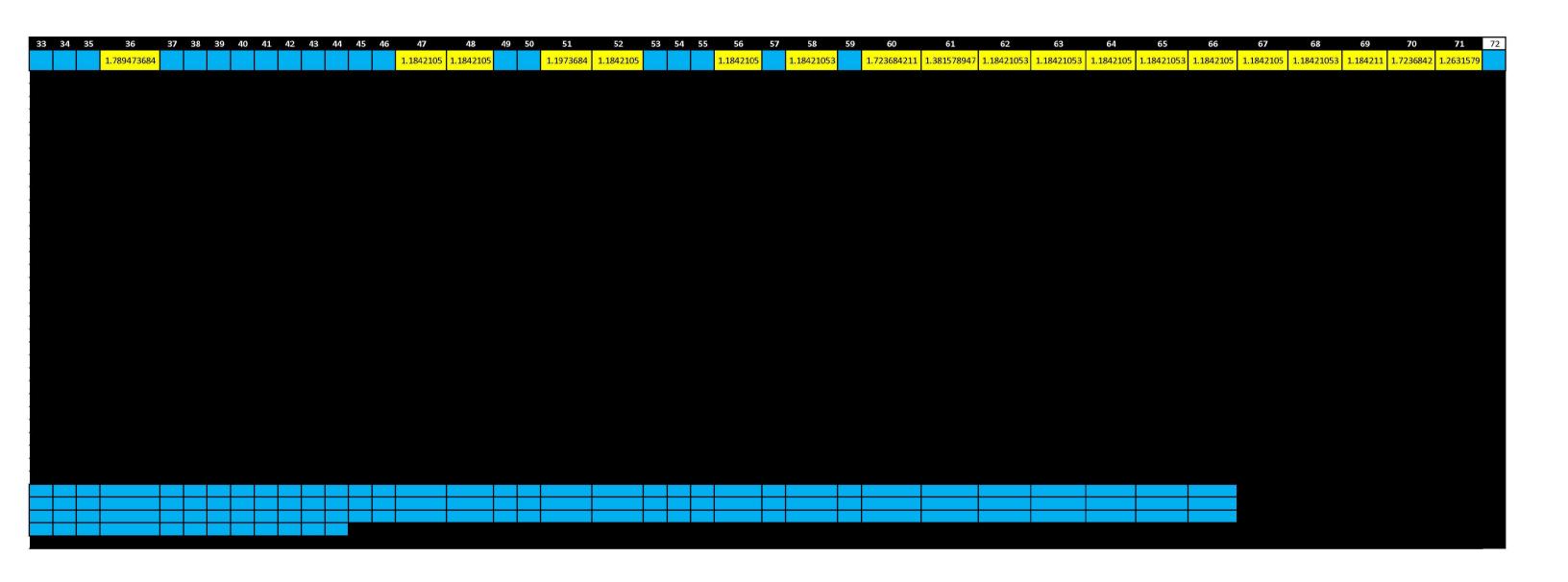
Floor – Negligible – measured plate thickness was within mill tolerance.

See attached shell roll out for location in tank.

Tank 5 – API 653 Inspection Red Hill Fuel Storage Facility, NAVSUP FLC, JBPHH EEI Project No.: 8877 ATTACHMENT G, Page 1

Tank 5 corrosion r	Tank 5 corrosion rate by plate.										
All rates are in mils per year											
<u>Legend</u>											
	Ξ	Thickness of plate greater than 0.200"									
	=	Measureable corrosion									
	Л	No Plate Exists in this Shell Course									

	Column1	1	2 3	4	5	6	7	8	9	10	11	12	13	14	15	16	17 18	19	20	21	22	23	24	25	26	27	28 29	9 30 31
Jpper Dome	Α			0.65789474	1.18421053	1.1842105	1.1842105	1.184210526	1.184210526	1.18421053						1.4473684			1.18421053									
	E4		1.84210526											1.1842105	1.46052632	1.2368421											3 3	
sior g	E3		1.26315789				1						1110 121000	1.3157895	1.46052632	1,2000,121												
Extension Ring	E2								0.657894737	0.65789474	1.4605263	1.36842105				1.3157895												
Ä	E1											0.90789474																
	28																											
	27											1.34210526		1.7236842		0.6578947												
	26	1.1842105																										
	25												0.80263158															
	24																											
	23																											
	22								1.184210526																			
	21																											
	20																											
	19							1.184210526		1.18421053				1.1842105														
	18																											
	17			_																								
<u></u>	16				4		_																					
Barre	15																											
ä	14 13			+			_	1.184210526																				
	12			+			_	1.184210526																				
	11			+				1.184210526																				
	10			+				1.184210526						0.8026316	1													
	9							1110 1210320						0.0020310														
	8																											
	7							1.184210526																				
	6							1.184210526																				
	5							1.328947368				1.18421053																
	4																											
	3																											
	2								1.184210526																			
	1																											
ψ	4																											
mo	3														0.65789474													
er Do	2																											
3W6	1																											
Ľ	Floor				11																							



ATTACHMENT H VBT/MT REPORTS



EEI-MT-001 ATTACHMENT 1

MAG	NETIC	PARTI	CLE EX	AMIN	ATION REPORT	NDE	REPORT NO.:	
PROJE	ECT NO.			CLIEN		CLIEN	IT REF. NO.	PAGE
	88	377			NAVFAC EXWC	N394	30-15-D-1678, TO 0011	1 OF 3
IDENT	IFICATION	1				DRAW	/ING NO.	DATE
			8" Dra	in Cap			N/A	1/5/2018
LOCA	TION				PART/WELD NO.	EQUIF	PMENT MODEL & S/N	CAL DUE DATE
	Re	d Hill Ta	ank 5		Various	Magn	aflux Y-1	Done on Day of Use
METH	OD				•	EXAM	INATION	PROCEDURE NO.
☑	WET	✓	AC	✓	YOKE	☑	INITIAL	EEI-MT-001
	DRY		DC		OTHER:		REPAIR NO.	CODE/SPEC
								ASME Section V, Article 7
Mate 8" circ	ular 1/2" th		pection.					
RESUI	LTS:		ACCEPT	•	☑ REJECT	☑	FOR INFORMATION ONLY	
TECHI	VICIAN				CERTIFIED TO LE	VEL CLIEN	NT REPRESENTATIVE	DATE
NAME			DJK		ASNT-SNT-TC-1A	П		
SIGNA	TURE:		DJK		DATE: 1/5/2018	AUTH	IORIZED INSPECTOR	DATE
REVIE	WED BY:	_			DATE:		DJK	1/5/2018



8" Drain Cap

ID#	Location	Photos	MT Results	Indication info	Repair Details	Extra Comments
N/A	3:00		R	1/8" LW	Grind out and re-weld if need be	
N/A	4:00	D vo.	R	1/8" LT	Grind out and re-weld if need be	
N/A	6:00		R	1/8" LW	Grind out and re-weld if need be	



EEI-MT-001 ATTACHMENT 1

N/A	10:00		R	1/8" LT	Grind out and re-weld if need be	
-----	-------	--	---	---------	----------------------------------	--

	Glossary	
R: Reject		
A: Accept		
L: Longitudinal		
T: Toe of Weld		
W:Within weld		



EEI-MT-002 ATTACHMENT 1

MAG	NETIC F	PARTIC	LEEX	AMINA	TION REPOR	₹ T	NDE	REPORT NO.:		
PROJE	CT NO.			CLIENT			CLIENT	T REF. NO.		PAGE
	88	377			NAVFAC EXWC		N3943	0-15-D-1678, TO 00	011	1 OF 6
IDENT	IFICATION						DRAW	ING NO.		DATE
			Strain C	auges				N/A		1/15/2018
LOCAT	TION				PART/WELD NO.		EQUIP	MENT MODEL & S/N		CAL DUE DATE
Red Hill Tank 5				Various		Magnaflux Y-1			Done on Day of Use	
METH	DD						EXAMII	NATION		PROCEDURE NO.
☑	WET	☑	AC	✓	YOKE		☑	INITIAL		EEI-MT-001
	DRY		DC		OTHER:			REPAIR NO.		CODE/SPEC
										ASME Section V, Article 7
DESCF	RIPTION						•			
Mate 3 1/2" Some	oipe, with p pipes had b	late weld	ed at end	circle Pa	itch Plates					
RESUL	-TS:	☑	ACCEP ⁻		□ REJECT		Ø	FOR INFORMATION	N ONLY	
TECHN	NICIAN				CERTIFIED TO	LEVEL	CLIEN	IT REPRESENTATIV	VΕ	DATE
NAME:			JMS		ASNT-SNT-TC-1A	II				
SIGNA	TURE:		JMS		DATE: 1/15/201	8	AUTH	ORIZED INSPECTO)R	DATE
REVIE'	WED BY:				DATE:			DJK		1/15/2018



Strain Gauges

ID#	Location	Photos	MT Results	Indication info	Repair Details	Extra Comments
TK5-SG-R5P3	R5P3		N/A	N/A	NR	Already MT under WGS warrenty work
TK5-SG-R5P7	R5P7	197 858 204	N/A	N/A	NR	Already MT under WGS warrenty work
TK5-SG-R5P11	R5P11	SG DOWN 8511 SG 151- 108	Α	N/A	NR	



EEI-MT-002 ATTACHMENT 1

TK5-SG-R5P15	R5P15	RSP15 SIS MT/VIT OK	А	N/A	NR	
TK5-SG-R12P2	R12P2	RIPA RIVINION OK	А	N/A	NR	
TK5-SG-R12P6	R12P6	155 P. S.	N/A	N/A	NR	Already MT under WGS warrenty work



TK5-SG-R12P10	R12P10	PIQ PIO SON/INT OK	А	N/A	NR	
TK5-SG-R12P13	R12P13	210 25 C	А	N/A	NR	
TK5-SG-R19P1	R19P1	RIA PI 15 SG-MT/VI OK	Α	N/A	NR	



TK5-SG-R19P5	R19P5	#158	N/A	N/A	NR	Already MT under WGS warrenty work
TK5-SG-R19P9	R19P9	17 390	N/A	N/A	NR	Already MT under WGS warrenty work
TK5-SG-R19P13	R19P13	120 S6 19 R19 13 1	Α	N/A	NR	



Glossary

R: Reject
A: Accept
L: Longitudinal
T: Toe of Weld
W:Within weld
NR: No Repair
N/A: Not Applicable

NRI: No Reported Indications



MAG	NETIC	PARTI	CLE E	(AMIN	ATION REPORT	NDE REPORT NO.:	
PROJ	ECT NO.			CLIEN.	Γ	CLIENT REF. NO.	PAGE
	8	877			NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 15
IDENT	TFICATION	J				DRAWING NO.	DATE
			Plug	Welds		N/A	1/15/2018
LOCA	TION				PART/WELD NO.	EQUIPMENT MODEL & S/N	CAL DUE DATE
	Re	ed Hill T	ank 5		Various	Magnaflux Y-1	Done on Day of Use
METH	OD				•	EXAMINATION	PROCEDURE NO.
✓	WET	☑	AC	☑	YOKE	☑ INITIAL	EEI-MT-001
	DRY		DC		OTHER:	□ REPAIR NO.	CODE/SPEC
							ASME Section V, Article 7
RESU	LTS:	V	ACCEF	РΤ	☑ REJECT	☑ FOR INFORMATION ONLY	
TECH	NICIAN				CERTIFIED TO LEVE	CLIENT REPRESENTATIVE	DATE
NAME			JMS		ASNT-SNT-TC-1A II		
SIGNA	ATURE:		JMS		DATE: 1/15/2018	AUTHORIZED INSPECTOR	DATE
REVIE	WED BY:				DATE:	DJK	1/15/2018



Plug Welds ID# Location Photos MT Results Indication info Repair Details Extra Comments **EXPANSION** TK5-PW-2 NR Α N/A **JOINT EXPANSION** TK5-PW-3 Α NR N/A JOINT **EXPANSION** TK5-PW-8 N/A NR Α **JOINT**



TK5-PW-9	EXPANSION JOINT	9 31	А	N/A	NR	
TK5-PW-13	EXPANSION JOINT		А	N/A	NR	
TK5-PW-14	EXPANSION JOINT		А	N/A	NR	



TK5-PW-19	EXPANSION JOINT		А	N/A	NR	
TK5-PW-24	EXPANSION JOINT	24	А	N/A	NR	
TK5-PW-26	EXPANSION JOINT		А	N/A	NR	



TK5-PW-34	EXPANSION JOINT	3ª Max	А	N/A	NR	
TK5-PW-35	EXPANSION JOINT		А	N/A	NR	
TK5-PW-36	EXPANSION JOINT	36	Α	N/A	NR	



TK5-PW-40	EXPANSION JOINT		А	N/A	NR	
TK5-PW-41	EXPANSION JOINT		А	N/A	NR	
TK5-PW-52	EXPANSION JOINT	CK P	А	N/A	NR	



TK5-PW-53	EXPANSION JOINT	54 53	А	N/A	NR	
TK5-PW-63	EXPANSION JOINT		А	N/A	NR	
TK5-PW-64	EXPANSION JOINT		Α	N/A	NR	



TK5-PW-70	EXPANSION JOINT	70 Kot	А	N/A	NR	
TK5-PW-71	EXPANSION JOINT	TI AT OK	А	N/A	NR	
TK5-PW-71B	EXPANSION JOINT		А	N/A	NR	



TK5-PW-76	EXPANSION JOINT		А	N/A	NR	
TK5-PW-77	EXPANSION JOINT	11 Max	А	N/A	NR	
TK5-PW-77B	EXPANSION JOINT		Α	N/A	NR	



TK5-PW-82	EXPANSION JOINT	А	N/A	NR	
TK5-PW-83	EXPANSION JOINT	A	N/A	NR	
TK5-PW-83B	EXPANSION JOINT	А	N/A	NR	



TK5-PW-88	EXPANSION JOINT		А	N/A	NR	
TK5-PW-89	EXPANSION JOINT	SA MARIE OF A STATE OF	A	N/A	NR	
TK5-PW-94	EXPANSION JOINT		А	N/A	NR	



TK5-PW-95	EXPANSION JOINT	Q.S. ANT OX	А	N/A	NR	
TK5-PW-101	EXPANSION JOINT		А	N/A	NR	
TK5-PW-102	EXPANSION JOINT	100	Α	N/A	NR	



TK5-PW-103B	EXPANSION JOINT		R	Multiple L W Cracks	Grind and Re-weld 6" WR	Located on E1 P9
TK5-PW-121	Adjustment Plate		А	N/A	NR	
TK5-PW-139	Adjustment Plate	m ok	А	N/A	NR	



TK5-PW-156	Adjustment Plate		А	N/A	NR	
TK5-PW-192	Adjustment Plate	EZ PO 192 ATTOK	А	N/A	NR	
TK5-PW-210	Adjustment Plate		Α	N/A	NR	



TK5-PW-228 Adjustment Plate	А	N/A	NR	
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Glossary

R: Reject A: Accept

L: Longitudinal T: Toe of Weld

W:Within weld

NR: No Repair

N/A: Not Applicable NRI: No Reported Indications



MAG	MAGNETIC PARTICLE EXAMINATION REPORT					NDE REPORT NO.:			
PROJ	ECT NO.			CLIENT	•	CLIENT REF. NO.	PAGE		
	88	377			NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 2		
IDENT	TFICATION	1				DRAWING NO.	DATE		
Miter Welds in 32" pipe				ds in 32"	pipe	N/A	1/17/2018		
LOCATION PART					PART/WELD NO.	EQUIPMENT MODEL & S/N	CAL DUE DATE		
	Re	d Hill T	ank 5		Various	Magnaflux Y-1	Done on Day of Use		
METH	OD					EXAMINATION	PROCEDURE NO.		
☑	WET	☑	AC	☑	YOKE	☑ INITIAL	EEI-MT-001		
	DRY		DC		OTHER:	□ REPAIR NO.	CODE/SPEC		
							ASME Section V, Article 7		
Mate Welds	located in	the Mite	er bend or						
RESU	LTS:	✓	ACCEF	PT	□ REJECT	✓ FOR INFORMATION ONLY			
TECH	NICIAN				CERTIFIED TO LEVE	_ CLIENT REPRESENTATIVE	DATE		
NAME	:		JMS		ASNT-SNT-TC-1A II				
SIGNA	ATURE:		JMS		DATE: 1/17/2018	AUTHORIZED INSPECTOR	DATE		
REVIE	WED BY:		KRS		DATE: 1/17/2018	DJK	1/17/2018		



ID# Location Photos MT Results Indication info Repair Details Extra Comments N/A 32" pipe A N/A NR

Glossary

R: Reject

A: Accept

L: Longitudinal

T: Toe of Weld

W:Within weld

N/A: not applicable

NR: no repair



MAG	NETIC	PART	ICLE E	XAMIN	ATION REPORT	NDE	NDE REPORT NO.:			
	ECT NO.			CLIENT		CLIE	NT REF. NO.	PAGE		
	8	877			NAVFAC EXWC	N394	30-15-D-1678, TO 0011	1 OF 5		
IDENT	IDENTIFICATION					DRAV	VING NO.	DATE		
	TesTex Weld Indications						N/A	1/5/2018		
LOCA	TION				PART/WELD NO.	EQUI	PMENT MODEL & S/N	CAL DUE DATE		
	Re	d Hill T	ank 5		Various	Magr	naflux Y-1	Done on Day of Use		
METH	OD					EXAN	MINATION	PROCEDURE NO.		
☑	WET	☑	AC	☑	YOKE	☑	INITIAL	EEI-MT-001		
	DRY		DC		OTHER:		REPAIR NO.	CODE/SPEC		
								ASME Section V, Article 7		
	ndications	were re	ported by	Testex a	fter using the Hawkeye	system				
RESU	LTS:	v	ACCEP	Т	□ REJECT	Ē	FOR INFORMATION ONLY			
TECH	NICIAN				CERTIFIED TO LEV	EL CLIE	NT REPRESENTATIVE	DATE		
NAME	:		JGM		ASNT-SNT-TC-1A	I				
SIGNA	ATURE:		JGM		DATE: 1/5/2018	AUTI	HORIZED INSPECTOR	DATE		
REVIE	WED BY:				DATE:		DJK	1/5/2018		



Weld Indications

		T		Γ		
ID#	Location	Photos	MT Results	Indication info	Repair Details	Extra Comments
5-BA-19-2-0-34	R19P2	The RIGHT OF THE R	А		Visual examination found UF and UC present	
5-UD-A-17-31-0	A17	To be to the state of the state	Α		Grind out and re-weld failed on visual	
5-UD-A-18-0-0	A18		Α		Grind out and re-weld failed on visual	



5-UD-A-18-26-0	A18	А		Grind out and re-weld failed on visual	
5-UD-A-20-10-0	A20	А		Grind out and re-weld failed on visual	
5-UD-A-23-6-128	A23	R	1/8" LW	Grind out and re-weld nozzle, failed on visual	Small indication, went away after burring out



5-UD-A-24-0-27	A24	ու <mark>նակակավ</mark> արիակական անական ա	R	1/4" LT	Grind out and re-weld	Still present after burring out
5-UD-A-26-34-127	A26		А		Grind out and re-weld	
5-UD-C-16-55-125	C16	Control of the state of the sta	Α		Grind out and re-weld	



	Glossary
R: Reject	
A: Accept	
L: Longitudinal	
A: Accept L: Longitudinal T: Toe of Weld	
W:Within weld	



EEI-VBT-005 ATTACHMENT 1

VACUUM BOX TESTING REPORT						NDE REPORT NO.:	NDE REPORT NO.:				
PROJEC	CT NO.			CLIENT	•	CLIENT REF. NO.	PAGE				
	88	77			NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 2				
IDENTIF	ICATION					DRAWING NO.	DATE				
8" Drain Cap						N/A	1/20/2018				
LOCATION PART/WELD NO.						EQUIPMENT MODEL & S/N	CAL DUE DATE				
Red Hill Tank 5 Various					Various	EEI CUSTOM BOX #006	N/A				
METHOD)				•	EXAMINATION	PROCEDURE NO.				
Ø	SOAP	☑	21 kPa		56 kPa	☑ INITIAL	EEI-VBT-001				
	LD		35 Kpa	✓	70 kPa	☐ REPAIR NO.	CODE/SPEC				
							API 650 SECTION 8.6				
RESULT	S:	V	ACCEP	ī .	□ REJECT	☐ FOR INFORMATION ONLY					
TECHNIC	CIAN				CERTIFIED TO LEVE	CLIENT REPRESENTATIVE	DATE				
NAME:			ADS		ASNT-SNT-TC-1A II						
SIGNAT	URE:		ADS		DATE: 1/20/2018	AUTHORIZED INSPECTOR	DATE				
	/ED BY:		SCW		DATE: 1/20/2018	DJK	1/20/2018				



8" Drain Cap

ID#	Location	Photos	VBT Results	Indication info	Repair Details	Extra Comments
TK5-8"DC	Floor		А	N/A	Grind out and re-weld if need be	Repair due to failed MT

Glossary

R: Reject A: Accept NR: No Repair N/A: Not Applicable

NRI: No Reported Indications



EEI-VBT-002 ATTACHMENT 1

THE DESIGNATION OF STATES AND SECURITIONS OF SECURI					NDE REPORT NO.:	NDE REPORT NO.:			
PROJI	ECT NO.		CLIENT		CLIENT REF. NO.	PAGE			
	88	377		NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 3			
IDENTIFICATION				DRAWING NO.	DATE				
		Adjust	ment Pla	te	N/A	1/23/2018			
LOCA.	TION			PART/WELD NO.	EQUIPMENT MODEL & S/N	CAL DUE DATE			
	Re	d Hill Tank 5		Various	EEI CUSTOM BOXS #001,#003	N/A			
METH	OD			•	EXAMINATION	PROCEDURE NO.			
☑	SOAP	☑ 21 kPa	ı 🗆	56 kPa	☑ INITIAL	EEI-VBT-001			
	LD	□ 35 Kpa	a 🗹	70 kPa	□ REPAIR NO.	CODE/SPEC			
						API 650 SECTION 8.6			
Mate The to Angle All thre	the higher pressure. A soap film solution was used for the all testing with vacuum box. Material The top and bottom of the 2 1/2"x 3"x 5/16" angle iron for a total of two filet welds. Angle weld on the bottom of Adjustment Plate. All three welds travel around the entire tank resulting in 942' of weld. Plug Welds and Joint Plates are located all along the Adjustment Plate								
RESU	LTS:	☑ ACCE	⊃T	□ REJECT	☐ FOR INFORMATION ONL'	(
TECH	NICIAN			CERTIFIED BY LEVE	CLIENT REPRESENTATIVE	DATE			
NAME	:	ADS		ASNT-SNT-TC-1A II					
SIGNA	ATURE:	ADS		DATE: 1/23/2018	AUTHORIZED INSPECTOR	DATE			
REVIE	WED BY:	JGM		DATE: 1/23/2018	DJK	1/23/2018			



Adjustment Plate

ID#	Location	Photos	MT Results	Indication info	Repair Details	Extra Comments
N/A	Upper Angle Iron Fillet welds	Upper Argle non Filter Wittes ATT 2 - 24 FIELD 14 FIELD (TANKS * 5 - 20)	А	N/A	NR	
N/A	Corner Weld Under the Adjustment Plate	1 At 1 (Tooks - 5-20)	А	N/A	NR	
N/A	Plug Welds and Joint Plates	JOINT FOR J PARTE (TRIKS = 5-20)	А	N/A	NR	Some Plug Welds we not tested due to geometric constrant



EEI-VBT-002 ATTACHMENT 1

Glossary
R: Reject A: Accept IR: No Repair I/A: Not Applicable
x: Accept
IR: No Repair
I/A: Not Applicable



EEI-VBT-001

VACUUM I	3OX TE	STING	REPO	ORT	NDE REPORT NO.:				
PROJECT NO. CLIENT					CLIENT REF. NO.	PAGE			
	8877			NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 3			
DENTIFICATI	NC				DRAWING NO.	DATE			
	Exp	ansion Jo	int File	t Welds	N/A	1/24/2018			
OCATION				PART/WELD NO.	EQUIPMENT MODEL & S/N	CAL DUE DATE			
F	Red Hill T	ank 5		Various	EEI CUSTOM BOXS #001,#002	N/A			
METHOD					EXAMINATION	PROCEDURE NO.			
☑ SOAF	. □	21 kPa		56 kPa	☑ INITIAL	EEI-VBT-001			
□ LD		35 Kpa	✓	70 kPa	□ REPAIR NO.	CODE/SPEC			
						API 650 SECTION 8.6			
DESCRIPTIO	N								
he higher pres A soap film sol Material The top and bo A filet weld at t	sure. ution was ottom of the he end of	used for the e upper an the expasion	e all tes d lower on joint	sting with vacuum box. 2 1/2"x 3"x 5/16" angle in	ch the vacuum was formed. Pressured was	increased to between 56 and 70 kPa. Material was then tested a			

Plug welds are located all along the Expansion joint.

RESULTS: ☑ ACCEPT		□ REJECT	☐ FOR INFORMATION ONLY	
TECHNICIAN		CERTIFIED BY LEVEL	CLIENT REPRESENTATIVE	DATE
NAME:	ADS	ASNT-SNT-TC-1A II		
SIGNATURE:	ADS	DATE: 1/24/2018	AUTHORIZED INSPECTOR	DATE
REVIEWED BY:	JGM	DATE: 1/24/2018	DJK	1/23/2018



Expansion Joint ID # Location Photos MT Results Indicate

ID#	Location	Photos	MT Results	Indication info	Repair Details	Extra Comments
N/A	Upper Angle Iron Fillet welds	Daner Angue Fron Welds Fron Welds Source Service Ser	А	N/A	NR	
N/A	Lower Angle Iron Filet welds	Lower Angle Iron Welds	Α	N/A	NR	
N/A	End of Plate Filet Weld	To be second Afres Precipe Different	Α	N/A	NR	



EEI-VBT-001 ATTACHMENT 1

N/A Plug Welds	Sman A	N/A	NR	
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Glos	sary
R: Reject A: Accept NR: No Repair N/A: Not Applicable	
A: Accept	
NR: No Repair	
N/A: Not Applicable	



AND THE DESIRED FROM THE PROPERTY AND THE SECOND THE TOTAL PROPERTY AND THE PROPERTY AND TH					RT	NDE	NDE REPORT NO.:			
PROJE	CT NO.			CLIENT		CLIEN	IT REF. NO.	PAGE		
	88	377			NAVFAC EXWC	N394	30-15-D-1678, TO 0011	1 OF 6		
IDENTIFICATION					DRAV	VING NO.	DATE			
			Strain (Gauges			N/A	1/18/2018		
LOCAT	ION				PART/WELD NO.	EQUIF	PMENT MODEL & S/N	CAL DUE DATE		
		d Hill Tar	nk 5		Various	EEI C	CUSTOM BOXS #004	N/A		
METH	OD					EXAM	IINATION	PROCEDURE NO.		
☑	SOAP	v	21 kPa		56 kPa	✓	INITIAL	EEI-VBT-001		
□	LD		35 Kpa	✓	70 kPa		REPAIR NO.	CODE/SPEC		
								API 650 SECTION 8.6		
A soap Mate 12 Stra	Test was conducted at intial pressure between 21 and 35 kPa in which the vacuum was formed. Pressured was increased to between 56 and 70 kPa. Material was then tested at the higher pressure. A soap film solution was used for the all testing with vacuum box. Material 12 Strain gauges were examined. 5 Strain gauges were already Vacuum Box Tested from the warrenty work done previously.									
RESUL	.1S:	✓	ACCEPT		□ REJECT		FOR INFORMATION ONLY			
TECHN	NICIAN				CERTIFIED TO LEVE	CLIE	NT REPRESENTATIVE	DATE		
NAME:	2		AKD		ASNT-SNT-TC-1A II					
SIGNA	TURE:		AKD		DATE: 1/18/2018	AUTH	HORIZED INSPECTOR	DATE		
REVIE'	WED BY:				DATE:		DJK	1/18/2018		



Strain Gauges

ID#	Location	Photos	VBT Results	Indication info	Repair Details	Extra Comments
TK5-SG-R5P3	R5P3		N/A	N/A	NR	Already VBT under WGS warrenty work
TK5-SG-R5P7	R5P7	19 85R/SE 204	N/A	N/A	NR	Already VBT under WGS warrenty work
TK5-SG-R5P11	R5P11	SG DOWN 851 194 154 154 154 154	А	N/A	NR	



TK5-SG-R5P15	R5P15	RSP15 SGN1OK	А	N/A	NR	
TK5-SG-R12P2	R12P2	RIARA RI	А	N/A	NR	
TK5-SG-R12P6	R12P6	LAW 204 155 Pages	N/A	N/A	NR	Already VBT under WGS warrenty work



EEI-VBT-003 ATTACHMENT 1

TK5-SG-R12P10	R12P10	PIQ PIO SIN/V	А	N/A	NR	
TK5-SG-R12P13	R12P13	215 24 25 0 t	А	N/A	NR	
TK5-SG-R19P1	R19P1	RIA PI IIS SG- MIZVA- OK	Α	N/A	NR	

4 of 6



EEI-VBT-003 ATTACHMENT 1

TK5-SG-R19P5	R19P5	#158 36	N/A	N/A	NR	Already VBT under WGS warrenty work
TK5-SG-R19P9	R19P9	17 (a) (a) (b) (a) (a) (a) (a) (a) (a) (a) (a) (a) (a	N/A	N/A	NR	Already VBT under WGS warrenty work
TK5-SG-R19P13	R19P13	120 SGARIA INIA	А	N/A	NR	



EEI-VBT-003 **ATTACHMENT 1**

Glossary

R: Reject A: Accept NR: No Repair N/A: Not Applicable
NRI: No Reported Indications



EEI-VBT-004 ATTACHMENT 1

VACUUM BOX TESTING REPORT PROJECT NO. CLIENT					RT	NDE REPORT NO.:	
PROJEC ⁻	T NO.			CLIENT		CLIENT REF. NO.	PAGE
	887	77			NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 3
DENTIFI	CATION					DRAWING NO.	DATE
			Towe	r Legs		N/A	1/26/2018
OCATIO	N				PART/WELD NO.	EQUIPMENT MODEL & S/N	CAL DUE DATE
	Red	Hill Ta	ank 5		Various	EEI CUSTOM BOX #005	N/A
METHOD						EXAMINATION	PROCEDURE NO.
☑	SOAP	☑	21 kPa		56 kPa	☑ INITIAL	EEI-VBT-001
	_D		35 Kpa	✓	70 kPa	□ REPAIR NO.	CODE/SPEC
							API 650 SECTION 8.6
RESULTS	S :	v	ACCEPT	Ī'	□ REJECT	☐ FOR INFORMATION ONLY	
TECHNIC	IAN						
					CERTIFIED BY LEVEL	CLIENT REPRESENTATIVE	DATE
NAME:			ADS		CERTIFIED BY LEVEL ASNT-SNT-TC-1A II	-	
NAME: SIGNATU	JRE:		ADS ADS			AUTHORIZED INSPECTOR	DATE



		Tower	r Legs	i		
ID#	Location	Photos	VBT Results	Indication info	Repair Details	Extra Comments
TK5-TL-1	Floor		А	N/A	NR	
TK5-TL-2	Floor		Α	N/A	NR	
TK5-TL-3	Floor		А	N/A	NR	



EEI-VBT-004 **ATTACHMENT 1**

TK5-TL-4 Floor	Α	N/A	NR	
----------------	---	-----	----	--

Glossary

R: Reject A: Accept
NR: No Repair
N/A: Not Applicable
NRI: No Reported Indications



VACUUM BOX REP	ORT	NDE REPORT	NO.:				
PROJECT NO. 8877	CLIENT NAVFAC EXWC	CLIENT REF. NO. N39430-15-D-1678,	TO 0011	PAGE	1	OF	1
IDENTIFICATION Red Hill Tank 5		VACUUM BOX NO. EEI-001		DATE OF 1/15/18	COMP	LETION	
DIMENSIONS L: 24"	W: 6"	H: N/A		BUILDER CMH	INTIAL	.S	

DESCRIPTION

Flat weld box

24"x6"

1 ¼" foam on the bottom

3/8" acrylic sheet







VACUUM BOX REPO	ORT	NDE REPORT NO.:	
PROJECT NO.	CLIENT	CLIENT REF. NO.	PAGE 1 OF 1
8877	NAVFAC EXWC	N39430-15-D-1678, TO 0011	
IDENTIFICATION		VACUUM BOX NO.	DATE OF COMPLETION
Red Hill Tank 5		EEI-002	1/16/18
DIMENSIONS L: 24"	W: 4"	H: 4"	BUILDER INTIALS CMH

DESCRIPTION Angle weld box 24"x4"x4" 2" foam on bottom

3/4" acrylic sheet







VACUUM BOX REPO	RT	NDE REPORT NO.:	
PROJECT NO.	CLIENT	CLIENT REF. NO.	PAGE
8877	NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 1
IDENTIFICATION		VACUUM BOX NO.	DATE OF COMPLETION
Red Hill Tank 5		EEI-003	1/16/18
DIMENSIONS L: 24"	W: 12"	H: 3 ½"	BUILDER INTIALS CMH

DESCRIPTION

Expansion joint weld box

24"x12"x3 ½"

1 ½" foam on bottom

3/8" acrylic sheet







VACUUM BOX REPO	ORT	NDE REPORT NO.:	
PROJECT NO. 8877	CLIENT NAVFAC EXWC	CLIENT REF. NO. N39430-15-D-1678, TO 0011	PAGE 1 OF 1
IDENTIFICATION Red Hill Tank 5		VACUUM BOX NO. EEI-004	DATE OF COMPLETION 1/12/18
DIMENSIONS L: 12"	W: 12"	H: 6½"	BUILDER INTIALS CMH

DESCRIPTION
Strain Gauge box
12"x12" with 9"x9" x6 ½" cube on top
2" foam on bottom
3/8" acrylic sheet







VACUUM BOX REPO	RT	NDE REPORT NO.:	
PROJECT NO.	CLIENT	CLIENT REF. NO.	PAGE
8877	NAVFAC EXWC	N39430-15-D-1678, TO 0011	1 OF 1
IDENTIFICATION		VACUUM BOX NO.	DATE OF COMPLETION
Red Hill Tank 5		EEI-005	1/18/18
DIMENSIONS			BUILDER INTIALS
L: 15"	W: 15"	H: 5 ½"	CMH

DESCRIPTION
Tower Leg box
15"x15"x5 ½"
1 ¼" foam
¾" acrylic sheet







VACUUM BOX REPO	ORT	NDE REPORT NO.:	
PROJECT NO. 8877	CLIENT NAVFAC EXWC	CLIENT REF. NO. N39430-15-D-1678, TO 0011	PAGE 1 OF 1
IDENTIFICATION Red Hill Tank 5	•	VACUUM BOX NO. EEI-006	DATE OF COMPLETION 1/9/18
DIMENSIONS L: 24"	W: 24"	H: N/A	BUILDER INTIALS CMH

DESCRIPTION

8" Drain Cap box

24" x24"

2" foam

3/8" acrylic sheet





ATTACHMENT I PHASED ARRAY REPORT FOR THE 32-INCH PRODUCT LINE WELDS

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EEI-PAUT-001 ATTACHMENT 1

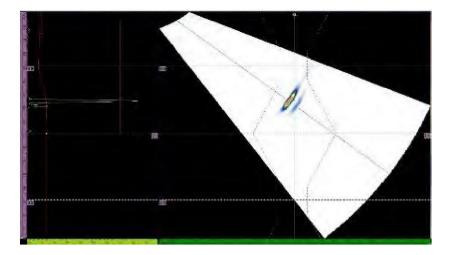
						PAI	UT ANG	SLE BEA	M EXA	MINATIO	ON REPORT
						NDE REPO	RT NO.: PA	AUT 8877			
PROJECT NO.:		CLIENT:				CLIENT RE	F. NO.:				
	8877		NAVE	AC EXWC							
IDENTIFICATION:						DRAWING	NO.:			DATE:	
	Normal Fluid Ser	vice Piping	g Welds				1	N/A			1/17/2018
LOCATION:			PART/WE	LD NO.:	MATERIAL	:	PROCEDU	IRE:	TECHNIC	QUE:	CODE/SPEC:
	Red Hill Tank 5		Va	rious	Carbo	n Steel	EEI-P	AUT-01	45° to	70° PAUT	B31.3
CONDITION:	TEMPERATURE:		DIAMETE	R:	THICKNES	S:	SENSITIVI	TY:	RANGE:		COUPLANT:
Non-coated	✓ AMBIENT	Тон	32	2-inch	.375	-inch	7	TCG		1.8"	SONOSAFE
TRANSDUCER: ID N	o. / FREQ / ELEMENTS /	PITCH		INSTRUM	ENT			CAL. BLO	CK TYPE	CAL. BLOC	L CK SERIAL NO.
	16 element / 0.6 mm			MODEL:		Omniscan S	SX	NIA	VSHIP		
				S/N:		QC-001865	5	INA	VOLIII		
							EXAMINA	TION:	✓ INIT	TAL \square	REPAIR No
DESCRIPTION:											
SCAN PLAN:	I										
Probe ID	Wedge ID		Beam A			D 1 0		T ,,,,,,,,	1.71		
5L16	N55S-A10	MIN		ngles (deg.)			offset (in.)		ngle (deg.) Mate	erial Thickness (in.)
			40	ngles (deg.) MAX	70		offset (in.) 800		ngle (deg.)	Mate	erial Thickness (in.) 0.375
Note: Plan for 32-in	ch pipe.		40	1) Mate	
Note: Plan for 32-in	ch pipe.		40	1) Mate	
Note: Plan for 32-in	ch pipe.		40	1						Mate	
Note: Plan for 32-in			40	1						Mate	
Note: Plan for 32-in		15	40	1						Mate	
Note: Plan for 32-in	•	35	40	1						Mate	
Note: Plan for 32-in	•	35	40	1						Mate	
Note: Plan for 32-in	•		40	1						Mate	
Note: Plan for 32-in	•		40	1						Mate	
Note: Plan for 32-in	•	35	40	1			800) Mate	
RESULTS:	Tanta-co-	REJECT		MAX	70	0.8	800		30		
	151 1.19		9.79	MAX MAX	70	0.8	800	5.0	30	LM.	
RESULTS:	151 1.19		QC REVIE	MAX MAX	70	0.8	800	S.G.	1,13	ATIVE	
TECHNICIAN	1.2r 1.18		QC REVIE	MAX ### FOR INFO W arl Schlenek	70	0.8	800	S.G.	J.IS	ATIVE	

1 of 6

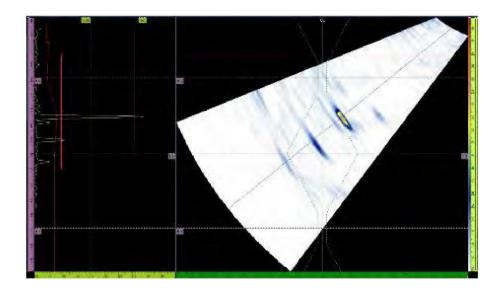


EEI-PAUT-001 ATTACHMENT 1

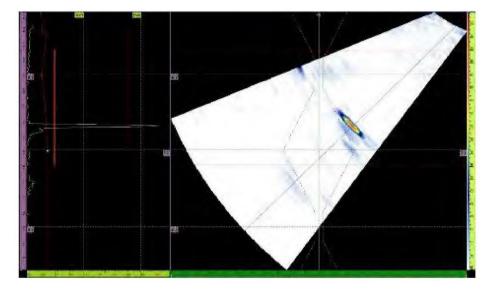
Calibration screen capture showing reference gain being set on NAVSHIP calibration block.



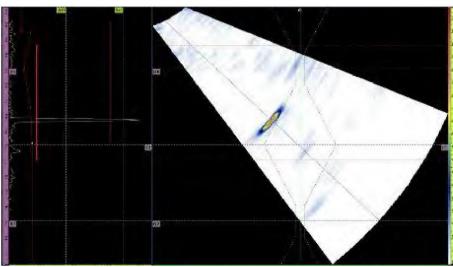
Weld C2 LOF @ 0 deg x 2"



Weld C2 LOF @ 30 deg x 3"

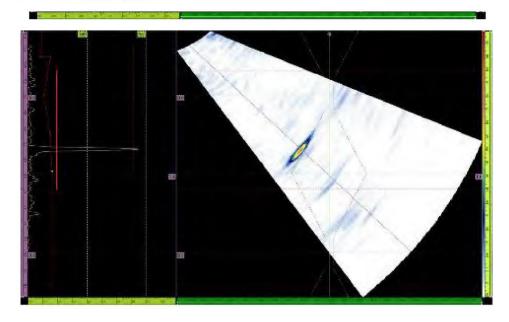


Weld C2 LOF @ 350 deg x 1"

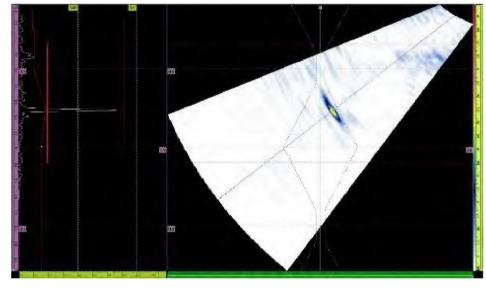


3 of 6

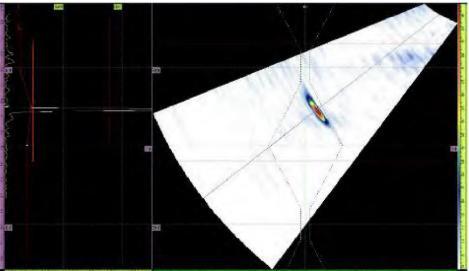
Weld C2 LOF @ 180 deg x 1"



Weld C3 LOF @ 330 deg x 1"



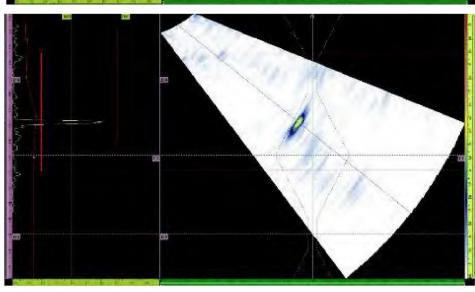
Weld C3 LOF @ 315 deg x 1"



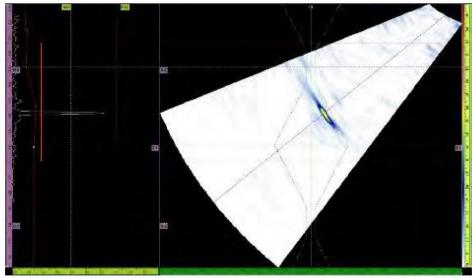


EEI-PAUT-001 ATTACHMENT 1

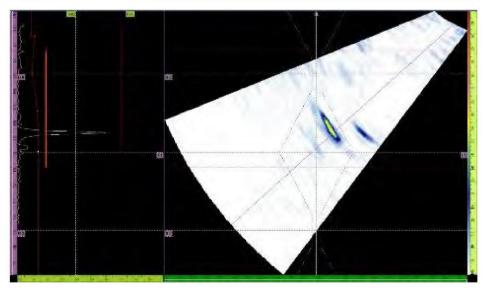
Weld C4 LOF @ 210 deg x 2"



Weld C4
LOF @ 260 deg x 1"



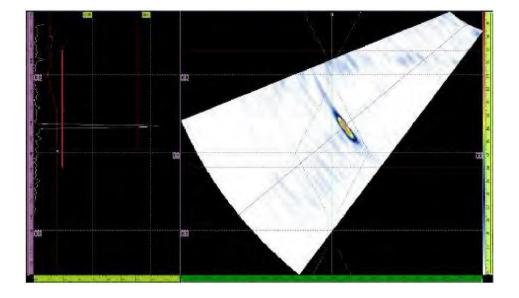
Weld C4 LIN @ 270 deg x 2.5"





EEI-PAUT-001 ATTACHMENT 1

Weld C4 LOF @ 315 deg x 8"



ATTACHMENT J NOZZLE PRESSURE TEST REPORT

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TEST REPORT

Submitted To: Enterprise Engineering, Inc.

Prime Contract: N39430-15-D-1678

Task Order Number: HCNA 15-D-1678 DO 011

January 19, 2018











Submitted by: Hansa Consult of North America, LLC 200 International Drive, Bldg. 120 Fortsmouth, N.H. 03801 info@hcna-llc.com www.hcna-llc.com



January 19, 2018 HCNA Project: 2017-1076 Page 2 of 9

Hansa Consult of North America, LLC

Red Hill - Tank 5, FLC Pearl Harbor, HI

January 19, 2018

Prepared for:

ENTERPRISE ENGINEERING, INC.

400 US Route 1 North, Suite B Falmouth, ME 04105

Telephone: 207-869-8006

Prepared and Submitted by:

HANSACONSULT NORTH AMERICA

200 International Drive Building 120 Portsmouth, N.H. 03801

Telephone: 603.422.8833 FAX: 603.422.8865



January 19, 2018

HCNA Project: 2017-1076

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2.1 Test Procedures	
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1 INTRODUCTION

Hansa Consult of North America, LLC (HCNA) has been tasked by Enterprise Engineering, Inc. (EEI) to perform mechanical integrity assessment testing at Red Hill - Tank 5, FLC Pearl Harbor, HI. Testing is conducted under prime contract(s) N39430-15-D-1678 (NAVFAC EXWC SB A/E IDQ) and N39430-15-D-1697 (NAVFAC EXWC LB A/E IDQ) and EEI order number HCNA 15-D-1678 DO 011. This subcontract provides for HCNA to conduct Hydrostatic and leak integrity testing of Tank 5 – Nozzle pipelines at Red Hill - Tank 5, FLC Pearl Harbor, HI, in accordance with the NAVFAC EXWC requirements for Conduct Modified API 653 OOS Inspection and established master service agreement. The final testing and certification for piping was conducted December 12 - 14, 2017 with passing results.

1.1 Purpose of Inspection

The purpose of the testing was to perform hydrostatic pressure testing in accordance with specified A/E engineering services including planning, design and mechanical integrity assessment as described at Red Hill - Tank 5, FLC Pearl Harbor, HI

1.2 Testing Criteria

The current scope is for HCNA to conduct four (4) hour pressure testing of piping system with *water* at 225 psig in accordance requirements – specifically HCNA Red Hill Mobile Testing Proposal r1 – dated 7 FEB 2016. HCNA Pressure-Step tightness testing to certify the section as "*tight*" shall occur following 4-hour pressure testing. Water as a test medium shall be furnished by EEI.

2 SITE AND EQUIPMENT DESCRIPTION

2.1 Test Procedures

HCNA provided testing of the pressurized sections at Red Hill - Tank 5, FLC Pearl Harbor, HI (See Table 1 for details). All test section pipe dimensions and volumes were reviewed and confirmed with EEI and AMPTIM personnel and validated by HCNA staff during the testing event. Line pressures were initially established by APTIM personnel. HCNA established test connection and a visual inspection was conducted. Prior to the start of recorded test, a "pre-stress" soak period was conducted for each section to allow the lines to stabilize at the final test pressures. During testing, visual inspections of the test sections were conducted at periodic intervals. A general description of the piping layout is provided in Section 2.4.

2.2 Test Sections

The test segment number and associated pipeline description for the test sections were as follows:

SECTIO	_	PIPELINE	PIPELINE	PIPELINE LENGTH [ft]						TOTAL
n No.	DESIGNATION	MATERIAL	SCHEDUL E	6"	8"	12"	18"	20"	32"	LENGTH [ft]
1	Tank 5 - 32" Nozzle Line	cs	STD.	0	0	0	0	5	44.2	49.2
2	Tank 5 - 18" Nozzle Line	cs	STD.	0	0	5	60.5	0	0	65.5
	TOTAL:			0	0	5	60.5	5	44.2	114.7

Table 1: General Pipeline Configuration Data of Tested Piping @ Red Hill - Tank 5, FLC Pearl Harbor, HI

Legend: CS: Carbon Steel



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2.3 <u>Test Fluid Specifications</u>

Water was used as the test medium for all static pressure testing during this event at Red Hill - Tank 5, FLC Pearl Harbor, HI.

2.4 <u>Description of Facility</u>

The testing at Red Hill - Tank 5, FLC Pearl Harbor, HI was conducted in accordance with NAVFAC EXWC requirements for A/E engineering services including planning, design and mechanical integrity assessment. The fuel system Red Hill FLC Pearl Harbor, HI consists of twenty (20) bulk field constructed underground storage tanks (BFCUSTs), pump shelter, transfer line, an eastern hydrant loop and a western hydrant loop. Currently, Red Hill - Tank 5, FLC Pearl Harbor, HI is out-of-service and undergoing required inspections. As part of the inspection, a Hydrostatic test of 32 & 18-inch nozzle lines of the Tank 5 fuel system were required with water followed by 3rd – party certification integrity testing. Since Tank 5 is out-of-service, nozzle pipelines were flanged on each end of the pipeline. Each section of pipeline was flanged on the interior of the tank and exits the tank wall into a tunnel, where the pipeline was flanged, and test connections established.

The length of the pipeline was calculated from provided documents as well as on-site personnel knowledge and shorter sections of pipe were measured by HCNA personnel. The piping diameter for the entire piping system ranges from 12" to 32".

2.5 Set-up and Testing

The test set-up, execution, and dismantling were conducted on December 12 - 14, 2017. Specific tables and photographs detail each section and are provided in Appendix A.



Figure 1: HCNA Pier Typical Test Setup Located at Red Hill - Tank 5, FLC Pearl Harbor, HI.

Equipment required to conduct the HCNA Leak Detection System tightness test was shipped
to the facility, and pressure recording equipment was installed on the test section, (please
refer to figures 2-7). HCNA equipment includes: portable pump, connection hoses, pressure
transmitter, data interface, the control and evaluation unit, laptop computer, as well as fuel
holding tank for test segment pressurization/depressurization.

All electrical components associated with the trailer and permanent skid are explosion-proof (Class I Div I) from the National Electrical Code (NEC), and the trailer is equipped with an onboard generator to provide power for all components. The trailer unit was independent from the local infrastructure during the tests. Fuel quality is guaranteed by the fact that all metal parts are made of stainless steel. (Please see Figures 2-7.)



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- Using the pump provided in the trailer or on the permanent skid, the test sections were
 pressurized to the high cycle test pressure in 50 psi intervals, and the system was visually
 inspected for leaks. No drips, seeps, etc. were identified and HCNA static pressure testing
 commenced after the test section pressures stabilized. A similar procedure was performed
 for each individual test section. Accordingly, the valve configuration used for each can be
 assumed satisfactory; otherwise there would have been symptoms of pressure decay during
 the test.
- Following the static pressure testing for each section, test equipment was disconnected and all fluid from hose connections was collected. Lastly, site personnel were notified at the completion of the testing and insured all valves were returned to their original positions.
- Detailed test section specifications, results, and photographs are provided in Appendices A E. The information is presented and delineated by test section.

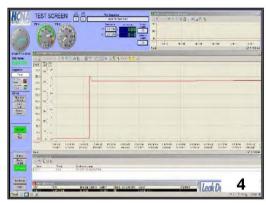


January 19, 2018 **HCNA Project: 2017-1076** Page 7 of 9

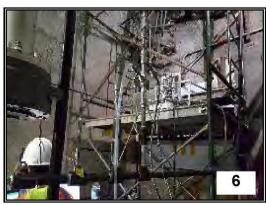
Description	Figure
HCNA LDS Portable Pump, Tank, and Pressure Device	2
HCNA LDS Suitcase - Test Control Screen	3
HCNA LDS Suitcase – Pressure Trend Screen	4
HCNA LDS Suitcase - Laptop and Printer	5
"Typical" Trailer Test Connection	6
Mobile Test Cart "Typical" Trailer Leak Simulation Test Connection	7

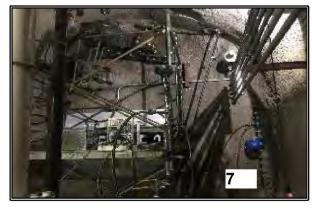
















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3 HCNA HYDROSTATIC LIQUID PRESSURE TEST PROTOCOL

3.1 Testing Protocols:

- California State Fire Marshal (CSFM): Pressure Testing Requirements for Hazardous Liquid Pipelines.
- American Petroleum Institute—Recommended Practice RP-1110: Pressure Testing of Liquid Petroleum Pipelines (with approved alternates as noted) and ASME B31.3.
- Test conducted with water as test medium.
- Pipeline test sections that were above ground were visually monitored for leaks during testing.
- Test sections were free of entrapped air as confirmed by bleeding of all high point vents.
- Proper spill response equipment and personnel were available during testing.
- HCNA portable equipment and tank provided adequate makeup and water recovery capacity.
- Pressure Transmitter(s) calibrated within the past 12 months utilized to measure test pressures. (Approved alternate to deadweight tester, calibration certificates attached in Appendix C)
- PLC based propriety software/visualization provided a permanent record of pressure/temperature vs. time.
- Test calculations, charts, and records comply with or are equivalent to those provided in API RP-1110.

3.2 Tester Qualification:

 HCNA personnel Michael Sherlock conducted the onsite testing and are listed as approved testers by CSFM.



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4 RESULTS / CONCLUSIONS

4.1 Test Assessment Methods

The pipeline test sections were assessed by the following methods:

4.1.1 Visual Inspection

Test section above ground exposed piping, fittings and other appurtenances were visually inspected and there was no evidence of external leakage.

4.1.2 Test Results

Testing was per contract specification piping system with *water* at 225 psig in accordance with the stated test equipment requirements/procedures and accepted industry practices. This testing comprised 4-hour hydrostatic strength testing followed by certified HCNA LDS activities utilizing the HCNA Pressure Step Test Methodology. Certificate pages are provided in Appendix C. The overall piping and test medium physical characteristics are evaluated using these collective techniques and meets the requirements for a combination "stress and strength" test.

The HCNA Leak Detection System Version 2.1 is capable of detecting a leak of 0.068 gallons per hour or 0.002% of line volume, with a probability of detection (P_D) > 95% and probability of false alarm (P_{FA}) < 5% at a reference pressure of 145 psi; as per Ken Wilcox Associates, Inc. Third Party Certifications. In accordance with the above stated "Criteria for Classification of Tightness", the results of all of the sections are summarized and provided below:

All test sections were successfully tested and passed based on the criteria established above.

SECTION No.	DESIGNATION	SECTION VOLUME [gal]	REFERENC E PRESSURE [PSI]	TOTAL LENGTH [ft]	TEST PRESSURE (MIN TO MAX) [PSI]	TEST DATE	Result
							WITHIN
1	Tank 5 - 32" Nozzle Line	1,837	225	49.2	231.7 – 231.8.	12/13/2017	ACCEPTABLE LIMITS
2	Tank 5 - 18" Nozzle Line	764	225	65.5	231.8 – 234.0	12/14/2017	WITHIN ACCEPTABLE LIMITS

Table 2: Hydrostatic Pressure Testing Section Results @ Red Hill - Tank 5, FLC Pearl Harbor, HI

SECTION No.	DESIGNATION	SECTION VOLUME [gal]	REFERENCE PRESSURE [PSI]	CERTIFIED MDLR [gal/h]	RECORDED LEAK RATE [gal/h]	TEST DATE	TEST RESULT
1	Tank 5 - 32" Nozzle Line	1,837	225	0.07	-0.01	12/13/2017	PASS
2	Tank 5 - 18" Nozzle Line	764	225	0.07	0.00	12/14/2017	PASS

Table 3: Leak Detection Sections Test Results @ Red Hill - Tank 5, FLC Pearl Harbor, HI.



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4.2 Problems Encountered

None.

5 RECOMMENDATIONS

See Appendix B.

6 HCNA TECHNOLOGY APPROVALS

The HCNA Leak Detection System technology has been recognized and approved by the following authorities:

- <u>U.S. EPA Third Party Certification:</u> Ken Wilcox Associates Evaluation of the Hansa Consult of North America, LLC Pipeline Leak Detection System, Version 2.0—Final Report. December 15, 2005
- <u>Listing by the National Work Group on Leak Detection Evaluations (NWGLDE):</u> for Pipeline Leak Detection Applications: HCNA Pressure Step Leak Detection System Listing. HCNA Pipeline Leak Detection System Version 2.0 Approval Letter, Issue Date March 7, 2006.
- <u>U.S. EPA Third Party Certification:</u> Ken Wilcox Associates Evaluation of the Hansa Consult of North America, LLC Pipeline Leak Detection System, Version 2.1—Final Report. May 24, 2010.
- <u>Listing by the National Work Group on Leak Detection Evaluations (NWGLDE):</u> for Pipeline Leak Detection Applications: HCNA Pressure Step Leak Detection System Listing. HCNA Pipeline Leak Detection System Version 2.1 – LINE TIGHTNESS TEST METHOD. Approval Letter, Issue Date February 17, 2011.
- <u>Listing by the National Work Group on Leak Detection Evaluations (NWGLDE):</u> for Pipeline Leak Detection Applications: HCNA Pressure Step Leak Detection System Listing. HCNA Pipeline Leak Detection System Version 2.1 LARGE DIAMETER LINE LEAK DETECTION METHOD (6 Inches Diameter or Above). Approval Letter, Issue Date February 17, 2011.
- <u>California Department of Forestry and Fire Protection--Office of the State Fire Marshal--Pipeline Safety Division:</u> Hydrostatic Testing Company Approved to Test Hazardous Liquid Pipelines, HCNA Listing Expires June 30, 2016. http://osfm.fire.ca.gov/pipeline/pdf/hydrotest/approhydro.p

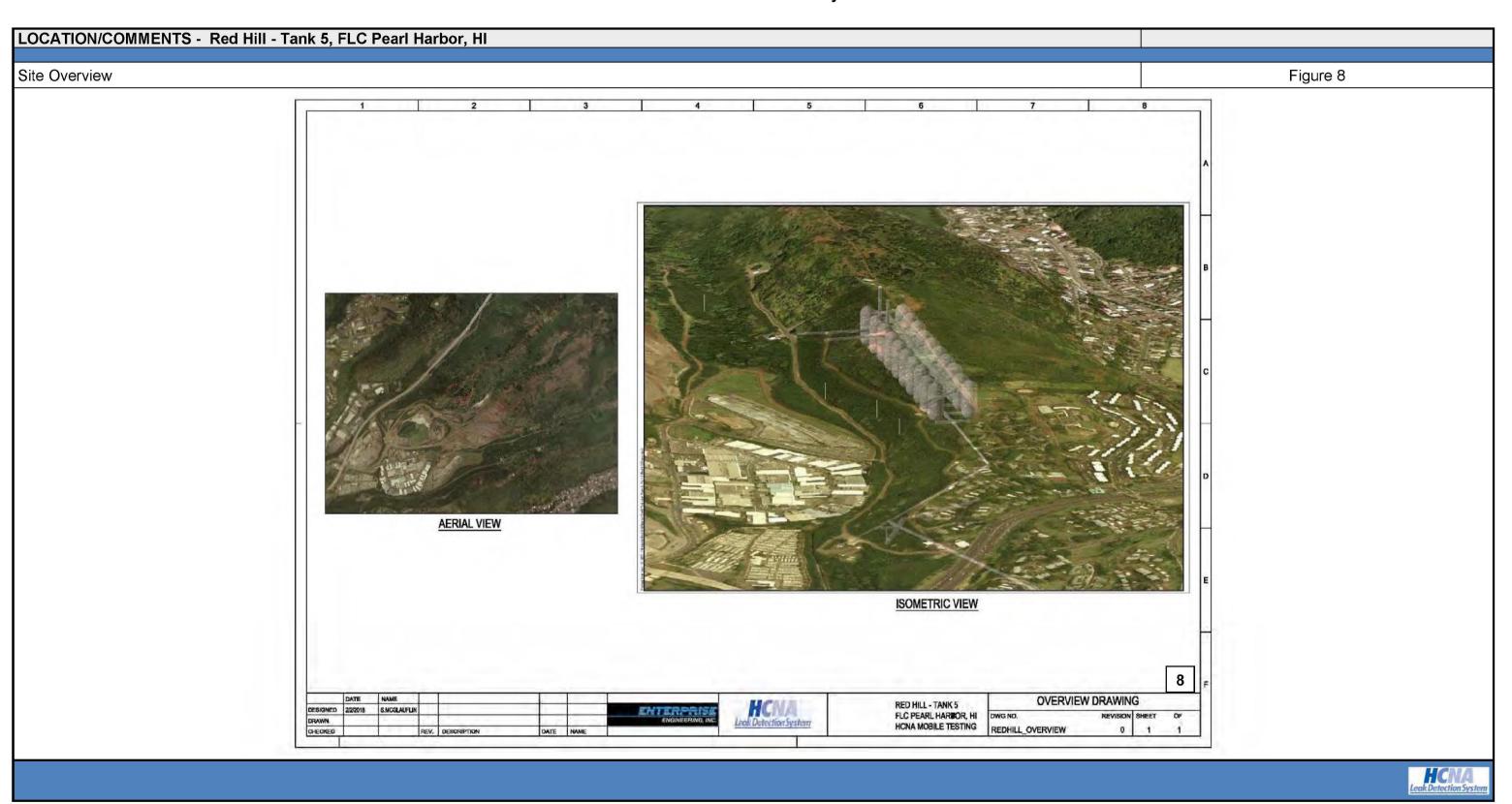


January 19, 2018 HCNA Project: 2017-1076 Appendix A

APPENDIX A: TEST SECTION DETAILS

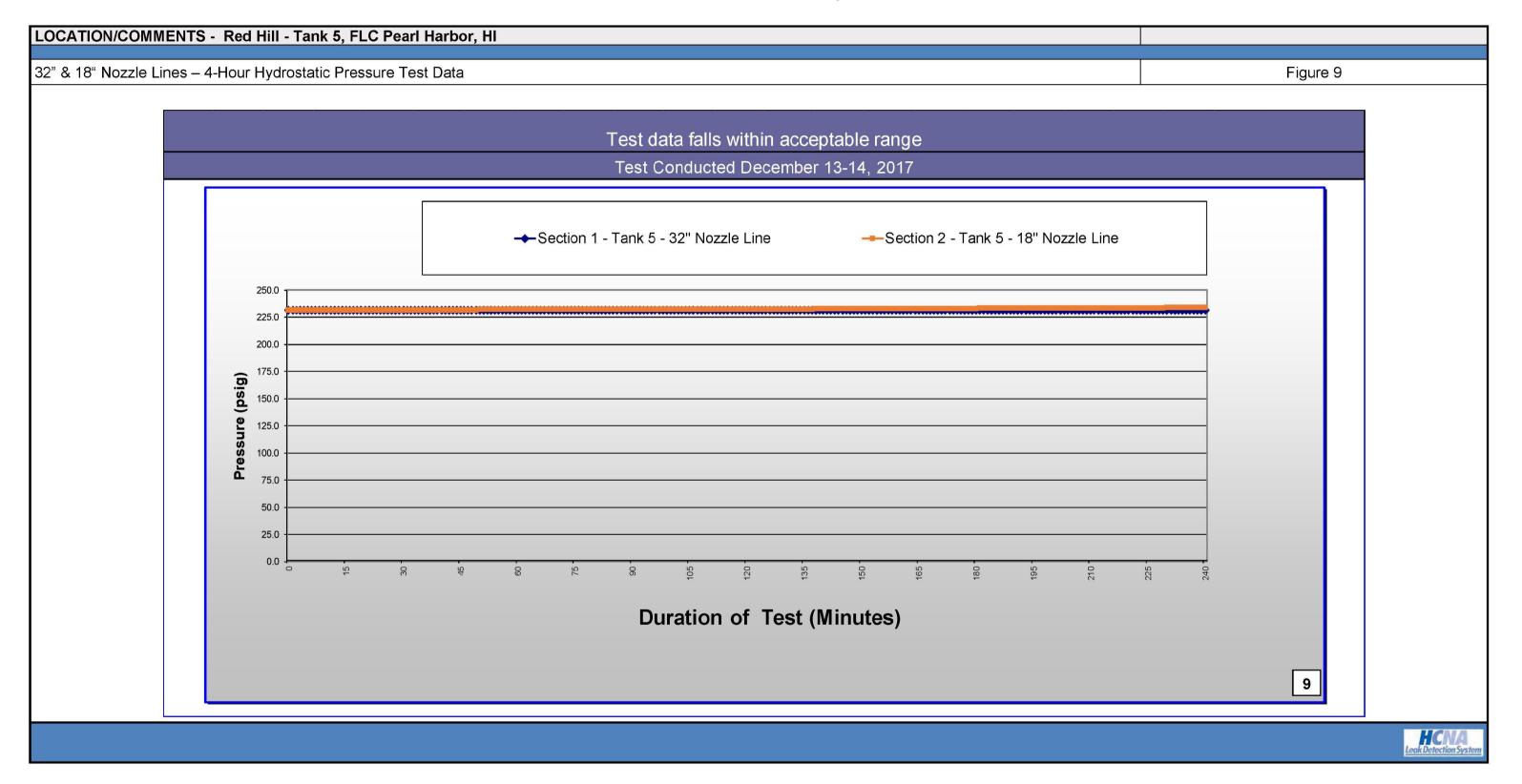


Appendix A





Hydrostatic test of 32" & 18" nozzle lines January 19, 2018



The information provided in this report is private, confidential and should not to be disclosed, copied or provided to anyone other than the client without the express written approval of HCNA LLC



January 19, 2018 HCNA Project: 2017-1076 Appendix A

HANSA	200 Internationa Bldg. 120			Internationa Bldg. 120		Tel: (603) 422-8833 Fax: (603) 422-8865			
		Red	Hill, FL	C Pearl H	larbor, HI, Oahı	u - Tank 5			
51.		Perf	orm l	Hydro	static Pre	ssure Tes	t		
Date / Time	e / Section:	2	0171213 50	1		User:	HCNA		
	est Section:	Section 1 -	Tank 5 - 32"	Nozzle Line		Date:	December 13, 2017		
					HCNA Pr	oject Number:	2017-1076		
		Pipe Segme	nt Specificat	ion					
Pipe Se	gment	Nominal	w.t.	Length (ft)		HCNA Engine	er: Michael Sherlock		
		Dia. (in.)	(in.)	Total	Volume (gal)	Notes:			
1		1.9000	3.9116	0.00	0.00				
2	-0.00	2.3750	3.9116	0.00	0.00				
3		6.6250	7.1120	0.00	0.00				
4	10	12.7500	9.5250	0.00	0.00				
5		16.0000	9.5250	0.00	0.00				
6		18.0000	9.5250	0.00	0.00				
7		20.0000 32.0000	9.5250 9.5250	5.00 44.20	75.60 1761.28				
9		0.0000	0.0000	0.00	0.00				
1		0.0000	0.0000	0.00	0.00				
1	u	0.0000	Totals:	49.20	1,836.88				
curingen			Locals	The State of the S	turer/Model				
quipmen.	rdor			Rosemount 305					
ressure Recor	nucl			HONA LDS Ver					
the second second second second	ssure Test Equ	nment		HUNA LDS VEI HUNA LDS Vei					
	ALL DESCRIPTION OF THE PARTY OF	proces		NIA NIA	301/2,0				
emperature R emperature Ti				N/A					
emperature in 4echanical Equ				HCNALDS - S	03				
Test D		Transmucer							
Sample		Pressure -					Remarks		
Number	Time	HCNASC-8 (psig)				(weather or	nditions or test activities		
1	8:00	231.8				Testing with w			
2	8:01	231.8		+ +		iesting with w	MASSE A		
3	8:02	231.8				Pipeline system	n was @ 231.8 psig when		
4	8:03	231.8				connection wa			
5	8:04	231.8			1 11				
6	8:05	231.8		1					
7	8:06	231.8							
8	8:07	231.8							
9	8:08	231.8) = - 1		- 6(
10	8:09	231.8							
11	8:10	231.8		7		- 1			
12	8:11	231.8		J. L					
13	8:12	231.8							
14	8:13	231.8		1	1				
15	8:14	231.8							
13700	8:15	231.8							
16									
16 17	8:16	231.8							
16 17 18	8:17	231.8							
16 17	200	the second secon							

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 1 of 6

1/26/201811:06 AM



Test Data:						
Sample		Pressure - HCNA SC-8				Remarks
Number	Time	(psig)				(weather conditions or test activities
21	8:20	231.8			1	
22	8:21	231.8			3	
23	8:22	231.8			1 /	
24	8:23	231.8				
25	8:24	231.8				
26	8:25	231.8				1 is a second se
27	8:26	231.8				
28	8:27	231.8				
29	8:28	231.8				
30	8:29	231.8				
31	8:30	231.8				
32	8:31	231.8				
33	8:32	231.8				
34	8:33	231.8				
35	8:34	231.8				
36	8:35	231.8				
37	8:36	231.8				
38	8:37	231.8				
39	8:38	231.8		_		
40	8:39	231.8		-		
41	8:40	231.8		_		
42	8:41	231.8		_		
43	8:42	231.8			_	
44	8:43	231.8		_		
45	8:44	231.8		_		
46	8:45	231.8				
47	8:46	231.8				
48	8:47	231.8				
49	8:48	231.8		_	_	
50	8:49	231.8				
51	8:50	231.8				
52	8:51	231.8				
53	8:52	231.8				
54	8:53	231.8				
55	8:54	231.8				
56	8:55	231.8				
57	8:56	231.8				
58	8:57	231.8				
59	8:58	231.8				
60	8:59	231.8				
61	9:00	231.8				
62	9:01	231.8				
63	9:02	231.8				
64	9:03	231.8	1			
65	9:04	231.8				
66	9:05	231.8				
67	9:06	231.8				
68	9:07	231.8				
69	9:08	231.8			_	
70	9:09	231.8		_	_	
71	9:09	231.8				
72	9:10			_		
	100000000000000000000000000000000000000	231.8				
73	9:12	231.8				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 2 of 6



Test Data:						
Sample		Pressure - HCNA SG-8				Remarks
Number	Time	(psig)				(weather conditions or test activities
75	9:14	231.8	The second			
76	9:15	231.8				
77	9:16	231.8				
78	9:17	231.8				
79	9:18	231.8		1		
80	9:19	231.8		1		
81	9:20	231.8				
82	9:21	231.8	_	<u> </u>		
83	9:22	231.8		+		
84	9:23	231.8	_			
85	9:24	231.8				
86	9:24					
		231.8				
87	9:26	231.8				
88	9:27	231.8				
89	9:28	231.8				
90	9:29	231.8				
91	9:30	231.8				
92	9:31	231.8				
93	9:32	231.8				
94	9:33	231.8				
95	9:34	231.8				
96	9:35	231.8				
97	9:36	231.8				
98	9:37	231.8				
99	9:38	231.8				
100	9:39	231.8				
101	9:40	231.8				
102	9:41	231.8				
103	9:42	231.8		1		
104	9:43	231.8				
105	9:44	231.8	_	1		
106	9:45	231.8				
107	9:46	231.8				
108	9:47	231.8	_	+		
109	9:48	231.8	_			
110	9:46	231.8	_	-		
111	9:49	231.8				
						7
112	9:51	231.8				
113	9:52	231.8				
114	9:53	231.8				
115	9:54	231.8				
116	9:55	231.8				
117	9:56	231.8				
118	9:57	231.8				
119	9:58	231.8				
120	9:59	231.8				
121	10:00	231.8				
122	10:01	231.8				
123	10:02	231.8				
124	10:03	231.8				
125	10:04	231.8				
126	10:05	231.8	1			
127	10:06	231.8				
128	10:07	231.8				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

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Test D	ata:		400		
		Pressure -			
Sample		HCNA SC-8			Remarks
Number	Time	(psig)			(weather conditions or test activities)
129	10:08	231.7			
130	10:09	231.7			
131	10:10	231.7			
132	10:11	231.7			
133	10:12	231.7			
134	10:13	231.7	- 1 1 1 1	1	
135	10:14	231.7			
136	10:15	231.7			
137	10:16	231.7			
138	10:17	231.7			
139	10:18	231.7			
140	10:19	231.7			
141	10:20	231.7			
142 143	10:21 10:22	231.7 231.7			
144	10:22	231.7			
145		170000000000000000000000000000000000000			
145	10:24 10:25	231.7 231.7			
147	10:26	231.7			
148	10:26	231.7			
149	10:28	231.7			
150	10:29	231.7			
151	10:30	231.7			
152	10:31	231.7			
153	10:32	231.7			
154	10:33	231.7			
155	10:34	231.7			
156	10:35	231.7	$\overline{}$		
157	10:36	231.7			
158	10:37	231.7			
159	10:38	231.7			
160	10:39	231.7			
161	10:40	231.7			
162	10:41	231.7			
163	10:42	231.7			
164	10:43	231.7			
165	10:44	231.7			
166	10:45	231.7			
167	10:46	231.7			
168	10:47	231.7			
169	10:48	231.7			
170	10:49	231.7			
171	10:50	231.7			
172	10:51	231.7			
173	10:52	231.7			
174	10:53	231.7			
175	10:54	231.7			
176	10:55	231.7			
177	10:56	231.7			
178	10:57	231.7			
179	10:58	231.7			
180	10:59	231.7			
181	11:00	231.7			
182	11:01	231.7			

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

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		Transmitte				
Sample Number	Time	Pressure - HCNA SG-8 (psig)				Remarks (weather conditions or test activities)
183	11:02	231.7				(PEDGIC) CONDICTOR OF CONTROL OF
184	11:02	231.7				
185	11:04	231.7		_		
186	11:05	231.7				
187	11:06	231.7				
188	11:07	231.7		_	_	
189	11:08	231.7	-			
190	11:09	231.7			_	
191	11:10	231.7				
192	11:11	231.7				
193	11:12	231.7		_		
194	11:12	231.7		_		
195	11:14	231.7				
196	11:15	231.8				
197	11:16	231.8				
198	11:17	231.8				
199	11:17	231.8			_	
200	11:19	231.8				
201	11:20	231.8		_	_	
202	11:21	231.8			_	
203	11:22	231.8		_		
204	11:23	231.8		_		
205	11:24	231.8				
206	11:25	231.8		_		
207	11:26	231.8		_		
208	11:27	231.8		_		
209	11:28	231.8		_	_	
210	11:29	231.8	-			-
211	11:30	231.8	_			
212	11:31	231.8		_		
213	11:32	231.8				
214	11:33	231.8				
215	11:34	231.8				
216	11:34	231.8			_	
217	11:36	231.8				
218	11:37	231.8		_		
219	11:38	231.8			_	
220	11:38	231.8			_	
221	11:39	231.8				
222	11:40	231.8			_	-
223	11:41	231.8		_	_	-
224	11:42	231.8				
225	11:45	231.8				
226	11:44	231.8				
227	11:45	231.8				
228	11:47	231.8				
229	11:47	231.8				
230	11:49	231.8				
231	11:50	231.8				
232	11:50	231.8				
233	11:52	231.8				
234	11:53	231.8				
235	11:53	231.8				
200	11:54	251.8				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

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Sample Number	Time	Pressure - HCNA SC-8 (psig)	Remarks (weather conditions or test activities)
237	11:56	231.8	
238	11:57	231.8	
239	11:58	231.8	
240	11:59	231.8	
241	12:00	231.8	

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

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SECTION 1: TANK 5 - 32" NOZZLE LINE								
ISOLATION	OPEN	CLOSED	Location/Comments	FIGURE				
Interior Tank 5		Flanged	Interior Tank 5	1-1				
Nozzle Pipeline		Flanged	Interior Tank 5	1-2				
Isolation Flange – Interior Tank 5		Flanged	Interior Tank 5	1-3				
Isolation Flange – Interior Tank 5		Flanged	Interior Tank 5	1-4				
Test Connection and Water Fill Flange		Flanged	Tank 5 – Tunnel	1-5				
Test Equipment on Scaffold		Flanged	Tank 5 – Tunnel	1-6				
		TEST CONNECTION	v	FIGURE				
Connection for HCNA LDS Suitcase to	est equip	ment – PC, pump, pres:	sure transmitter, and portable PLC.	1-7				

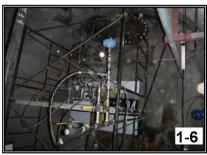














See below Appendix B.





200 Internation Bldg. 12 HANSACONSULT					l Drive		503) 422-8833 503) 422-8865	
		Red	Hill, FL	C Pearl H	larbor, Hl, Oahu	ı - Tank 5		
		Per	form	Hydro	ostatic Pre	essure Test		
ate / Tim	ne / Section:		201 7 1214 S0	2		User: HCNA		
	Test Section:	Section 2 -	Tank 5 - 18"	Nozzle Line		Date:	December 14, 2017	
		Nine Comme	nt Specificat	Sala.	HCNA Pr	oject Number:	2017-1076	
Pipe Si	egment	Nominal	w.t.	Length (ft)		HCNA Engineer:	Michael Sherlock	
		Dia (in.)	(in.)	Total	Volume (gal)	Notes:		
	1	1.9000	3.9116	0.00	0.00			
	2	2.3750	3.9116	0.00	0.00			
	4	6.6250 12.7500	7.1120 9.5250	0.00 5.00	0.00 29.38			
	5	16.0000	9.5250	0.00	0.00			
	6	18.0000	9.5250	60.50	734.58			
	7	20.0000	9.5250	0.00	0.00			
	8	32,0000	9.5250	0.00	0.00			
	9	0.0000	0.0000	0.00	0.00			
1	10	0.0000	0.0000	0.00	0.00			
uipment			Totals:	65.50	763.96 turer/Model			
ssure Reco				Roserrount 305	A COUNTY OF THE PARTY OF THE PA			
				KOSCH BUILDOS	10			
				HONAL DS Ver	sion 2 ft			
ta Interface		pment		HCNALDS Ver HCNALDS Ver	1			
ita Interface	essure Test Equi	pment		HCNALDS Ver HCNALDS Ver N/A	1			
ta Interface tomated Pre mperature F	essure Test Equi Recorder	pment		HCNALDS Ver	1			
ita Interface tomated Pre	essure Test Equi Recorder Fransmitte:	pment		HCNALDS√er N∕A	sion 2.0			
ta Interface tomated Pre mperature F mperature T	essure Test Equi Recorder Fransmitter quipment	prnent		HCNA LDS Ver N/A N/A	sion 2.0			
ta Interface tornaled Pre mperature F mperature T chanical Eq	essure Test Equi Recorder Fransmitter quipment	pment		HCNA LDS Ver N/A N/A	sion 2.0		- 0	
ta Interface tomated Pre mperature F mperature T chanical Eq est D	essure Test Equi Recorder Fransmitter quipment	Transmiker Pressure -		HCNA LDS Ver N/A N/A	sion 2.0		Remarks	
ia interface tornated Pre imperature F imperature T chanical Eq est D ample	essure Test Equi Recorder Fransmitter quipment	Pressure - HCNASC-8		HCNA LDS Ver N/A N/A	sion 2.0		Remarks Itiions or test activities)	
ia Interface omaled Pre inperature F inperature T chanical Eq est D ample	essure Test Equi Recorder Fransmitter quipment	Transmiker Pressure -		HCNA LDS Ver N/A N/A	sion 2.0		litions or test activities)	
ia Interface connaled Pre imperature Pre imperature T chanical Eq est D ample umber 1 2	Recorder Fransmitter Transmitter Transmitt	Pressure - HENASC-8 (psig) 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water	litions or test activities)	
ia Interface remarked Pre imperature Pre imperature Tehanical Eq est D ample umber 1 2 3	recover Frankritter quarter to the transmitter quarter to the transmitter quarter to the transmitter to the	Pressure - HCNASC-8 (psig) 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system wa	litions or test activities) as @ 250.3 psig when tes	
a Interface ornated Pro imperature Pro imperature Pro imperature Techanical Eq est D ample umber 1 2 3 4	Pessure Test Equi Recorder Fransmiller quipment Data: Time 7:15 7:16 7:17 7:18	Pressure - HCNASC-8 (ps/g) 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water	litions or test activities) as @ 250.3 psig when tes	
ia Interface omated Pre imperature in imperature in chanical Equ est D ample umber 1 2 3 4 5	Recorder Fransmitter Quipment Fransmitter Transmitter	Pressure - HENASC-8 (psig.) 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system wa connection was co	litions or test activities) as @ 250.3 psig when tes impleted.	
ia Interface omatica Pre imperature in imperature in chanical Equ est D ample umber 1 2 3 4 5 6	ressure Test Equi Recorder Fransmitter quipment Jata: Time 7:15 7:16 7:17 7:18 7:19 7:20	Transmitter Pressure - HCNASC-8 (ASIC) 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
ia Interface omated Pre imperature in imperature in chanical Equ est D ample umber 1 2 3 4 5	Recorder Fransmitter Quipment Fransmitter Transmitter	Pressure - HENASC-8 (psig.) 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system wa connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
ta Interface ormated Pre- imperature Pre- imperature I interface I Ed est D ample umber 1 2 3 4 5 6 7	Pessure Test Equi Recorder Transmitter quiprine d Partie 7:15 7:16 7:17 7:18 7:19 7:20 7:21	Transmitter Pressure - HCNASCS (assc) 231.8 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la Interfaca omated Pre imperature in merature in chanical Eq est D ample umber 1 2 3 4 5 6 7 8 9 10	Page 1	Pressure - HENASC-8 (ps/g) 231.8 231		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la Interface omated Pre imperature in imperature in chanical Eq est D ample umber 1 2 3 4 5 6 7 8 9 10 11	Firms 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25	Transmitter Pressure - HCNASC-8 (ASIS) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la Interfaca comisted Pre imperature Pr imperature Pr imperature I chanical Eq est D ample ample ample 2 3 4 5 6 7 8 9 10 11 12	Firme 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26	Transmitter Pressure - HENASC-8 (nsig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la interfaca tormated Pre imperature Priminerature Pre imperature I chanical Equ est D ample umber 1 2 3 4 5 6 7 8 9 10 11 12 13	Time 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26 7:27	Transmitter Pressure - HCNASCS (assc) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la interfaca tormated Pre imperature Pr imperature Pr imperature I chanical Eq est D ample umber 1 2 3 4 5 6 7 8 9 10 11 12	Firme 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26	Transmitter Pressure - HENASC-8 (nsig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
a Interface omated Pre imperature in imperature of the interface ample a	Firms 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:24 7:25 7:26 7:27	Pressure - HCMASC-8 (psig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.9 231.9 231.9		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
a miletrace consider Pre- imperature Pre- impe	Time 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26 7:27 7:28 7:29 7:30 7:31	Transmitter Pressure - HCMSGS 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.9 231.9 231.9 231.9		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
a Interface ormated Pre- Imperature Pre- Imper	Firms 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26 7:27 7:28 7:29 7:30 7:31 7:32	Pressure - HEMASUR (psig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.9 231.9 231.9 231.9 231.9 231.9 231.9		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la interfaca lormated Pre imperature is imperature is interface. Equ est D ample umber 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	Page 1	Pressure - HCMASC-8 (psig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.9 231.9 231.9 231.9 231.9 231.9 231.9 231.9 231.9		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	
la interfaca tormated Pre imperature Priminerature I chanical Equ est D ample umber 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Firms 7:15 7:16 7:17 7:18 7:19 7:20 7:21 7:22 7:23 7:24 7:25 7:26 7:27 7:28 7:29 7:30 7:31 7:32	Pressure - HEMASUR (psig) 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.8 231.9 231.9 231.9 231.9 231.9 231.9 231.9		HCNA LDS Ver N/A N/A	sion 2.0	(weather cond Testing with water Pipeline system was connection was co	litions or test activities) as @ 250.3 psig when tes mpleted. ure lowered to 231.8 psig	

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 1 of 5



Test D	ata:					
Sample Number	Time	Pressure - HGNA SC-8				Remarks (weather conditions or test activities)
_		(psig)			-	(Weather Collabora of test activities)
23	7:37	231.9		-		
	7:38	231,9		-		
25	7:39 7:40	231.9				
26		231.9				
27	7:41 7:42	231.9			_	
	7:42	231.9				
30	7:43	231.9				
31	7:44	231.9	- - 			
32	7:45	231.9				
33	7:40					
		231.9				
34	7:48 7:49	231.9				
35 36	7:49 7:50	232.0 232.0		-		
37	7:50					
	7:51	232.0				
38 39		232.0				
	7:53	232.0				
40	7:54	232.0				
41	7:55	232.0				
42	7:56	232.0	\rightarrow			
43	7:57	232.0	-			
44	7:58 7:59	232.0				
45		232.0				
46 47	8:00	232.0				
	8:01	232.0	\rightarrow			
48	8:02	232.0				
49	8:03	232.0				
50	8:04	232.0				
51	8:05	232.1				
52	8:06	232.1				
53	8:07	232.1				
54	8:08	232.1				
55	8:09	232.1	\rightarrow			
56	8:10	232.1				
57	8:11	232.1	_			
58	8:12	232.1				
59	8:13	232.1				
60	8:14	232.1	\rightarrow			
61	8:15	232.1				
62	8:16	232.1				
63	8:17	232.1				
64	8:18	232.1	_			
65	8:19	232.1				
66	8:20	232.1				
67	8:21	232.1				
68	8:22	232.2				
69	8:23	232.2				
70	8:24	232.2	\rightarrow			
71	8:25	232.2				
72	8:26	232.2	\rightarrow			
73	8:27	232.2				
74	8:28	232.2	_			
75	8:29	232.2				
76	8:30	232.2	\rightarrow			
77 78	8:31 8:32	232.2 232.2				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 2 of 5



Sample Number 79 80 81 82 83 84 85 86	8:33 8:34 8:35 8:36 8:37 8:38	Pressure - HCNA 5C-8 (psig) 232.2 232.2				Remarks
79 80 81 82 83 84 85	8:33 8:34 8:35 8:36 8:37	HGNA 5C-8 (psig) 232.2 232.2				Remarks
79 80 81 82 83 84 85 86	8:33 8:34 8:35 8:36 8:37	(psig) 232.2 232.2				
80 81 82 83 84 85 86	8:34 8:35 8:36 8:37	232.2				(weather conditions or test activities)
81 82 83 84 85 86	8:35 8:36 8:37					
82 83 84 85 86	8:36 8:37			30	- 1	
83 84 85 86	8:37	232.2				
84 85 86		232.2	1		4	
85 86	0.20	232.2			1	
86	0,30	232.2	- 1	- 1	- 1	
	8:39	232.2				
87	8:40	232.2				
0,	8:41	232.2				
88	8:42	232.2				
89	8:43	232.2				
90	8:44	232.2				
91	8:45	232.3				
92	8:46	232.3				
93	8:47	232.3				
94	8:48	232.3				
95	8:49	232.3				
96	8:50	232.3				
97	8:51	232.3				
98	8:52	232.3				
99	8:53	232.3				
100	8:54	232.3				
101	8:55	232.3				
102	8:56	232.3				
103	8:57	232.3				
104	8:58	232.3				
105	8:59	232.3				
106	9:00	232.3				
107	9:01	232.3				
108	9:02	232.3				
109	9:03	232.3				
110	9:04	232.3				
111	9:05	232.3				
112	9:06	232.3				
113	9:07	232.3				
114	9:08	232.3				
115	9:09	232.3				
116	9:10	232.4				
117	9:11	232.4				+
118	9:11	232.4				+
119	9:12	232.4				
120	9:13	232.4				+
121	9:14	232.4				
122	9:16	232.4				
123	9:16	232.4				+
124	9:17	232.4				
125	9:18	232.4				+
126	9:19	232.5				
127	9:20	232.5				+
						
128	9:22	232.5				Small was at 3% and the state of the state o
129	9:23	232.6				Small weep at 2" connection used by APTIN
130	9:24	232.6				to fill line with water. HCNA further tighten
131	9:25	232.6				connection and weep no longer evident.
132	9:26	232.6	$\overline{}$			
133 134	9:27 9:28	232.6 232.6				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 3 of 5



Test Data:						
Sample		Pressure - HCNA 5C-8				Remarks
Number	Time	(psig)				(weather conditions or test activities)
135	9:29	232.6			- 1	7
136	9:30	232,6		30	- 10	
137	9:31	232.6				
138	9:32	232.6	- 1	- 4		
139	9:33	232.7				
140	9:34	232.7		- ()		
141	9:35	232.7				
142	9:36	232.7				
143	9:37	232.7				
144	9:38	232.7				
145	9:39	232.8				
146	9:40	232.8				
147	9:41	232.8				
148	9:42	232.8				
149	9:43	232.8				
150	9:44	232.8				
151	9:45	232.8				
152	9:46	232.8				
153	9:47	232.8				
154	9:48	232.8				
155	9:49	232.9				
156	9:50	232.9				
157	9:51	232.9				
158	9:52	232.9				
159	9:53	232.9				
160	9:54	232.9				
161	9:55	233.0				
162	9:56	233.0				
163	9:57	233.0				
164	9:58	233.0				
165	9:59	233.0				
166	10:00	233.0				
167	10:01	233.1				
168	10:02	233.1				
169	10:03	233.1				
170	10:04	233.1				
171	10:05	233.1				
172	10:06	233.1				
173	10:07	233.1				
174	10:08	233.1		$\overline{}$		
175	10:09	233.1				
176	10:10	233.1				
177	10:11	233.2		-	_	
178	10:12	233.2				1
179	10:13	233.2	- 			
180	10:14	233.2		-		
181	10:15	233.2				
182	10:16	233.3				+
183	10:17	233.3			_	+
184	10:18	233.3	- 			+
185	10:18	233.3				+
186	10:19	233.3				+
187	10:20	233.3		-		+
188	10:21	233.3			_	+
189	10:22	233.3			_	+
190	10:23	233.3				

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

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Sample Number	Time	Pressure - HCNA 5C-8 (psig)			Remarks (weather conditions or test activities)
191	10:25	233.3			(Westing Constitutions of test sections)
192	10:26	233.4			1
193	10:27	233.4			
194	10:28	233.4			
195	10:29	233.4			
196	10:30	233.4			
197	10:31	233.4		+	
198	10:32	233.4			
199	10:33	233.5			
200	10:34	233.5			
201	10:35	233.5			
202	10:36	233.5			
203	10:37	233.5			
204	10:38	233.5			
205	10:39	233.5			
206	10:40	233.6	 		
207	10:41	233.6			
208	10:42	233.6			
209	10:43	233.6			
210	10:44	233.6			
211	10:45	233.6			
212	10:46	233.6			
213	10:47	233.6			
214	10:48	233.6			
215	10:49	233.6			
216	10:50	233.6			
217	10:51	233.7			
218	10:52	233.7			
219	10:53	233.7			
220	10:54	233.7			
221	10:55	233.7			
222	10:56	233.7			
223	10:57	233.8			
224	10:58	233.8			
225	10:59	233.8			
226	11:00	233.8			
227	11:01	233.8			
228	11:02	233.8			
229	11:03	233.8			
230	11:04	233.8			
231	11:05	233.9			
232	11:06	233.9			
233	11:07	233.9			
234	11:08	233.9	41 2	4 1	
235	11:09	233,9			
236	11:10	233.9	TI IV TO I	1	
237	11:11	233.9	44 5		
238	11:12	233.9	- 1 -	4 1 4	
239	11:13	233.9		11/2	
240	11:14	234.0			
241	11:15	234.0			

Red Hill, FLC Pearl Harbor, HI, Oahu - Tank 5

Page 5 of 5



SECTION 2: TANK 5 - 18" NOZZLE LINE								
Isolation	OPEN	CLOSED	Location/Comments	FIGURE				
Interior Tank 5		Flanged	Interior Tank 5	1-1				
Nozzle Pipeline		Flanged	Interior Tank 5	1-2				
Isolation Flange – Interior Tank 5		Flanged	Interior Tank 5	1-3				
Isolation Flange – Interior Tank 5		Flanged	Interior Tank 5	1-4				
Power Connectivity – Interior Tank 5		Flanged	Interior Tank 5	1-5				
Test Connection and Water Fill Flange		Flanged	Tank 5 – Tunnel	1-6				
	TEST CONNECTION							
Connection for HCNA LDS Suitcase to	est equip	ment – PC, pump, pres	sure transmitter, and portable PLC.	1-7				















See below Appendix B.



APPENDIX B: SITE SPECIFIC INFORMATION



HCNA Representative(s):	Karl Overman, Michael Sherlock, and Douglas Vorderbruggen	Date of Service	December 12 - 14, 2017

Task Order Number:	HCNA 15-D-1678 DO 011	
Primary/Site Contact (EEI)	Telephone	Email:
Douglas Kieley, P.E	Cell Phone: (207) 838-1250	kieleyd@eeiteam.com
Kit Dahlstrom	Cell Phone: (907) 529-7827	dahlstromka@eeiteam.com

Project Comments

December 10-12, 2017

On December 10th, HCNA engineers mobilized to Oahu, HI. On December 11th, HCNA contacted EEI representative Mr. Kit Dahlstrom regarding HCNA LDS test equipment. Mr. Dahlstrom confirmed receipt of equipment and we coordinated kick-off and safety meeting for December 12th. On December 12th, HCNA personnel Karl Overman, Michael Sherlock, and Douglas Vorderbruggen meet with Mr. Dahlstrom at Red Hill fuel facility, then proceeded to FLC Pearl Harbor to completed required badging process. Once badging was completed, all returned to Red Hill facility and completed required site-specific health and safety program. HCNA LDS test equipment was moved to lower-level tunnel access outside tank 5 valving and piping. Test section was previously isolated and pressurized with water, HCNA LDS test equipment was unpacked and connected test section 1 – 32" Nozzle line.

December 13, 2017

On December 13th, HCNA engineers arrived at Red Hill - Tank 5, FLC Pearl Harbor, HI for 0600 safety meeting. Following meeting, HCNA meet with EEI representative(s) Mr. Douglas Kieley and Mr. Kit Dahlstrom regarding testing schedule. Additionally, we meet with APTIM representative Mr. Eric Yatabe, who is coordinating required mechanical and packing of test sections for EEI. We meet at upper-level Tank 5, had another safety brief, confirmed test activities, which included Doug Vorderbruggen gaining access to the inside of Tank 5 to inspect test section flange isolation. We again proceeded lower-level tunnel access outside tank 5 and finalized HCNA LDS test set-up. Pressure still remained on test section 1 – 32" Nozzle line, piping was inspected for leaks, once satisfied, test was started at approximately 0800. Additionally, we meet with APTIM representative Mr. Eric Yatabe, who is coordinating required mechanical and packing of test sections for EEI. HCNA performed 4-hour stress, several LDS tests, and leak simulations, with satisfactory results. Once required testing was complete, system was depressurized, hoses were disconnected, and equipment was stowed/packed for testing of test section 2 – 18" Nozzle line. APTIM personnel still needed to isolate, fill, and pressurize the next section. We coordinated schedule for December 14 – 0600 safety meeting - and departed site.

HCNA Pipeline Pressure/Leak Integrity Testing Site: Red Hill - Tank 5, FLC Pearl Harbor, HI Hydrostatic test of 32" & 18" nozzle lines



January 19, 2018 HCNA Project: 2017-1076 Appendix B

December 14, 2017

On December 14th, HCNA engineers arrived at Red Hill - Tank 5, FLC Pearl Harbor, HI for 0600 safety meeting. Following meeting, HCNA meet with EEI representative(s) Mr. Douglas Kieley and Mr. Kit Dahlstrom regarding testing schedule. We meet AMPTIM and EEI personnel at upper-level Tank 5, had another safety brief, confirmed test activities, which included Doug Vorderbruggen gaining access to the inside of Tank 5 to inspect test section flange isolation. We again proceeded lower-level tunnel access outside tank 5 and finalized HCNA LDS test set-up. Pressure still remained on test section 2 – 18" Nozzle line, piping was inspected for leaks, once satisfied, test was started at approximately 0715. HCNA performed 4-hour stress, several LDS tests, and leak simulations, with satisfactory results. Once required testing was complete, system was depressurized, hoses were disconnected, and equipment was packed in HCNA vehicle for return shipment to HCNA office. We provided out-brief to EEI personnel and departed site. On December 15th, HCNA personnel shipped HCNA LDS equipment and demobilized from Oahu, HI.



APPENDIX C: TEST CERTIFICATION REPORTS





200 International Drive Bldg. 120 Portsmouth, NH 03801 Tel +1 - 603 - 422 8833 Fax +1 - 603 - 422 8865 E-Mail info@hcna-llc.com Infernet www.hcna-llc.com



Leak Detection Certification

Location: Red Hill - Tank 5, FLC Pearl Harbor, HI

Date:

December 14, 2017

Customer: Enterprise Engineering, Inc.

Project No.: 2017 1076

Project: HCNAI

HCNA Pipeline Pressure/Leak Integrity Testing

NAVFAC EXWC

General Pipeline Configuration Data:

SECTIO		PIPELINE	PIPELINE	PIPELINE LENGTH [ft]						TOTAL
N No.	DESIGNATION	MATERIAL	SCHEDUL E	6"	8"	12"	18 ^u	20"	32"	LENGTH [代]
1	Tank 5 - 32" Nozzle Line	CS	STD.	0	0	0	0	5	44,2	49.2
2	Tank 5 - 18" Nozzle Line	cs	STD.	0	0	5	60.5	0	0	65.5
Legend: 55: Staint CS: Carbo CP: Cappe STD: Stand	Steel									
	TOTAL			0	0	5	60.5	5	44.2	114.7

Table 1: General Pipeline Configuration Data of Tested Fuel System @ Red Hill - Tank 5, FLC Pearl Harbor, Hi

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**Sometimes (Continued (Conti





200 International Drive Bldg. 120 Portsmouth, NH 03801

+1 - 603 - 422 8833 Tel +1 - 603 - 422 8865 Fax E-Mail

info@hcna-llg.com Internet www.hona-lic.com



Leak Detection Certification

Certification Test Data:

Section No.	DESIGNATION	SECTION VOLUME [gsl]	REFERENCE PRESSURE [PSI]	CERTRIED MDLR [gai/h]	RECORDED LEAK RATE (gailth)	TEST DATE	TEST RESULT
1	Tank 5 - 32" Nozzle Line	1,837	225	0.07	-0,01	12/13/2017	PASS
2	Tank 5 - 18' Nozzie Line	764	225	0.07	0,00	12/14/2017	PASS

Table 2: Leak Detection Sections' Results of Tested Fuel System @ Red Hill - Tank 5, FLC Pearl Harbor, Hi

Result Criteria:

PASS:

Test results were within the stated MDLR.

FAIL

Test results exceed the stated MDLR.

Hansa Consult of North America, LLC (HCNA) certifies that the piping listed in the above table has been tested by means of the HCNA Leak Detection System, which meets the criteria set forth in U.S. EPA/530/UST-90/010 for precision leak test.

The HCNA Leak Detection System method is capable of detecting leaks of 0.068 gallons per hour or 0.002% of line volume at a reference pressure of 145 psi, with a probability of detection (PD) > 95% and a probability of false alarm (PFA) < 5%; as per Ken Wilcox Associates, Inc. Third Party Certifications.

In accordance with the above stated "Criteria for Classification of Tightness", HCNA hereby cartifies that this piping was tested on the date(s) and with the result(s) at the respective reference pressure stated in the above table.

Poltsmouth, New Hampshire, December 14, 2017

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APPENDIX D: INSTRUMENT CALIBRATION CERTIFICATES





Asset Optimization Services

Instrument & Valve Services

Calibration Report

η Request Number: 1620218

Customer:	Hansa Consult North America	Date:	Aug 28,2017
Location:	Portsmouth, NH	Application:	Fuel Trailer Spare pressure
Manufacturer:	Rosemount	Tag Number:	PT-SPARE-en821117
Model Number :	3051S1TG3A2A11A1AE5M5	Serial Number:	821117
Range:	0-800	Units:	PSIG

Measurement Standards:							
Model:	Serial Number:	Calibration Date:	Calibration Due:				
Fluke 754 Calibrator	3462002	30-July-17	8-Aug-1				
Fluke 700P08 pressure module	98850802	18-Nov-16	25-Nov-1				

. Environmental / Ambient Conditions: 20deg C, and 30%RH

	Transmi	tter Calibration	Data:				
Input	Data, in	Transfer Function/Output Type: Linear					
PSIG:		Output Data, in milliAmps DC::					
Percent of Span:	Applied Value:	As Found:	Nominal:	As Left:			
0.00%	0.00	3.997	4.000	3.997			
20.00%	160.00	7.194	7.200	7.194			
40.00%	320.00	10.394	10.400	10.394			
60.00%	480.00	13.595	13.600	13.595			
80.00%	640.00	16.793	16.800	16.793			
100.00%	800.00	19.993	20.000	19.993			

Certification of Traceability to NIST:

This calibration is traceable to the National Institute of Standards and Technology, or to national, international, or intrinsic standards of measurement, with supportive data available at Rosemount Inc. for audit verification. This report shall not be reproduced except in full.

Comments/Notes

1. Within spec as found, with less than 0.03% error. No adjustment necessary. Found set to 0 to 800 psig

Accuracy Specification: ±0.25 % of Span Result: Meets applicable specifications

A. Variano

8/28/17

Service Engineer

ROSEMOUNT

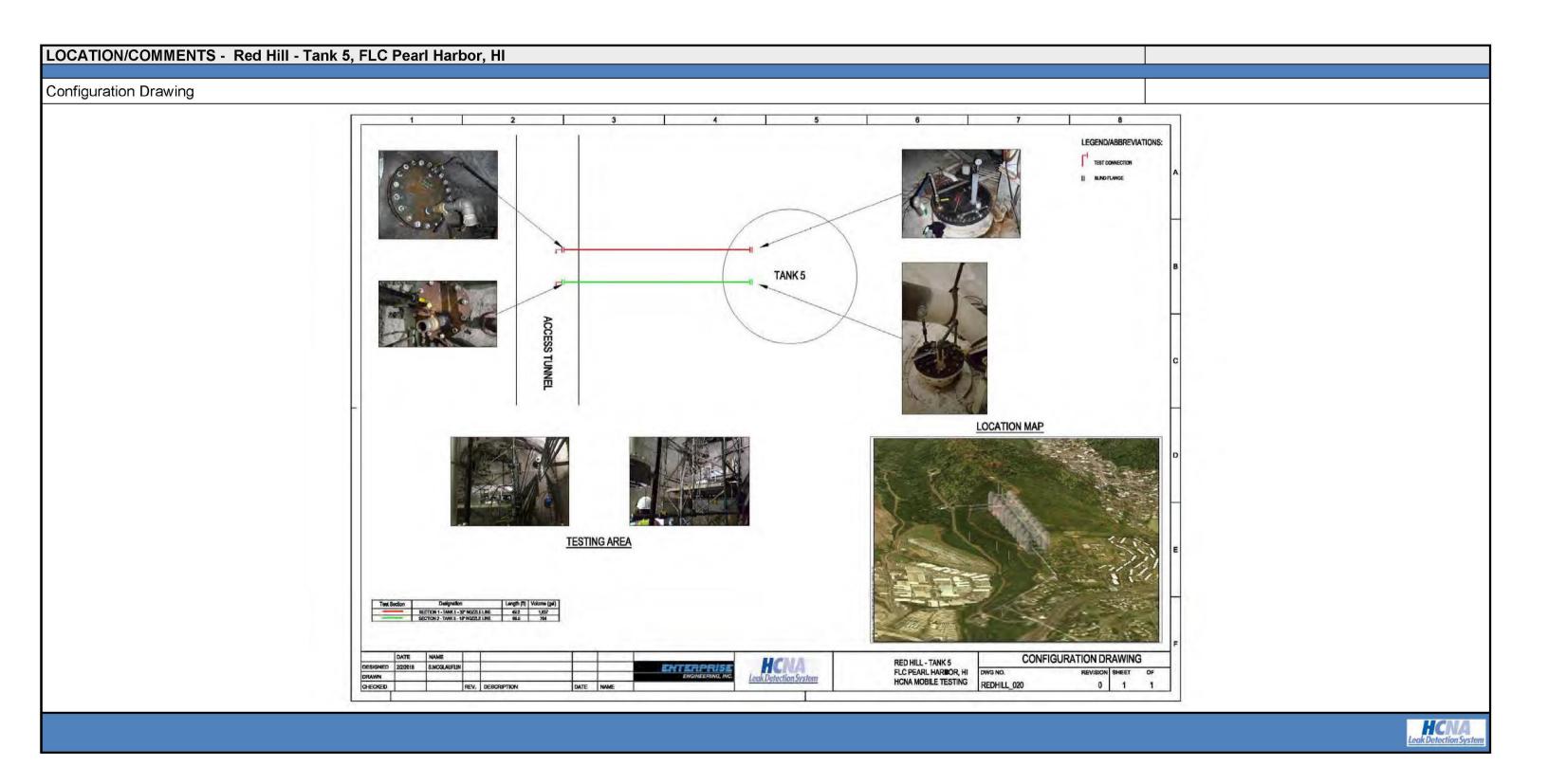
Emerson Process Management 12001 Technology Drive Eden Prairie, JMN 55344 USA T 1-800-654-776 E 1-952-828-334



APPENDIX E: CONFIGURATION DRAWINGS

January 19, 2018 HCNA Project: 2017-1076







APPENDIX F: CA. OFFICE OF THE STATE FIRE MARSHAL - APPROVAL





California Department of Forestry and Fire Protection

Office of the State Fire Marshal

Pipeline Safety Division

Approved Hydrostatic Testing Companies

LIST EXPIRES June 30, 2018

The following companies have met minimum requirements and are approved to hydrostatically test hazardous liquid pipelines in California for the period specified. The California State Fire Marshal makes no recommendations and has no information or involvement in the charges for such testing. Testing may be witnessed or certified only by the individual employees as specified on the individual company pages.

CURRENT AS OF 08/21/2017

AHS Construction/Century Calibrating

Akri Hydrotesting

ARB

Baker Hughes Process and Pipeline Service LLC

Barnard Pipeline, Inc.

Brothers Pipeline Corp

Brown Integrity, LLC

CCI - Antioch

CCI - Visalia

CMAC

Coastal Chemical Co., LLC

Doty Bros. Construction Company Goldsman Construction Company, Inc.

Hansa Consult of North America, LLC (HCNA)

Harder Mechanical Contractors, Inc.

Interspec LLC

Milbar Hydro-Test, Inc.

NAVFAC Engineering & Expeditionary Warfare Ctr

Performance Mechanical, Inc.

Pipeline Petroleum Services, Inc.

PROS, Inc.

PSI Pipeline Services

Underground Construction Company, Inc.

Vista Precision Solutions, Inc.

Westex Company



Office of the State Fire Marshal Approved Hydrostatic Testing Companies Details of Company Approval Page 15 of 26 List is Current as of: List Expires: 08/21/2017 06/30/2018

Company Name	Hansa Consult of North	America, LLC (HCNA)				
Address	200 International Drive, Bldg, 120 Portsmouth, NH, 03801					
Business Phone	603/422-6833	603/422-8833				
Business Fax	603/422-8865					
Email Address	cfenton@hcna-llc.com					
Employees Approved to WITNESS Testing Activities	Charles Fenton Logan Phelps	Daryl Vorderbruggen Michael Sherlock	Joerg Hoehner Walter Phelps			
Employees Approved to CERTIFY Test Results	Joerg Hoehner					



January 19, 2018 HCNA Project: 2017-1076

Hansa Consult of North America, LLC appreciates the opportunity to be of service to your organization. Because we are constantly striving to improve our service to you, we welcome any comments or suggestions you may have about how we can be more responsive to the needs of your organization. If you have any questions about the testing, analytical results, or this report, please give us a call at 1-888-MY-HANSA.

ATTACHMENT K TESTEX API 653 PERSONNEL TESTING

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NAME: Agistin Non

		TOP-SIDE	PITTING	
PLATE NUMBER		LOWER RIGHT ARKED "TOP"		
NOMBLIC	Х	Y		
001				

		BOTTOM-S	DE PITTIN	NG	
PLATE NUMBER	The state of the s	LOWER RIGHT RKED "TOP"			
NOWIDER	Х	Υ			
	7 000	15			
_	8	-8	,		
	4	18	4	-	
4	2	78		+	
003	y	14			34
	1.5	95			
				-	
		/		1	-

DATE: 12/4/17

		TOP-SIDE	PITTING		
PLATE NUMBER		A LOWER RIGHT ARKED "TOP"			
IVOIVIDEIX	X	Y			
	10	14 4	7		
	9.5	101			
004	_8_	45			
	15	6.5 V	7.5	185	
	5	8.	7.5	14	
	2	DV	2	16	
	y	20			

		BOTTOM-SI	DE PITTING	
PLATE NUMBER		LOWER RIGHT ARKED "TOP"		
NOIVIDER	Х	Υ		
004				

NAME: SLOTT KEUSE

2011 1-200-	DATE:
TOP-SIDE PITTING	The same
CHES FROM LOWER RIGHT CORNER MARKED "TOP"	PLATE INC

NUMBER .	CORNER MA	RKED "TOP"		
NOIVIBER	Х	Υ		
001				
-				

		BOTTOM-SI	DE PITTI	NG	
PLATE NUMBER		I LOWER RIGHT			
NOWIDER	Х	Y			
	2	18			
	4	14			
	2	8			
	8	15			
	පි	8			
003	4-5	14			
	7	8-9			

DATE: 12/4/17

TOP-SIDE PITTING						
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"					
IVOIVIBLIC	Х	Υ				
002						

		BOTTOM-SI	DE PITTIN	IG	
PLATE NUMBER		A LOWER RIGHT ARKED "TOP"			
NOWBER	Х	Y			
	3-4	20			
	2	16			
	2	7			
	9	14			
	9	10			
004	9	4			
		18			

NAME: Andrew Kim

		TOP-SIDE	PITTING	
PLATE NUMBER		LOWER RIGHT ARKED "TOP"		
MOINIDEK	Х	Υ		
	2 3/8"	3 3/4"		
	1"	19 /2"		
	7/2"	93/4"		
001	4/4"	16 48"		
	7/2"	37/4"		
	10"	12/4"		
	8 /2"	20/8"		

		BOTTOM-S	IDE PITTIN	G	
PLATE NUMBER	The second second	LOWER RIGHT ARKED "TOP"			
NOWIDER	X	Υ			
	2/2"	175/8"			
	43/8"	133/8"			
	13/411	9/2"			
	8/411	7 1/4"	્ર		
	774"	1511			
003	7-8/211	8/8"			
	11/1	12/4/1			
	814"	15 "			

DATE: 10-25-17

		TOP-SIDE	PITTING	
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"			
,	Х	Υ		
	12"	8/2"		
	40	12/2"		
	3/2"	1911		
002	7 18"	13%"		
	93/4"	2 3/4"		
	ilu	9 /4"		
	97/8	20 1/2"		

		BOTTOM-S	DE PITTIN	NG	
PLATE NUMBER	The second secon	LOWER RIGHT ARKED "TOP"			
NOWIDER	Х	γ			
	2/41	74			
	M"	200			
	6 1/4"	19"			
	5"	20"			
	6 36	15"			
004	8"	1811			
	721	HII			
	7/2"	100			
	81/2"	4"			
	101/2"	14"			
	9/2"	10441			

NAME: Emmanuel Ugochukwu

		TOP-SIDE	PITTING		
PLATE		LOWER RIGHT	DIA.	DEPTH	REMAINING WALL
NUMBER	Х	Υ			(APPROX.)
	81/2	20			/
	1	19			
	41/2	16		7	
	10	12			
001	4 1/2	10			
001	71/2	5		1	
	242	4	/		
			7		
			1		

		TOP-SIDE	PITTING		
PLATE NUMBER		LOWER RIGHT ARKED "TOP"	DIA.	DEPTH	REMAINING WALL
IVOIVIDEIX	Х	Υ			(APPROX.)
7 X VT	10	3			
	5	9			/
	10	9		/	
	4	123		/	
002	8	14			
5 x LEET	342	19		X	
Crei	10	2012			
			/		
			/		
			(

		BOTTOM-SI	DE PITTING	i	
PLATE NUMBER	A CONTRACTOR OF THE PARTY OF TH	LOWER RIGHT ARKED "TOP"	DIA.	DEPTH	REMAINING WALL
NOIVIDEN	Х	Υ			(APPROX.)
7 41	3	X		/	240
	2	14	_		237
	4	181/2			242
-X	7 1/2	51/2		_	240
	6	8/2			104
	6	14			240
003	8/2	9			242
	9	15/2	-		135

		BOTTOM-SI	DE PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
	Х	Υ			(APPROX.)
	5	7.			230
	5	20		-	160
	8	8			233
	4	16			230
	9	16	*		235
	6/2	19			236
004	11	10			236
	7/2	14			232
					14
j_ = 10					

NAME: Brad

TOP-SIDE PITTING						
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL	
NOWBER	Х	Υ			(APPROX.)	
	1	19			1	
	2	4			/	
	4	93				
	4	16				
001	72	5		X		
001	81/2	20	/			
			/		1	
			/			
		/				

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
HOMBEN	Х	Υ			(APPROX.)
TXVT	34	19			
1	41/2	84			
	4	12			
	8	14			
002 5×LFET	9 1/2	3			
	(0)	20 1/2			
7 6161	11	9			

NUMBER X Y (AI	REMAINING WALL (APPROX.)
003 - Zt 8t - 4 14	
003 - Zt 8t 1 14	
003 - Z± 8± 	
003 - 7 8 8 5 - 4 14	
7 14	
7 14	
2 14	

PLATE NUMBER	INCHES FROM CORNER MA	LOWER RIGHT RKED "TOP"	DIA.	DEPTH	REMAINING WALL
NOWIDER	Х	Υ			(APPROX.)
	,75	7	2/7		+175
	25	16	1.		1204
	4	8		-	1198
	75	15			238
	83	18 5			1115
	6	185			,230
004	75	100			-
	10	10 -	79/10		.119
	105	135	10/14		.103
	105	175			
	10	21	10/22		1123
	9	4	21	/10x	1161
	H	194	27	1016	1.204

BASE 0,233

FALSEH Plate

NAME: 1446

TOP-SIDE PITTING							
PLATE	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
NUMBER	Х	Υ			(APPROX.)		
	25	3 t					
	72	4					
	45	9 2					
	10	122					
001	42	16					
001	1	192					
	85	20					
					-		

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOMBER	Х	Υ			(APPROX.)
	10	3	1		/
	4.5	2.5	1		/
	17	9.5		/	
	4	12.5		/	
000	8	14		X	
002	3.5	19			
	10	20,5	1	1	
			1		1
			1		1
			/		1

	i i	BOTTOM-SI	IDE PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOIVIDEN	X	Υ			(APPROX.)
1	- 4	85			
L	3'	18t	0		
L	6	145			
	9	85			
	9生	15%			
	103	at.			
003		82	V		
	5	55	1		
	4 =	144	1		
	8	男主	-		-
	8	155	/		
	11	12	-		

PLATE	INCHES FROM L	Contract to the second	DIA.	DEPTH	REMAINING WALL
NUMBER	Х	Υ			(APPROX.)
	3	7			/
	2	16			/
	5	8			/
	4	15			/
	4	20		1	
	9	10		1	
004	9	14			
	8	18			
	9	9	-	1	
			-		1
					1
			1-		1

NAME: Joe Stanishausk

TOP-SIDE PITTING						
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL	
NOIVIDEN	Х	Υ			(APPROX.)	
	2 5/16"	3 5/8"				
	71/2"	3718"				
	41/2"	9 3/4"				
	10 1/16"	1214"				
001	4 3/8"	1618				
001	T "	191/7"				
	85/8"	201/8"				

TOP-SIDE PITTING						
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL	
NONDER	Х	Y			(APPROX.)	
	97/211	33/4				
	41/2"	89/14				
	10 5/16	9 1/4"				
	4118"	17318				
002	77/8"	13718"				
002	31/2"	191/16				
	9 7/8"	705/8"				

PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOWBER	Х	Υ			(APPROX.)
T	2	18			
	5	14			
		8.			
L	3	3			
	8	15			
	7	8			
003	6	11			
	9	7_			
				-	
				-	
					-

BOTTOM-SIDE PITTING						
PLATE NUMBER		M LOWER RIGHT MARKED "TOP"	DIA.	DEPTH	REMAINING WALL	
NONDER	Х	Υ			(APPROX.)	
	6	70				
	7	16				
	3	7				
	4	3				
	7-	18				
	7	15				
004	5	8				
	8-9	4				
	10	14				
	q	10				

NAME: TOM HARDIN

TOP-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
IVOIVIDEN	Х	Υ			(APPROX.)		
	3"	2.5					
	7.5	1 ~					
	10.	4.5"					
	16.	4.5					
001	4.1	7.5					
001	19	10"					
	90.,	2.5"					

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
IVOIVIDEIL	Х	γ			(APPROX.)
	8.	9			
	4.1	14"			
	6	21"			
003	185	19"			
003	2	27-			
902	7'	8"			
	7.	15			-
	11~	13 "			

BOTTOM-SIDE PITTING							
PLATE NUMBER	INCHES FROM CORNER MA		DIA.	DEPTH	REMAINING WALL		
HOWBER	Х	Υ			(APPROX.)		
	4,5	8.5					
	4-	12.5"					
	3,5"	19"					
	8,	14"					
1-0	70	3'					
002	11-	9.5"					
U03	10.	91.					
				-			
				-			

BOTTOM-SIDE PITTING							
		DIA.	DEPTH	REMAINING WALL (APPROX.)			
Х	Υ						
5	8.,						
4"	21"						
8.,	10"						
100	14"						
4"	フ゛						
-	16						
8"	21"						
	INCHES FROM CORNER MA	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y 3 8 7 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y 3 8 10 10 10 17 10 17 10 10 10 10 10 10 10 10 10 10 10 10 10	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y 3 8 10 10 10 10 17 10 10 10 10 10 10 10 10 10 10 10 10 10			



		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NONDER	Х	Υ			(APPROX.)
	24	3 5			
	75	334			
	45	934			
	10	17.4			
001	4 1	164			
001	1	195			
	85	204			

TOP-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
IVOIVIDEI	Х	Υ			(APPROX.)		
	3	10	/		/		
	4/2	8/2	1		/		
	11	9	1		/		
	4	12		1	1		
002	8	14		/			
002	3	19		1			
	10	21		/			
			1				
					- 3		

BOTTOM-SIDE PITTING							
PLATE NUMBER	and the second s	LOWER RIGHT ARKED "TOP"	DIA.	DEPTH	REMAINING WALL		
NOWIDER	Х	Υ			(APPROX.)		
	- 1	9			/		
4	5	14			/-		
-	- 2	18			_/_		
	7	8					
1	8	8					
002		12		-/-			
003	8	15					
				/			
			-		-		
			-/				
			/				

BOTTOM-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
,,omben	Х	Υ			(APPROX.)		
	2	7			/		
	2	16	1		/		
	4	20	70				
	5	8					
	7	15					
	9	10		/			
004	10	14					
	11/2	16					
	-7	19					
			/_				
			1				
			1		1		

AME:

RON ALLON

TOP-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
NOWIDER	Х	Υ			(APPROX.)		
-	21	3 ½	1		/		
	7 +	4			/		
	山土	10		/			
	10	12		/			
001	H主	16		/			
001	- 1	193		/			
	X ½	20	/				
			/		1.		
			1		1		
			4				

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOWIDER	Х	Υ			(APPROX.)
002	10" 412 11 4 3/1 10	3" 9"/4 12"/2 14 19 70/2			

BOTTOM-SIDE PITTING							
The state of the s		DIA.	DEPTH	REMAINING WALL			
Х	Υ			(APPROX.)			
- 2	9						
- 35	14						
- 3	19			/			
1	9	3,					
8	15		1				
5	5		/				
			X				
			/)				
			/				
		/		1			
		/					
		/		-			
	CORNER M.	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y Z 9 3 19	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y Z 9 3 19	INCHES FROM LOWER RIGHT CORNER MARKED "TOP" X Y Z 9 3 19			

		BOTTOM-SIL	DE PITTIN	G	
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NO MIDEN	Х	Υ			(APPROX.)
	2 %	7			/
	4	20	7		
	5	7			1
	3	15		1	
	7	7		1	
	7	15		X	
004	7	19		1 1	
	9	10		/	
	9	14			176
			-/-		100
			· ·		
		1 50			

NAME: Dennis STEFanko

TOP-SIDE PITTING								
PLATE	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL			
NUMBER	х >	γΛ		DEPTH	(APPROX.)			
	23/2	3 3/4						
	フナ	4						
	45	93/4						
	10	12 5		1				
001	44	164						
001	1	195						
	8 克	Zot						
	2							
		3						

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NONDER	X	Υ			(APPROX.)
	93/4	23/4			/
	412	8/2			
	11	9/4			/
	4/4	12/2			V
002	8	14		/	
	3/2	19		/	
	10	20/2		/	1

		BOTTOM-SIC	Z PITTING		
PLATE NUMBER	Company of the Compan	LOWER RIGHT ARKED "TOP"	DIA.	DEPTH	REMAINING WALL
NOWIDEN	Х	Y			(APPROX.)
2-	2主	18			
t _o	2	84			
-	- 2	334			
L	- 42	19			
, L	5	5			
	5	35	END	of plate	
003	- 8	15			
1	75	8		-	
	9	4			
	92	34			
L	11	12			

BOTTOM-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
NOWIDER	X	Υ			(APPROX.)		
	3	20					
	2	7					
	3	5					
	4	20					
	5	15					
	5	8					
004	5	4					
	8	19					
	92	14					
	9	10					
	8	4					

NAME: Bill

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOIVIDEN	Х	Υ		DEPTH	(APPROX.)
	3	2			/
All	7	1			/
rine.	10	4		/	1
locuted	17	'S			
001	5	8		/	
001	12	10			
V7 _	20	8	/		
+3 El					
			/		
			/		

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
IVOIVIDEIX	Х	Υ			(APPROX.)
7 /	9	2			
/XVI	10	9			/
cvd	4	12			
2 VE	7	13			
002	4	8			
002	3	19		DEPTH	
	9	20			

	BOTTOM-SIDE PITTING								
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL				
, to moen	Х	Υ			(APPROX.)				
	22	182	_	-	242				
	5	14	_	_	245				
	2	8 1/2		/	242				
	8.1/4	15			245				
	4'	14	_		246				
	8	8	_		169				
003	5	5	_	_	185				
	71/2	15			129				
	11/2	12			170				
	7	8/2	1	_	186				

		BOTTOM-SI	DE PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOWIDEN	Х	Υ			(APPROX.)
	2	7			/
	2	15			/
	4	19			
	5	9'			
	7	15		/	
	9	11			
004	9,5	14			
	11	16	/		
1 - 12	7	19	/		
			/		
		/	/		

NAME: Mark

TOP-SIDE PITTING							
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL		
. ·	X	Υ			(APPROX.)		
UXVT	2	32			/		
LF	7	5	1		/		
3X ET	4	974		J			
	10	12'	1				
001	4	16	,				
001	/	19/2		X			
	8	20	1				
			/				
			1				

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOMBER	Х	Y			(APPROX.)
74118	10	3			7
1 ~ 07	5	9			1
5XET	11	9			
	4	12 3		1	
002	8	14		-/-	
002	4	19		1	
	15	205			
			1		
			- 4		

		BOTTOM-SII	DE PITTIN	G	
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
NOWBER	Х	Υ			(APPROX.)
	1	14	_	_	240
	3/2	18 1/2	_		238
	5	83/4			216
	7	\$9			240
	6/2	15			243
	8	15			242
003	12	12		-	174

BOTTOM-SIDE PITTING						
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL	
	Х	Υ			(APPROX.)	
	2	7			1	
	2	16			-11	
	4	20				
	5	8				
	6	15				
	9	10				
004	10	14		1		
	7	19		1		
				1	<u> </u>	
			-			

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
	Х	Y			(APPROX.)
001	2 3/8	3 5/8	0.250	0.060	0.190
	7 1/2	4 7/8	0.250	0.068	0.182
	4 1/2	9 3/4	0.375	0.145	0.105
	10 1/16	12 1/4	0.375	0.125	0.125
	4 3/8	16 1/8	0.250	0.085	0.165
	1	19 1/2	0.250	0.091	0.159
	8 5/8	20 1/8	0.375	0.153	0.097

		BOTTOM-SII	DE PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
	Х	Υ			(APPROX.)
003	2 1/2	3 3/16	0.500	0.178	0.072
	9 3/4	2 3/16	0.375	0.145	0.105
	5 1/4	5 1/4	0.250	0.083	0.167
	7 7/16	8 1/8	0.500	0.170	0.080
	1 5/16	8 3/8	0.375	0.142	0.108
	10 7/8	12 1/8	0.250	0.098	0.152
	4 7/16	13 7/8	0.500	0.210	0.040
	7 3/16	15 1/16	0.375	0.123	0.127
	2 1/8	18 5/16	0.375	0.138	0.112
	9 5/8	21 1/8	0.500	0.160	0.090
	5	21 3/4	0.375	0.130	0.120

		TOP-SIDE	PITTING		
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
	X	Y			(APPROX.)
002	9 7/8	2 3/4	0.375	0.123	0.127
	4 9/16	8 9/16	0.375	0.169	0.081
	10 15/16	9 1/4	0.250	0.090	0.160
	4 1/8	12 3/8	0.250	0.083	0.167
	7 7/8	13 7/8	0.375	0.128	0.122
	3 7/16	19 1/8	0.250	0.083	0.167
	9 13/16	20 5/8	0.250	0.084	0.166

		BOTTOM-SI	DE PITTING	5	
PLATE NUMBER	INCHES FROM LOWER RIGHT CORNER MARKED "TOP"		DIA.	DEPTH	REMAINING WALL
	X	Υ			(APPROX.)
	3 1/16	3	0.500	0.180	0.070
	7 7/8	4	0.500	0.190	0.060
	2	7	0.375	0.162	0.088
	5 3/16	7 15/16	0.250	0.098	0.152
	9	10	0.375	0.155	0.095
004	10	13 15/16	0.500	0.195	0.055
	6 1/16	14 13/16	0.375	0.150	0.100
	2	15 7/8	0.250	0.083	0.167
	7 5/16	18 9/16	0.375	0.150	0.100
	4	20 15/16	0.500	0.195	0.055
	10	21 15/16	0.375	0.152	0.098



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